Daily Assistant, Down

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A Short, Eafy, and Plain Method

OF KEEPING

A JOURNAL at SEA,

In which are contained,

RULES,

SHEWING

How the Allowances for Leeway, Variation, Heave of the Sea, Set of Currents, &c. are to be made, and to correct the Dead-Reckoning by an Observation, in all Cases: And also all the TABLES that are any Ways necessary for the SEAMAN's Use in keeping a Journal.

By THOMAS HASELDEN,
Late Teacher of the MATHEMATICS in the
ROYAL NAVY.

LONDON:
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T. PAGE, jun. on Tower-Hill.

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A Short, Esting and Plain Method

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Letter of the MATLETATICS IN ALLES

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To the REALER

READER.

AVING been educated in the Theory of Navigation, almost from my Childhood, and having had about sixteen Years Experience of the Practical Part at Sea, both in the Merchants Service, and also as Teacher of the Mathematics in the ROYAL NAVY; and having, in the Course of that Time, generally observed, that many Seamen would gladly keep a Reckoning, had they any short, easy and plain Method to do it by; but are deterred from it by the Want thereof. And also, that there are others who throw their Money away to little or no Purpose, by going to School to such Masters, of which Sort (there are too many) that have only got a Smattering of the Theory, and a few Terms of Art by Rote, which enables them to talk in such a Manner as to deceive those they pretend to teach, and having never been at Sea, cannot know any Thing of the Practice.

Therefore, for the Use of such in particular, and all other Seafaring Men in general, I have written the following Treatise; in which, I think, I have inserted all the Rules, and all the Tables, with their Uses, that are necessary to be used in any Case at Sea: And also, particular Rules for keeping a Journal, with the Manner of correcting the Dead-Reckoning by an Observation, either for

A 2

one Day, or a longer Time; the first of which, viz. correcting for one Day, has been treated of by several Authors; but the latter, viz. correcting for a longer Time, I know has been barely mentioned in several, but not particularly explained by any Author at all, I believe, at least not in those I have read; and for that Reason I have done it in the Journal at the latter End of this Book, it being absolutely necessary for every Man who keeps a Reckoning to know it; because they are more likely to be out in their Reckoning, when they have one every Day, and consequently more necessary to correct for three or four Days, than for a single one.

I do not begin this Book with Arithmetic, as is common with most of the Books on this Subject; because I think, if any Person has had so little Education, as not to be capable of adding, substracting, multiplying, and dividing, he will scarcely be able to make any Progress either in Arithmetic or Navigation, by the Help of Books alone, without the Assistance of a Master; and that putting such Things into Books of this Kind, serve only to enhance the Price, and are of no real Service to the Reader. And now having given an Account of the Reasons which induced me to publish this Book, (which I hope, and am pretty well assured, will be found the most useful Book of its Kind now extant) for the daily Practice at Sea. I have nothing more to add, but to beg the Reader's kind Acceptance of it.

And am

Their humble Servant,

Thomas Haselden.

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TABLE

OF

DIFFERENCE of LATITUDE

AND

DEPARTURE

To every Single DEGREE,

And as far as 300 Miles DISTANCE.



DIFFERENCE. of LATIFFEE

And as far as 300 Miles Distantes.

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6	06.000	0.1	56	56.0	01.0	106	106.0	8.10	156	156.0	02.7	206	206.0	03.5		256.0	04.4
7	07.0 00	0.1	57	57.0	01.0	07	107.0	01.9	57	157.0	02.7	07	207.0	03.6	RECOMMENDED.	257.0	04.4
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TI	11.000	A series	61	61.0	100000000000000000000000000000000000000	111	111.0	01,9	161	161.0	02.8	211	211.0	03.6	261	261.0	04.5
12	13.000		62		01.1	13	112.0	01,9	62		02.8	12	212.0	03.6	F 41 - 22 SPA	262.0	04.5
13	14.000	100 100	64		01.1	14	114.0	02.0	64	163.0	02.8	13	213.0	03.7		263.0	04.5
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22	22.000	0.4	72		01.3		122.0	02,1	72	172.0	03.0	22	222.0	03.8	1000	272.0	04.7
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26	26.00		76	76.c	-		126.0	02.2	176	176.0	03.0	1 1 1 1 1	226.0	03.9		276.0	04.7
27	28.00		77		01.3		127.0	02.2	77	177.0	03.1	27	227.0	03.9		277.0	04.8
29	29.00		79		01.4	- BAR 170	129.0	02,2	79	179.0	03.1	12.5	229.0	03.9	The second	278.0	04.8
30	30.00		80		01.4	10.8	130.0	02,3	80	180.0	03.1	1000,000	230.0	03.9		279.0	04.8
31	31.00		81	81.0	01.4		131.0	02.3	181	181.0	03.1	231	231.0	04.0	-	281.0	04.8
32	32.00		82		01.4		132.0		82	182.0	03.1	1000	232,0	04.0		282.0	04,8
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35	35.00	0.6	85	85.0		33	135.c	02,3	85		03.2	35	235.0	04.0	85	285.0	04.9
36	36.00	0.6	86	86.0	01.5	136	136.0		E 200 (1770) (180)	186,0	03.2	236	236,0	04.1		286.0	04.9
37	37.00			87.0	01.5	37					03.2		237.0	04,1	87	287.0	
	38.00				01.5	1911-1911	138.0			188.0	03.2		238.0			288.0	
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48	48.00	0.8	98	98.0	01.7	48	148.0	02.6	98	198.0	03.4	48	248.0	04.3		298.0	
49	49.00				01.7					199.0			249.0	04.3	99	299,0	05.1
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	3.0		53	53.0		03	102.9	03.6	53	152.9	05.4	03	202.9	07.1		252.8	08.9
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	9.0	Contract Con	59	60.0		10	109.4	03,9	60	159.9	05.6	10	209.9	07.4		259,8	09.1
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27.77		30.6	67		02.3	17	116.9	04.1	67	166.9	05.8	17	216.9	07,6		266.8	09.3
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31		01.1		81.0			131.9		82		06.4		231.9	08.1	2.0	281.8	09.9
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2		00.1	100 mg (100 mg)	-	02.7	028003000	101.9	05.3	52	151,8	08,0	02	201.7	10.t		251.6	13.2
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	-	00 3		54.9	02 9	-	104.9	05,5	-	154.8	08.1	05	204.7	10.7	55	254,6	13,3
	06,0	9,617571657	DESCRIPTION OF		02,9	170	105,9	05,5	156	155.8	08.2	206	205.7	10.8	256	255,6	13,4
		00,4		SECTION AND ADDRESS.	03.0	to the second	106.9	05,6		156,8	08,2	STATE OF THE PARTY.		10.8		256.6	13.4
		30,4			03,0		107.8	05.7	58	157,8	08.3		207.7	10.9		257.6	13,5
	10,0	00,5		58.9	03,1		108,8	05,7		158.8	08.3	10000000	208.7	10,9		258.6	13.6
	-		-	59,9	03.1		109.8	05.8	and the same	159.8	08,4	10	209.7	11.0	-	259.6	13.6
	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	00.6		60,9	03.2		110,8	05.8	100000000000000000000000000000000000000	160.8	08,4	Carlotte Cale	210.7	11.0	261	260,6	13.7
	100	00.7		61.9	03.2	STATE OF THE PARTY	111,8	05,9		161.8	08.5	1000	211.7	11.7		261.6	13.7
	13.0	00.7		63,9	03,3	13	112,8	05.9		162.8	08.5	13	212.7	11.1		262.6	138
		00.8		64,9	03,4	14	113,8	06.0		164.8	08.6	14	213.7	11,2		263.6	13.8
		00.8	-						-	-	Account to the second	15	214.7	11.2	65	264 6	13:9
	17,0	00.0		65,9	03.5	116	115.8	06,1	166	165.8	08.7	216	215.7		32	2656	13.9
	18.0	0.9		67 9	03.6	17	117,8	06.2	DATE OF THE PARTY	166.8	08.7		216.7	11.4	67	266.6	14.0
100	19.0	01.0		68.9	03.6		118.8	06.2		\$100 market \$100 m	08.8	S 6 4 5	217.7	11.4	68	267.6.	14.0
20 20.0 01.0 70 69,9 03.7 20 119,8 06.3 70 169.8 08.9 20 219.7 11,5 70 269.6 14.1 21 21.0 01,1 71 70.9 03.7 121 120.8 06.3 171 170.8 09.0 221 220,7 11.6 271 270.6 14.2																	
	-	21.1		-	-	-		-	-			-		-	-	-	
115	-	Process of the same	A COLUMN TO SERVICE			A COUNTY OF			A CONTRACTOR OF THE PARTY OF TH		ALTONOMIC STREET	100			E. S.		
A2 (100)	23,0	01.2	73	72,9	03.8	23	Mary Carl B. Land	06.4		172.8	09,0	22	221.7	11.6	72	271,6	14.2
	24,0	01,3	74	73,9	03.9	24	123.8		74	173.8	09.1	23	222.7	11.7		272,6	14.
25	25,0	01,3	75	74,9	03.9	25	124.8	06.5	75	174.8	09,2	24	224,7	11.7	74 75	273,6	14.
	26.0	01,4	76	75,9	04 0	126	125,8	-	176	175.8	-						14.
13120 2	27.0	01.4	77	76.9	04.0	27	126,8	The state of the s	77	176.8	09 2	226	225.7	11,8	276	275 6	14.
28	28.0	01.5	78	77.9	04,1	28	127,8	06,7		177.8	09,3	27	227.7	11,9	77 78	276,6	14.
29	29.0	31,5	79	78,9	04,1	29	128,8			178.7	09,4	29	228.7	12.0	79	278.6	14.
30	10,0	01,6	80	0.0000000000000000000000000000000000000	04.2	30	OF REAL PROPERTY.	06 8	80	179.7	09.4	30	229.7	12.0	80		14.
31	31,0	01.6	81	80,9	04,2	131	130,8	06.9	181	180.7	09.5	231	230.7	12.1		280.6	_
32	32,0	01.7	82	81.9			The state of the same of		82	181.7	09.5		231.7	12.1	82		14.
33	33.0	01.7	83	82,9	04.3		132,8	the state of the s	83		09.6			12.2	THE RESERVE OF THE PERSON NAMED IN	282.6	14.
34	34,0	01.8	84	83,9			133,8		84	183.7	09.6		233.7	12.2		283.6	14.
35	35.0	01.8	85	84,9	04 4	35			85		09.7	35	234.7	12,3	85		14,
36	35,9	01.9	86	85,9	04.5	136	135,8	07.1	186	185.7	09.7	236	235.7	12.3			
37	36,9	01.9	87	86,9	04.6	37			87	186.7			236.7			286,6	
38	37.9	02,0	88	87,9	04.6	38	137,8	07.2		187.7	09.8	100 100 100			88	287.6	
	38,9				94.7				III MATERIAL IN	188.7		39		12.5	89	288.6	15,
40	39.9	02,1	90	89,9	04.7	40	139.8	07.3	90	189.7	09.9			12.6	90	289.6	15,
41	40.9		91	90.	04.8			07.4	191	190.7	10.0		and the second	12.6	-	290.6	15.
42	41.9		92	91.9	04.8	42	141.8	07.4	92	191.7							
	42,9				04.9		142.8	07.5	200	192,7	10,1					292.6	
44	43,9	02,3		93,9					(0) PR - P - P - P - P - P - P - P - P - P	193.7		44	243.7	12.8	94	293.6	15.
45	44.9	02,4	No.	-	05.0						10,2	45					
46	45.9	02,4			05.0		145.	8 07,6		195.7	10,3	246	245,7	12,9		A Commenced	
47	46,9		97	96.9	05.1	47	146.	8 07,7		196,	10.3	47	246,7	12.9			
48	47,9	02.5	98	97.9	05.1	48	147.	07.7	100 00000000000	197.		48	247.7	13,6		297 6	15.
49	48.9	The second second	99		05.2		148.	07,8					248.7				15.
50	49.9	02.6	The same of the last		05.2	No. of Concession, Name of Street, or other Persons, Name of Street, or ot		and the same of th	200	199.	10.5	250	249.7	13.1	300	279.6	
Dift	Dan	Lat	Die	Der	Tat	Di	t Dep	STATE OF THE PERSON NAMED IN	D.(Dep	Lat	Dif	-	Lat	1	Dep	La

for 87 Deg.

4 Difference of Latitude and Departure for 4 Deg.

3:0												the ent-		Sept to a sep			
Dift	Lat	Dep	Dift	Lat.	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep
1	0.10	00.1	51	50.9	03.6	IOI	100.8	07.0	151	150.6	10,5	201	200.5	14.0	251	250.4	17.5
2	02.0	00.1	52		036		101.8	07.1		151,6	10.6	100000000000000000000000000000000000000	201.5	14.1	52	251.4	17.6
3	03.0	00.2	53		03.7	17 17 17 17	102.8	07.2		152.6	10.7	10000	202.5	14,1	1. 200	252.4	17.6
4	04,0	00.3	54		03,8	04	103.8	07.2		153.6	10.7		203.5	14.2	54	253.4	17.7
_5	25.0	00.3	55	54.9		05	104.7	07,3	55	154.6	10.8	05	204.5	14.3		254.4	17.8
6	06.0	00.4	56		03.9	106	105.7	07.4		155 6	10.9	206			-	District Control	
7	27.0	30.5	57		24.0	07	106.7	07.5	57	156.6	10.9	07	205.5	14.4	256	255.4	17.8
8	08.0	00.6	58		04.0	08	107.7	07,5	58	157.6	11.0	08	207.5	14.5		257.4	17,9
9	09.0	00.6	59		04.1	09	108.7	07.6	59	158.6	11.1	00	208.5	14.6		258.4	
10	10.0	20.7	60	140 11 11 11	04.2	10	109.7	07.7	60	159.6	11.2	10	209.5	14.6		259.4	18.1
11	11.0	00.8	61	-	04.3	111	110.7		161	160.6	-					-	
12	The second	00.8	62	61.0		12	1117	07.7	62	161.6	11.2	12	210.5	14.7		260.4	18.2
13		00.9	63	52.8	1 1 3	13	112.7	07,9	63	162.6	11.3	13		14.8		261.4	18.3
14	-	01.0	64	63.	04.5	14	113.7	07.9	64	163.6	11.4	14	212.5	14.8		262.4	18,3
15	150	01.0	65	64.8		15	114.7	08.0	65	164.6	11.5		214.5	14.7	64	263.4	18,4
1.50	16.0	_	66	-	-				166	-		-		150	65	264.4	18.5
16	17.0	01.1	67	66.8		116	115.7	08.1	67	165.6	11.6	216	215.5	15.1		265 4	18.5
17	0	1000	68	67.8	- 77/	17	116.7			166.6	11.6	17	216.5	15,1	67	266.4	
18	19.0	01.3	69	68.8	04.7	18	117.7	08,2	68	168.6	11.7	1 1 2 2 2 2	217.5	15.2		267.4	18.7
20 20.0 01.4 70 69.8 04.9 20 119.7 08.4 70 169.6 11.8 20 219.5 15.3 70 269.4 18															18.7		
21 20.9 01.5 71 70.8 05.0 121 120.7 08.4 171 170.6 11.9 221 220.5 15.4 271 270.3 18															18.8		
22 21.9 01.5 72 71.8 05.0 22 121.7 08.5 72 171.6 12.0 22 221.5 15.5 72 271,3 10															18.9		
1000					3	1 7 2 300					The second second	40	-		72	271,3	190
23 22.9 01.6 73 72.8 05.1 23 122.7 08,6 73 172.6 12.1 23 222.5 15.5 73 272.3 19. 24 23.9 01.7 74 73.8 05,2 24 123.7 08.6 74 173.6 12.1 24 223.5 15.6 74 273.3 10.															19.0		
23 22.9 01.6 73 72.8 05.1 23 122.7 08.6 73 172.6 12.1 23 222.5 15.5 73 272.3 19.6 24 23.9 01.7 74 73.8 05.2 24 123.7 08.6 74 173.6 12.1 24 223.5 15.6 74 273.3 19.6															19,1		
24 23.9 01.7 74 73.8 05,2 24 123.7 08.6 74 173.6 12.1 24 223.5 15.6 74 273.3 19,1 25 24.9 01.7 75 74.8 05.2 25 124.7 08.7 75 174.6 12.2 25 224.5 15,7 75 274.3 19.2															19.2		
26	25 24.9 01.7 75 74.8 05.2 25 124.7 08.7 75 174.6 12.2 25 224.5 15.7 75 274.3 19.2 26 25.9 01.8 76 75.8 05.3 126 125.7 08.8 176 175.6 12.3 226 225.5 15.8 276 275.3 19.2															10.2	
27		01.9	77	76.8		27	126.7	08.9	77	176.6	12.3	27	226.5	15,8	77	276,3	19.3
28	27.9	02.0	78	77.8	05.4	28	127.7	08.9	78	177.6	12.4	28	227.5	15,9	78	277,3	19.4
29	28,9	02.0	79	78.8		29	128.7	09.0	79	178.6	12.5	29	228.5	16.0	79	278.3	19,4
30	29.9	32.1	80	79.8	05.6	30	129.7	09.1	80	179.6	12.5	30	229.4	16,0	80	279.3	19,5
31	30.9	02.2	81	80.8	○5.7	131	130.7	c9.1	181	180.6	12.6	231	230.4	16.1	281	280.3	19.6
32	31.9	02,2	82	81.8		32	131.7	09.2	82	181.6	12.7		231.4	16.2	82	281.3	19.7
33	32.9	02,3	83	82.8	05,8	33	132.7	09,3	83	182.6	12.8	33	a The Act of the	16.2	83	282.3	19.7
34	33.9	02.4	84	83.8		34	133.7	09.3	84	183.6	12.8	34	233.4	16.3	84	283.3	19,8
35	34.9	02.4	85	84.8	05.9	35	134.7	09,4	85	184.6	12.9	35	234.4	16.4	85	284.3	19,9
36	35.9	02.5	86	85.8	06.0	136	135.7	09.5	186	185.6	13.0	236	235.4	16.4	286	285.3	
37	36.9		87	86.8	05.1	37	136.7	09.5	87.	186.6	13.0		236,4	16.5	87	286,3	19.9
38		02,7	88	87.8	06.1		137,7	09.6	88	187.5	13 1	38	237.4	16.6	88	287.3	20.0
39		02.7	89	88.8	06.2	39	138.7	09.7	89	188.5	13.2		238.4	16.7	89	288.2	20.1
40	39.9	2.8	90	89.8	06.3	40	139.7	09.8	90	189 5	13.2		239 4	16.7	90	289.3	20.2
41	40.9	02.9	91	90.8	06 4	141	140.7	09.8	191	190.5	13,3		240.4	16.8	291		
42					06.4				100	191.5	13,4		241.4	16,9		290.3	20.3
43		03.0	93	92.8	06.5	43	142.7			192.5	13.5		242.4	17.9	93	292.3	20,4
44	43.9	03.1	94	193.8	06,6	44	100	10.0		193.5	13.5		243.4	17.0		293.3	20,4
45	44.9	03.1	95	94.8	06.6	45	144,7	10.1	95	194.5	13.6		244,4	17.1	95	294.3	20.6
46	2 2 2	03.2	96		06.7		145.6		-	195.5	13.7		245.4				
47		03.3	97	96.8	06.8	47	146.6	10.2	97	196.5	13.7		246.4	17.1	296 97	295.3	20.6
48	47,9	03.4	98	97.8	06.8		147.6		98	197.5	13.8		247.4	17.3		296.3	20.7
49	48.9	03.4	99	08.8	106 0	40	148.6	10.4	99	198.5	13.9		248.4	17.4		297.3	20,8
50	49.9	03.5	100	99.8	07.0	150		10.5		199.5	13.9	250	249.4	17.4		298.3	
			D:0				-					-	_			299,3	
Ditt	Dep	Lat	ווען	Dep	Lat	Din	Dep	Lat	Dit	Dep	Lat	Drit	Lat	Lat	Dift	Dep	Lat
	.73 77 1				3 45 145		The state of the		12.11	Action Steel	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.16	V. 1. 1. 1. 1. 1. 1.	1. A			

		D	D: O		D 1	D:ai	T -4 1	Deta .	Dia	1 04 1	Dan	Dial	T 1	D	D.0		D
Ditt	Lat	Dep	STATE OF THE PERSON.		Dep	_	Lat		Dift	Lat	Dep	-	Lat	-	Dift	Lat	Dep
1	01,0	00.1	51	50,8	04,4		100.6	08.8	THE RESIDENCE OF	150.4	STATE OF THE PARTY	10,000	200.2	A COLUMN TO SECOND		250,0	21.8
2	02,0	00.2		51,8	94.5		101.6	08,9		151,4	13.2	1	201.2	17.6		251.0	21.9
3	03,0	00.3			04.6	-	102.6	09.0	Britain Co.	152.4	13.3		202.2	17.7	OF THE OWNER OF THE OWNER, THE OW	252.0	22.0
4	04.0	00.3	54	53.8	04.7	1000000	103.6	09,0	54	153.4	13,4		203.2	17,7	STATE OF THE PARTY	253.0	22.1
_5	05,0	-	-	54,8		05		09.1	55	154.4	13.5	05	204.2	17.8		254,0	-
6	06,0	00,5	56	55.8	04.9	01,70	105,6	09.2	156	155.4	13,6		205.2	17.9		255,0	22.3
7	07,0	30,7	57 58	57,8	05,0	07	106.6	09,3	57 58	150,4	13,7	08	205.2	18.1		256.0	22.4
8	09,0	00,8	59	58.8	05.1	09	108,6	09,5	59	158.4	13,8	09	208.2	18,2	59	257.0	22.5
10	10,0	00,9	60	59,8	05.2	10	109.6	09,6	60	159.4	13.9	10	209.2	18,3	60	259.0	22.6
-	11.0	01.0	61	60,8	25,3	111	110,6	09,7	161	160.4	14.0	211	210.2	18,4	261	260,0	22,7
11	12.0	01.0	62	61.8	05,4	12	111,6	09.7	62	161.4	14.1	12	211.2	18.4	62	261.0	22,8
13	3 19 55	01,1	63	The second	05,5	13	112,6		63	162.4	14.2	13	212.2	18.5	63	262.0	22,9
14	13.9	31,2	64	63,8	05.6	14	113,6	09.9	64	163,4	14.3	14	213.2	18.6	64	263.0	23.0
15		01.3	65	64,8	05,7	15	114,6	10.0	65	164.4	14.4	15	214.2	18,7	65	264.0	23.1
16	15,9	01,4	66	65,7	05.8	116	115.6	10,1	166	165.4	14.4	216	215.2	18.8	266	265.0	23.1
17	1	01,5	67	66,7	05.8	17	116.6	10,2	67	166.4	14.5	17	216.2	18.9	67	266.0	23.2
18		01,6	68	67.7			117,6		68	167.4	14.6	18		19.0	68	267.0	23.3
19	The second		69		06,0	19	118.5				14.7	19	The second second	19,1		268.0	23.4
20	19.9	-	1-		-	20	119,5	\$10,4	70	169.4	14.8	20	219.2	19.1	70	269.0	23.5
21						121	120.5	10 5		170.4	14.9	221	220,2	19.2	271	270.0	23.6
2.2		1			06,3	22	121.5	10.6		THE PARTY OF THE P	15:0		191	19.3	72	271,0	23.7
23			, ,			23	122,5						222.2			272,0	23.8
2.4			74			24	123.5			173.3		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					23.8
25		-	13		-	-	-			_	15,2	-		19.6		274.0	23.9
26	1-6		100000			126	1 3.			175.3			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		276	275.0	24.0
27						27			1 '	The second second	1 ,				77	275.9	24,1
20	1.0.	B. 10. 11. 1		1 0	The state of the s		1 0		30 1533 -03	0		7.1	0				24.3
30		1					The second second			A CONTRACTOR OF THE PARTY OF TH			200		-		24.4
3	-		81	-	-	-		-	-	180.3					281	-	
3:								12.12	A CONTRACTOR OF THE PARTY OF TH				CA				
3										182.	15.0		A STAN OF				
3			84	1 83,7	07.3	A 127 C					16.0		THE LABOR TO SE	- 1		282.9	24,7
3		03,	1 8	5 84,	7 07.4	35	134,	5 11.7	8 8 9	College		35		20.4	85	283.9	24.8
3		9 03,	1 86		7 07,	136	135,	5 11.8	186		16,2		235	20.	286		24,9
3	7 36,	9 03.	2 8	7 86,	7 107,6	37	136,	5 11.	87	186.	16,	3 37	236.1	20.		285.9	25.0
3	8 37.	9 03.	3 8	8 37,	7 107,7	35	137,		28 6	187.	3 16.4		37.1	20,			
1 3	9 38,	9 03.	4 8	9 38.	7 07,	39				188.	16.4	1 39	238.1				
4	0 39.			89,			139.			and the same of	16.		239.	-			
4	1 40.	8 03,			7 07,	14						24	240.			289.9	25.3
4		8 03,		2 91.	6 08,										9:	2 290.9	
	3 42,	8 03.	8 9	3 9 ² , 4 93,	6 08.	4 4					3 16,		3 242.				
	4 43,	8 03.				3 4			5 9				4 243. 5 244.			292.9	
					6 08.			And in concession,					6 245,				
	6 45	8 04.	1 0	7 06.	6 08,	5 4	6 145. 7 14 6 .				3 17.		7 246,	1 21.	4 29	6 294.9	
1 4	18 47	8 04,	2 9	8 97.	6 08.	5 4	8 147.			8 197.	2 17.		8 247.			8 296	9 25.0
	10 48	8 04,	3 9	9 98,	6 08,	6 4		4 13,	0 9	9 198.	2 17.			1 21.	7 9		9 260
	0 49	8 04.			6 08.	7 15	0 149	4 13,	0 9	0 199.	2 17.	4 25	0 249.	1 21.	8 30	0 298.	9 25.9 9 26.0 9 26.1
	ilt De		t n	The second	p Lat		_	-	District of the last	fl Dep		7 7	h De	Lat		ft Der	
1-		P	14		r 1~u		, 50	r, ±a	121	, 20	La	- 12	A De	· Dal	10	ici Del	Dat

6 Difference of Latitude and Departure for 6 Deg.

		Section 1	Marie 1	12		A Property of		1									
6 06.0 00.6 56 55.7 05 9 106 105.4 11.1 156 155 1 16.3 206 204.9 21.5 256 254.6 26. 7 07.0 00.7 57 56,7 06.0 07 106.4 11.2 57 156.1 16.4 07 205.9 21.6 57 255.6 26, 8 08.0 00.8 58 57.7 06.1 08 107.4 11,8 58 157.1 16.5 08 206.9 21.7 58 256.6 27,														Dep			
No.	_	Minteres. 1	-		-	_			161	150.2	-	201		-			-
a series of	1740000	2000	DOUBLE STORY	100		100		7				200000000000000000000000000000000000000	STATE OF THE PARTY				
		The state of the s	100	3800 3500	CONTRACTOR	STATE OF THE PARTY.		The second second	2 3 3 3 3 3 3 3								The second second
			No. of Contract of	F						CONTRACTOR OF THE	and the second						
10 3 4		Charles Co., Co., Co., Co., Co., Co., Co., Co.,	N 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	100					4 / 10 / 10 / 10		A STATE OF THE STA	The second second	1 1 1 1 1 1 1 1				26.6
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10	10.9		60		06.3	10	109.4	11.5		159.1	16.7	10		21.9		258.6	27.2
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11		01-3			06,5	12	100	11,7	62		16.9	60.74573	209.8	22,0	30 77 10	259.6	27.3
113		014		62.7		13		11,8	63		17.0		211.8	22.3		261.6	27.4
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15	15.9	01.6	65		06,8	15	114.4	12.0		164.1	17.2	15	Section 1 to a 1 to 1	22.5	2	263.5	27.7
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16	17.9	01.8	67		7,0		116.4	12.1		166.1	17.5		214.8	22.6		265.5	27.8
18		31.9	68		07.1	0.5	117.4	12.3		167.1	17.6		216.8	22,8		266.5	28.0
19	19.5	02.0			07,2	19	118.3	12.4	69	168.1	17.7	19		22,9		267.5	28.1
20	20.9	02.1	70		07.3	20	119.3	12.5	70	169.1	17.8	20	218.8	23.0		268.5	28.2
-	-	02.2	-		07.4	-	-	126	171	170.1	17.9	221			-		28.2
21 22	20.9	02.3	71 72		07.5	121	120.3	12.7	72	171.1	18.0		219.8	23.1		269.5	28 4
23	22.0	02,4			07.6	23	122.3	12,9	73	172.0	18.1	23		23.3		270.5	28.5
24	23.9	02.5	74	1 1 1 21	07,7	24	123.3	13.0	74	173.0	18.2	24	222.8	23.4	74	272.5	28,6
25	24.6	02.6	75		07.8	25	124.3	13.1	75	174.0	18.3	25	223.8	23.5	75	273.5	28.7
26	25.9	02.7	76	75.6	-	126	125.3	13.2	176	175.0	18.4	226	224.8	23.6		-	28,8
27	26.0	02.8	77		080	27	126.3	13.3	77	176.0	18.5	27	225.2	23.7	276 77	274.5 275,5	28.9
28	27.8	02.9	78		08.1	28	127.3	13.4	78	177.0	18.6	28	226.7	23,8		276,5	29.1
29		03.0	79		08.3	29	128.3	13.5		178.0	18.7	2.9	227.7	23.9	1 6 T B * C	277,5	29.2
30	29.8	03.1	8c		08.4	30	129.3	13.6	80	179.0	18.8	30	228.7	24.0		278.5	29,3
	30.8	03.2	81	-	08.5	131	130.3	13.7	181	180.0	18.9	231	229.7	24.1	281	279.5	29.4
31 32		03.3	82		08.6	32	131.3	13.8	18 6 1 1 1 1 1	181.0	19.0		230.7	24.2	F (5.5) 50 50 50	280.4	29,5
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34		03.6	84	83.5	08.8	34	133.3	14.0	84	183.0	19.2		232.7	24.5			29,7
35	34.8	03.7	85	84.5	08.9	35	134.3	14,1	85	184.0	19.3	. 35	233.7	246		283.4	29,8
36		03.8		-		-	135.3	14.2		185.0	19.4	-	234.7	24.7		284.4	
37	36.8	03.9	87	86.5	09.1	37	136.2		87	186.0	19.5		235.7	24.8	87	285.4	29,9
38	37.8	04.0	88	87.5	09.2	38	137,2	14.4	88	187.c	196	38	236,7	24.9	88	286,4	30,0
39	38.8	04.1	89	188.5	09.3		138.2	14.5		188.0	19.8	39	237.7	25,0	89	287.4	30.2
40		04.2	90	89.5	09.4	40	139.2	14.6	90	189 c	19.9	40	238.7	25.1	90	288.4	30.3
41		04.3	91		09.5	141	140.2	14.7	191	189.9			239.7	25,2		289.4	
42		04,4			09.6	42	141.2	148		190.9	20,1		240.7	25.3		290.4	
43	42.8	04.5		92.5	09.7	43.		14.9		191.9	20.2		241.7	25.4		291.4	
44	43.8	04,6	94	93.5	09,8	44	143.2	15.0		192.9	20.3	T	242.7	25.5		292.4	30.7
	44.8	04.7	95	94.5	09.9	45	144,2	15.2	95	193.9	20.4	45		25.6	95	293.4	30,8
45	45.7	04.8	96	95.5	10.0	146	145.2	15.3	196	194.9	20.5	246	244,6	25.7		294.4	
47	46.7	04.9	97.	96.5	10.1	47	146.2	15.4	97	195.9	20.6	47	245.6	25.8	97	295.4	31.0
47 48	47,7	05.0	-98	97.5	10.2	48	147.2	15.5	98	196.9	20.7	48	246.6	25.9	98	296.4	31,1
49	48.7		99	98.5	10.3	49	148.2	15.6	99	197.9	20.8		247.6	26.0	99	297.4	31.2
50	49.7	05.2	100	99.5	10.5	150	149.2	15.7	200	198.9	20.9	250	248.6	26.1	300	298.4	31.4
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36	35.	70	4.4	86	85	,4	10.5	136	135.0	16.6	186	13.	4,6	22.5	STREET, STREET,	233,2	28,6	85	282.9	34.7	ı
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39	38.	70	4.8	89	88	3	10.7	38	137.0	16,8	.88	18	6,6	22,9	38	236,2	29.0	88	285.8	34.9	ı
40	39.	7 3	4.9	90	89	.3	0.11	40	139.0	17.1	89		7,0	23,0	39	237,2	29,1	89	286.8.	35,2	ı
41	10.7	10	5.0	91	90	.3	11.1	141	1.39.9	17.2	191		9,6	23.1	THE RESERVE	238.2	29 2	90	287.8	35,3	
42	41.7	0	5.1	92	91	.3	11.2		140.9		92	190	5,6	23,3		239.2	29.3	291	288.8	35.4	
43 44	42.7			93 94	92	.3	11.3		141.9	17.4	93	19	1,6	23.4		240.2	29.5	92	289.8	35,5	
45	14.7	0	5.5		93	.3	11.3 11.5 11.6	44	142.9		94	192	2,5	23,6		242.2	29.7	93	290.8	35.7 35,8	
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47	16.6	0	5.71	97	96.	.3	11,8	47	144.9	17.8	196	194		23.9	246	244,2	29.9		293.8	36,0	1
48	47.6	0	5 8	98	97.	.3	11.9	48	146.9	18.0	97 98	19		24.0 24 I	47	245.1	30.1	97	294.8	36,2	
49	48.6	0	6.1	1000	98.		12.1	49	147.9	18.1	99	19	7,5	24.2	48 49	246.1	30,2		295.8	36,3	
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35 34,7 04.9 85 84.2 11.8 35 133.7 18,8 85 183,2 25.8 35 232.7 32,7 85 282.2 39 36 35.7 05.0 86 85,2 12.0 136 134.7 18.9 186 184,2 25.9 236 233,7 32.9 286 283.2 39 37 36.6 05.2 87 86.2 12.1 37 135.7 19.1 87 185,2 26.0 37 234.7 33.0 87 284 2 40 38 37.6 05.3 88 87.1 12.2 38 136.7 19,2 88 186,2 26.2 38 235.7 33.1 88 285.2 40 39 38.6 05.4 89 88,1 12.4 39 137.7 19,3 89 187,2 26.3 39 236,7 33.3 89 286.2 40 40 39.6 05.6 90 89.1 12.5 40 138.6 19.5 90 188,2 26,4 40 237,7 33.4 90 287.2 40 41 40.6 05.7 91 90.1 12.7 141 139.6 19,6 191 189,1 26,6 241 238.7 33.5 291 288.2 40 42 41.6 05.8 92 91.1 12,8 42 140.6 19,8 92 190,1 26,7 42 239.7 33.7 92 289.2 40 43 42.6 06.0 93 92.1 12.9 43 141.6 19.9 93 191,1 26,9 43 240.6 33.8 93 290.2 40 44 43.6 06.1 94 93.1 13.1 44 142.6 20,0 94 192,1 27,0 .44 241.6 34.0 94 291.1 40 45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193,1 27,1 45 242.6 34.1 95 292.1 41 46 45.6 06.4 96 95 1 13.4 146 144.6 20.3 196 194,1 27,3 246 243.6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27,6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27,7 49 246.6 34,7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41	V 22 19 75		20 20100			A STATE OF THE REAL PROPERTY.	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1					AT THE STATE OF		230.7				39.
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37 36.6 05.2 87 86.2 12.1 37 135.7 19.1 87 185,2 26.0 37 234.7 33.0 87 284 2 40 37.6 05.3 88 87.1 12.2 38 136.7 19.2 88 186,2 26.2 38 235.7 33.1 88 285.2 40 39.8 05.6 90 89.1 12.5 40 138.6 19.5 90 188,2 26.4 40 237,7 33.4 90 287.2 40 41 40.6 05.7 91 90.1 12.7 141 139.6 19.6 191 189,1 26.6 241 238.7 33.5 291 288.2 40 42 41.6 05.8 92 91.1 12.8 42 140.6 19.8 92 190,1 26.7 42 239.7 33.7 92 289.2 40 43 42.6 06.0 93 92.1 12.9 43 141.6 19.9 93 191,1 26.9 43 240.6 33.8 93 290.2 40 44 43.6 06.1 94 93.1 13.1 44 142.6 20.0 94 192,1 27,0 44 241.6 34.0 94 291.1 40 45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193,1 27,1 45 242.6 34.1 95 292.1 41 47 46.5 06.5 97 96.1 13.5 47 145.6 20.5 97 195,1 27,4 47 244.6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27.7 49 246.6 34.7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41	_	_	04.9	-	-	-	-	133.7	-			25.8	-		32,7	-		39.
38 37.6 05.3 88 87.1 12.2 38 136.7 19.2 88 186.2 26.2 38 235.7 33.1 88 285.2 40 39.6 05.6 90 89.1 12.4 39 137.7 19.3 89 187.2 26.3 39 236.7 33.3 89 286.2 40 40 39.6 05.6 90 89.1 12.5 40 138.6 19.5 90 188.2 26.4 40 237.7 33.4 90 287.2 40 41 40.6 05.7 91 90.1 12.7 141 139.6 19.6 191 189.1 26.6 241 238.7 33.5 291 288.2 40 42 41.6 05.8 92 91.1 12.8 42 140.6 19.8 92 190.1 26.7 42 239.7 33.7 92 289.2 40 43 42.6 06.0 93 92.1 12.9 43 141.6 19.9 93 191.1 26.9 43 240.6 33.8 93 290.2 40 44 43.6 06.1 94 93.1 13.1 44 142.6 20.0 94 192.1 27.0 44 241.6 34.0 94 291.1 40 45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193.1 27.1 45 242.6 34.1 95 292.1 41 46.5 06.5 97 96.1 13.4 146 144.6 20.3 196 194.1 27.3 246 243.6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196.1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197.1 27.7 49 246.6 34.7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297.1 41	3													22.1	2	C. C	3	39.
39 38.6 05.4 89 88,1 12.4 39 137.7 19,3 89 187,2 26.3 39 236,7 33.3 89 286.2 40 39.6 05.6 90 89.1 12.5 40 138.6 19.5 90 188,2 26,4 40 237,7 33.4 90 287.2 40 41 40.6 05.7 91 90.1 12.7 141 139.6 19,6 191 189,1 26,6 241 238.7 33.5 291 288.2 40 42 41.6 05.8 92 91.1 12,8 42 140.6 19,8 92 190,1 26,7 42 239.7 33.7 92 289.2 40 43 42.6 06.0 93 92.1 12.9 43 141.6 19.9 93 191,1 26,9 43 240.6 33.8 93 290.2 40 44 43.6 06.1 94 93.1 13.1 44 142.6 20,0 94 192,1 27,0 44 241.6 34.0 94 291.1 40 45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193,1 27,1 45 242.6 34.1 95 292.1 41 47 46.5 06.5 97 96.1 13.5 47 145.6 20.2 95 193,1 27,1 45 242.6 34.1 95 292.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27.7 49 246.6 34.7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41	37	36.6	05.2	87	00.2	12.1							37			87	284 2	40,
40 39.6 05.6 90 89.1 12.5 40 138.6 19.5 90 188,2 26,4 40 237,7 33.4 90 287.2 40 41 40.6 05.7 91 90.1 12.7 141 139.6 19,6 191 189,1 26,6 241 238.7 33.5 291 288.2 40 42 41.6 05.8 92 91.1 12,8 42 140.6 19,8 92 190,1 26,7 42 239.7 33.7 92 289.2 40 43 42.6 06.0 93 92.1 12.9 43 141.6 19.9 93 191,1 26,9 43 240.6 33.8 93 290.2 40 44 43.6 06.1 94 93.1 13.1 44 142.6 20,0 94 192,1 27,0 44 241.6 34.0 94 291.1 40 45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193,1 27,1 45 242.6 34.1 95 292.1 41 46 45.6 06.4 96 95 1 13.4 146 144.6 20.3 196 194,1 27,3 246 243.6 34.2 296 293.1 41 47 46.5 06.5 97 96.1 13.5 47 145.6 20.5 97 195,1 27,4 47 244,6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27.7 49 246.6 34.7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41			05.3	80														40,
41 40.6 05.7 91 90.1 12.7 141 139.6 19.6 191 189.1 26.6 241 238.7 33.5 291 288.2 40 42 41.6 05.8 92 91.1 12.8 42 140.6 19.8 92 190.1 26.7 42 239.7 33.7 92 289.2 40 43 42.6 06.0 93 92.1 12.9 43 141.6 19.9 93 191.1 26.9 43 240.6 33.8 93 290.2 40 44 43.6 06.1 94 93.1 13.1 44 142.6 20.0 94 192.1 27.0 44 241.6 34.0 94 291.1 40 45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193.1 27.1 45 242.6 34.1 95 292.1 41 46 45.6 06.4 96 95 1 13.4 146 144.6 20.3 196 194.1 27.3 246 243.6 34.2 296 293.1 41 47 46.5 06.5 97 96.1 13.5 47 145.6 20.5 97 195.1 27.4 47 244.6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196.1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197.1 27.7 49 246.6 34.7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297.1 41		20.6	05.6	100	80.1	12.4	1 40	128.6	19,3	00	188.2	26.4						
42 41.6 05.8 92 91.1 12,8 42 140.6 19,8 92 190,1 26,7 42 239.7 33.7 92 289.2 40 43 42.6 06.0 93 92.1 12.9 43 141.6 19.9 93 191,1 26,9 43 240.6 33.8 93 290.2 40 44 43.6 06.1 94 93.1 13.1 44 142.6 20,0 94 192,1 27,0 44 241.6 34.0 94 291.1 40 45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193,1 27,1 45 242.6 34.1 95 292.1 41 46 45.6 06.4 96 95 1 13.4 146 144.6 20.3 196 194,1 27,3 246 243.6 34.2 296 293.1 41 47 46.5 06.5 97 96.1 13.5 47 145.6 20.5 97 195,1 27,4 47 244,6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27.7 49 246.6 34.7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41		_			20 20 12 20		_						-					
43 42.6 06.0 93 92.1 12.9 43 141.6 19.9 93 191,1 26,9 43 240.6 33.8 93 290.2 40 44 43.6 06.1 94 93.1 13.1 44 142.6 20,0 94 192,1 27,0 .44 241.6 34.0 94 291.1 40 45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193,1 27,1 45 242.6 34.1 95 292.1 41 46 45.6 06.4 96 95 1 13.4 146 144.6 20.3 196 194,1 27,3 246 243.6 34,2 296 293.1 41 47 46.5 06.5 97 96.1 13.5 47 145.6 20.5 97 195,1 27,4 47 244,6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27.7 49 246.6 34,7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41							141	139.6					241	238.7	33.5	291	288.2	40,
44 43.6 06.1 94 93.1 13.1 44 142.6 20.0 94 192.1 27.0 .44 241.6 34.0 94 291.1 40 45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193.1 27.1 45 242.6 34.1 95 292.1 41 46.5 06.4 96 95 1 13.4 146 144.6 20.3 196 194.1 27.3 246 243.6 34.2 296 293.1 41 46.5 06.5 97 96.1 13.5 47 145.6 20.5 97 195.1 27.4 47 244.6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196.1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197.1 27.7 49 246.6 34.7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297.1 41		The state of the s										26.0	42	240 6				
45 44.6 06.3 95 94.1 13.2 45 143.6 20.2 95 193,1 27,1 45 242.6 34.1 95 292.1 41 46 45.6 06.4 96 95 1 13.4 146 144.6 20.3 196 194,1 27,3 246 243.6 34,2 296 293.1 41 47 46.5 06.5 97 96.1 13.5 47 145.6 20.5 97 195,1 27,4 47 244,6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27.7 49 246.6 34,7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41							43	142.6	20.0									
46 45.6 06.4 96 95 1 13.4 146 144.6 20.3 196 194,1 27,3 246 243.6 34,2 296 293.1 41 46.5 06.5 97 96.1 13.5 47 145.6 20.5 97 195,1 27,4 47 244,6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27.6 48 245.6 34.5 98 295.1 41 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27.7 49 246.6 34,7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41			06.2				45	143.6	20.2					242.6				
47 46.5 06.5 97 96.1 13.5 47 145.6 20.5 97 195,1 27,4 47 244,6 34.4 97 294.1 41 48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27.6 48 245.6 34.5 98 295.1 41 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27.7 49 246.6 34.7 99 296.1 41 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41						No. of Lots	_					-	The same of			-	the Contract of the	
48 47.5 06.7 98 97.0 13.6 48 146.6 20.6 98 196,1 27.6 48 245.6 34.5 98 295.1 41 49 48.5 06.8 99 98.0 13.8 49 147.6 20.7 99 197,1 27.7 49 246.6 34,7 99 296.1 41 50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41	40	46.5	06.5	07	95 1				20.5									
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50 49.5 07.0 100 99.0 13.9 150 148.5 20.9 200 198.1 27.8 250 247.6 34.8 300 297,1 41	40	48.5	06.8		98.0	13.8				99	197,1		49	246.6				41,
Dift Dep Lat		49.5	07.0		100 Sept 100		150	148.5		200	198.1	27.8	250	247.6				41.
mp it and a land				-		Lat	Dif	Den										Lat
		Poch			- cPi			P			- r			- vp			cp	Da

]	Diff	ere	nce	of 1	Lat	itud	le ar	nd !	Dep	artu	re	for c	De De	g.		9
Dift	Lat	Dep	Dift	Lat	Dep	oill	Lat		Dift	Lat	Dep	Diff	Lat	Dep	Ditt	Lat	nep
1	01.0		51	50.4	08.0	101	99 8	15.8	151	149.1	23,6	201	198.5	31.4	251	247.9	39.3
2	02.0	THE RESERVE AND ADDRESS OF THE PARTY.	STATE OF THE PARTY OF	51.4	08.1		100.7	16,0	BECKE STREET	150,1	23,8	02	199,5	31,6	52	248.9	39,4
3	03.0			52.3	08.4	03	101.7	16.1	53	THE RESERVE AND ADDRESS OF THE PARTY OF THE	23.9	No. of Contract of	200,5	31.7	53		39.6
4	04.9		55	54 3	08.6	05	103.7	16.4	54	152,1	24.1	THE RESIDENCE OF THE PERSON NAMED IN	201,5	31.9	54	251.9	39.7
-6	05 9		56	55-3	08.8	106	104.7	16.6		154,1	24.4		203,5	32.2	55 256	_	40.0
7	06.9	Part of the Part o	57	56.3	08.9	07	105.7	16,7	57	155,1	24.6		204,5	32,4	The second second	252.9	40.2
	07.9	01.3		57.3	09.1	08	106.7	16,9		156,1	24.7	1000 V	205,4	32.5		254.8	40.4
9	08.9	01.4	59	58.3	09.2	09	107.7	17.0	59	157,0	24,9	09	206.4	32.7	59	255.8	40.5
10	09.9	01.0	65	59.3	09.4	10	108.6	17.2	60	158,0	250	10	207,4	32.8	60	256.8	40 7
11	10.9	01.9	61	61.2	09.5	III	109.6	17.4	161	159,0	25.2		208,4	33,0		257.8	40.8
12	-	02.0	345.037.15	62 2	09.7	12	110.6	17.5	62	160,0	25.3	1 1 20	209,4	33.2	1000	258.8	41,0
14	20. 10. 10. 10. 1	02.2		63.2	10.0	14	112.6	17.8	64	162,0	25,6	13	211,4	33.3		259.8	41.1
15	14.8	02.3		64.2	10.2	15	113.6	18.0	65		25.8	15	212,4	33.6	65	261.7	41.4
16		02.5	66	65,2	10.3	116	114.6	18.1	66	164.0	26.0	216	213,3	33,8		262.7	41.6
17		02,7		66.2	10.5	17	115.6	18.3	67	164,9	26.1	17	214,3	33.9		263.7	41,8
18	1 2 2	2,8		67.2	10.6	A Charles	116.5	18.5	68	300	26.3	18	215,3	34.1		264.7	41,9
19	Programme and the second	03.0		68.2 69.1	10.8		117.5	18,6	69		26.4	19	216,3	34.3	69	265,7	42,1
20	-		-			-			70		26.6	-	217,3	34.4	-	266.7	42,2
21	20.7	03.3	71 72	70.I	11.1	121	119.5	18,9	171	168,9	26 7	221	218,3	34.6	100	267.7	42.4
23		03.6		72.1	11.4	23	121.5	19.2	72 73	170,9	26.9	22	219,3	34.7		268.7	42 5
24		038	10 3 4 7 1	73.1	11.6	24	122,5	19.4	74	171,9	27.2	24	121,2	35,0		270.6	42.9
25	247	03.9	75	74 1	11.7	25	123 5	19,6	75	172,8	27.4	25	222,2	35.2	75	271,6	43.0
26	1 -	04.1		75.1	11.9	126	124,5	19.7		173,8	27.5	226	223.2	35,3	276	272.6	43.2
27		04.2	1 0	76.1	12.0	27	125.4	19,9		174,8	27.7	27	224.2	35.5	5 St. 18 St. 18		43.3
1	27.7	A CONTRACTOR OF THE PARTY OF TH	1000	77.0	12.2	28	126.4	20.0	Section 1.	175,8	27.8	1000	225.2	35,7		274,6	43.5
30		04.7	79 80	79.0	12.5	30	127.4	20.3	79 80	CONTRACTOR OF THE PARTY OF THE	28,0		226,2	35.8		275.6	43.6
31			81	80.0	12.7		129.4	20.5	181	178,8	28.3		227.2	36,1	-	276.6	
32	1 .	College Charles	82	81.0	August 1987 The State of the St	THE REAL PROPERTY.	130.4	20.6	82	A STATE OF THE PARTY OF THE PAR	28.5		229,1	36.3		277 5	43,9
33	32.6	05.2	83	82.0	13.0	1 Table	131.4	20.8	83		28.6		230.1	36,4		279,5	
34	33.6	05.3	84	83.0	13 1	3.4	132.4	21.0	84	181,7	28.8		231.1	36,6	84	280.5	44,4
-	-	05.5	-	84.0		-	133.3			182,7	28,9	35	232.1	36,8	85	281,5	44.6
36	35.6	05.6	86	84.9	13.5		134-3	21.3	186	183,7		236	233,1			282.5	
37	36.5 37.5	05.8	87	85,9	13.6	37	135.3	21.4	87	184,7	29.2	37	234.1	37,1	87	283.5	
39	38.5	06.1	89	87.9	13.9		136.3	21,6	80	186,7	29.4	38	235.1			284 5	The second second second
40	39.5	06.3	90	88,9	14.1	40	138.3	21.9	90	^	29 7	39 40	237,0	37,4		285.4	
41		06.4	91	89.9	14.2	141	139.3	22.1	191		29,9		238.0		-	287.4	-
42	41.5	06.6	12 6 20 7 1 1 1	90.9	14.4	42	140.3	22.2	92	189,6	30.0	42	239.0	37.8	02	288.4	45.5
43	42.5	06.7		91.9	14.5	43	141.2		93	190,6	30.2		240.0	38,0	93	289.4	45.8
	43.5	06.9		92.8	14.7	THE RESIDENCE	142.2			191,6	Contract Visit Vis	44	241.0	38,2	94	290 4	46,0
45	CONTRACTOR OF THE PERSON NAMED IN	07.0	95	93.8	100 miles	45	143.2	22.7	95	192,6	30 5	45	242.0	38,3			
	45.4		96	94.8	15.0		144.2	22.8				246	243.0				46,3
	46.4		97	95 8 96.8	15.2		145.2	23.0	97	194,6			244,0			293.3	
	48.4		99	97.8	15.5	49	147.2	23.3	99			18 TO	244.9				
	49.4		100	98.8	15.6	150	148.2	23.5	200		Service Control of the Control of th		246.9			THE RESIDENCE OF SHAPE	46,9
Dift	Dep	Lat	Dift	Dep	Lat		Dep	Lat	Dift		Lat	Diff	-	Lat		t fep	Lat

for 81 Deg

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	-	Dep	-	Lat	Dep	Diff	-	Dep	Diff	The state of the state of	Dep	Diff	Lat	Dep	Diff	Lat	vep
V- 141 V	010000000000000000000000000000000000000	00.2	53	50.2	08.8	101	99.5	17,5	0.000			201	197.9	34,9	THE RESERVE OF THE PERSON NAMED IN	247.2	43.5
.2		20,3	52	51.:	09.0	02	100.4	17.7	52	101511000115100		02	198.9	35,0	52	248.2	43.7
3		00.5	53	52.2	09.2	03	101.4	17.9	53		26.5	20000000	199,9	35.2	COLUMN TO	249.2	43,9
4	2000	00.7	54	53.2	09.4	04	102.4	18.2	54	151,7	26.7	04	200,9	35,4	54	The second second	44.0
		-	55	54.2	09.5	05	103.4		55		26.9	05	201,9	35.5	55	251.1	44.7
6	25 9	X 2/2 2 8 8	56	55.1	09.7	106	104.4	18.4	156		27.1	206	202,9	35.7	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	252.1	44,
7	St. Committee	31.2	57	56.1	09.9	08	105.4	18,7	57	154,6	27.2	07	203,9	35.9	57	253 1	44.
100		01.4	59	57.1	10.1	09	107.3	18,9	A CONTRACTOR	155,6	27.4	08		36.1		254.1	44.
9	39.8	The state of the s	60	59.1	10.4	10	108.3	19,1	59 60	CAMBRIDGE AND COMPANY	27.6	10	205,8	36,2 36.4		255.1	44.
-	-		61	60,1	10.6	-			161			-	-			256.0	45,
11	10.8	22.1	62	61.1	10.8	111	109.3	19,2	62	158,6	27.9	211	207,8	36,6	62	257.0	450
12	12.8	32.3	63	62 0		13	111.3	19.6	63	23.2	28.3	-	209,8	36,3		258.0	45.4
14			64	63.0	11.1	14	112.3	19,8	64	161,5	28.4	14	210,7	36,9		259.0	45.8
15	14.8	32.6	65	64.c	11.2	15	113.3	19.9	65	162,5	28.6	15	211,7	37,1		261.0	46,0
10	15.8	12,8	66	65,0	11.4	116	114.2	20.1	66	-	28,8	216	212,7		-		-
17	16.7	32,9	67	660	11.6	17	1152	20.3	67	164.5	29.0	17	213,7	37,5	67	262.0	46,
18		23.1	68	67.0	11.8	1	116.2	20.5	68		29.1	18	214,7	37.6 37.8	68	263.9	46,
19	-	33.3	69	63.c	12.0	19	117.2	20.6	69		29.3	19	215,7	38,0		264.9	46,
20	19.7	03.5	70	58.9	12.1	20	118.2	20.8	70	167,4	29.5	20	216,7	38,1	70	265,9	46,8
21	20.7	23.6	71	69.9	12.3	121	119.2	21.0	171	168,4	29 7	221	217,6	38,3	-	266.9	
		2 3 2 2 3	72	70.9	12.5	12	120.1	21.2	72	169,4	29,8	22	218,6	38,5	ETC - AM SECURE	267.9	47,0
100	100	24,0	73	71.9	12.7	23	121.1	21.3	73	C - 20 - 12 - 12 - 12	30.0	23		38,7		268.8	47.3
	23.6	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	74	72.9	12.8	24	122,1	21.5	74	171,4	30.2	24	220,6	38.8		269.8	47.
	24 6	CONTROL OF THE STATE OF	75	73.9	13.0	2.5	123 1	21,7	75	172,3	30.3	25	221,6	39.0		270.8	47.
	25.6	04.4	76	74.8	13.2	126	124,1	21.8	176	173,3	30 5	226	222,6	39.2	-	271,8	
2000	-	04.7	77	75.8	13,4	27	125.1	22.0	77	174,3	30.7	27	223.5	39,4		272.8	47.9
- 1	27.6	B. C. W. S. W. B.	78	76.8	13.5	28	126.1	22.2	78	175,3	30,9		224.5	39.5		273.8	48.2
29	28.6	05.0	79	77.8	13.7	29	127.0	22 4	79	176,3	31.0		225-5	39.7		274,8	48.4
30	29.5	05.2	So	78.8	13.9	30	128 C	22.5	80	177.3	31.2	145	226,5.	39.9		275.7	48.6
31	30.5	05.4	81	79.8	14.0	131	129.0	22.7	181	173,2	31.4	-	227 5	40.1	-	276.7	48.
1.0	10 1 1 V	05.5	82	80.8	14.2	32	130.0	22.9	82	179,2	31,6	32	228,5	4 .2	F (12.2)	277 7	48.9
	32.5	05.7	83	81.7	14.4	33	131.c	23 1	83		31.7	33	229,5	40.4	Br 6 2075	278.7	49,1
34	33.5	05.9	84	82.7	14.6	34	132.0	23.2	84	181,2	31.9	34	230.4	40.6		279,7	49.2
35	34,5	06.1	85	83.7	14.7	35	132.9	23.4	85	182,2	31.1	35	231.4	40.7		280.7	49.4
36	35.5	06.2	86	84.7	14.9		133.9	23,6	186	183,2	32.3	236	234.4	40.9	286	281,6	49.6
37	36.4	06.4	87	85,7	15.1		134.9	23,8	87	184,2		37	233,4	41,1	87	282.6	49,8
381	37.4	06.6	88	86.7	15.3	38	135.9	23.9	88	185,1	32.6	38	234.4	41.3	88	283.6	59.5
39	38.4	06.8		87.6	154		136.9	24.1		186,1	32.8	39	235.4	41.4	89	284.6	50.1
40	39.4	06.9		88,6	15.6		137.9	24 3	90	187,1	32.9	40	236,3	41.6	90	285.6	50.3
	10.4			89.6	15.8	141	138.9	24.4	191	188,1	33,1	241	237,3	41,8	291	286.6	50.
42 4	11.4		92	90.6	16,0	42	139.8	24.6		189,1	33.3	42	238.3	42,0	92	287.6	50.6
	12.3			91.6	16.1	43	140.8	24.8	93	190,1	33.5		239.3	42,1	93	288.5	50.8
44 4	13.3	07.6		92.6	16.3	Contract Contract	141.8	25.0	94	191,0	33.6		240.3	42.3	94	289.5	51,0
	14.3		Bearing St.	93.6	16.5	-	142.8	25,1	95	192,0	33.8	45	241.3	42,5	95	290.5	51.2
46 4	15.3	08.0		94.5	16,6	146	143.8	25.3	196	193,0	34,0		242.3	42.7	296	291.5	51.3
47	16.3	08.1		95 5	16,8	47	144.8	25.5	97	194,0	34.2	47	243.2	42.8	97	292.5	51.
48	17.3	08.3	98	96.5	17.0		145.7	25,7	98	195,0	34.3		244,2	43.0	98	293.5	51.7
49 4	18.3	08.5	99	97.5	17.2		146.7	25,8	99	196,0	34.5	49	245.2	43.2	99	294.5	51.8
The second second	10.21	08.7	100	98.5	17.3	r50	147.7	26.0	200	197,0	34.7	250	246.2	43.4	300	295.4	52.0
	Dep		_	Dep	Lat	Dift		Lat	Dift	Dep	Lat		Dep			Dep	3

Difference	f I atitude and	Departure for	te Dec
Difference o	I Latitude and	Departure 101	II DEE.

Dift Lat

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Dep

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)e	g.	1	1	
ep	Diff	Lat	Dep	
.4	251	246.4	47.9	
,5	52	247.4	48.1	
.7		248.3	48.3	
.9		249.3	48.5	
.1	55	250.3	48 7	
1.3	256	251.3	48.8	
1.5		252.3	49.0	
1.7	58	253.2	49.2	

01.0 19.3 148.2 28.8 0.2 197.3 50.1 09.7 101 99.1 201 02.0 51:0 09.9 19.5 00.4 ICO.I 149.2 29.0 02 198.3 02.9 00.6 53 150.2 52.0 10.1 03 101.1 29 2 03 199.3 19,7 53 03.9 00.8 19.8 54 151,2 102.1 04 200.2 54 53.0 10.3 29.4 152.1 29.6 04,9 01.0 54.0 10.5 103.1 05 201.2 20.0 55 05 05.9 01.1 153.1 29.8 206 202.2 56 55.0 10.7 106 104.0 156 20.2 39 06.9 01.3 203.2 105.0 56.0 10.9 154.1 30.0 07 20.4 57 07 57 39 01.5 07.9 08 106.0 20.6 155.1 30.1 08 204.2 8 56,9 11.1 156.1 08.8 01.7 09 107.0 20.8 30.3 09 205.2 11,3 39.9 40:0 09.8 31.9 6c 58.5 108.0 157.1 30.5 10 206.1 60 255.2 49.6 11.4 21.0 10 10.8 207.1 40.3 256.2 32.1 59.9 11.6 109.0 161 158:0 261 61 111 21.2 30.7 211 49.8 II 11.8 60.9 40.4 02.3 11.8 109.9 214 12 208.1 62 62 159.0 30.9 62 257 2 12 50,0 12.8 63 63 209.1 50.2 02.5 61.8 110.9 21.6 160.0 31,1 40.6 258.2 12.0 63 13 13 13 02.7 64 161.0 14 210.1 40,8 13.7 62.8 111 9 21,8 64 50.4 12,2 14 31.3 64 259.1 02,9 112.9 50.6 14.7 63.8 15 65 162.0 211.0 41.0 260.1 12.4 21.9 31.5 15 15 162 9 166 157 03.1 64.8 12.6 116 113.9 22.1 31.7 216 212.0 41.2 266 261.1 50,1 16 65.8 16.7 41.6 33.2 12.8 17 114.8 22.3 163.9 31.9 17 213.0 67 262.1 50.0 17 68 164.9 03.4 66.7 13,0 22.5 51.1 17.7 18 115.8 32.1 18 214'0 68 263.1 19 116.8 165.9 18.7 41.8 03.6 69 67.7 13.2 22.7 69 32.2 19 215.0 69 264.0 51.3 19 68.7 13,4 19.6 03.8 166.9 20 215.9 20 117.8 32.4 70 265.0 51.0 70 22,9 70 42,0 20 20.6 04.0 121 118.8 216.9 167.9 271 266.0 69.7 13.5 23.I 171 32.6 221 42.2 21 71 51.7 72 168.8 21.6 04.2 32.8 119.8 72 267.0 70,7 13.7 22 23,3 22 217 9 42.4 51.9 22 73 268.0 22.6 04.4 23 218.9 71.7 169.8 120.7 23 73 13,9 23 23,5 73 33.0 42.5 52.1 23.6 04.6 170.8 74 269.9 14.1 24 121.7 23.7 74 33.2 24 219.9 42.7 52.3 24 74 04,8 73.6 14.3 171.8 44.5 23.9 269.9 25 122.7 75 33.4 25 220.9 42.9 52. 25 75 75 05.0 76 74.6 172.8 25.5 123.7 176 33.6 226 221.8 14.5 126 43.1 276 270.9 26 24.0 52.7 75.6 14.7 76.6 14.9 26.5 05.2 33.8 27 222.8 28 223.8 173.7 77 271,9 77 78 124.7 43.3 27 28 27 24,2 77 52.9 78 05.3 28 125.6 27.5 174.7 34'0 43.5 24.4 53.0 28,5 05.5 79 77·5 80 78.5 29 126.6 24.6 79 29 224.8 175.7 79 273.9 34.2 15.1 43.7 29 53.2 24.8 176.7 30 225.8 80 29.4 05.7 127.6 274.8 15.3 34.3 43,9 30 30 53,4 281 275, 226.7 30.4 128.6 05.9 81 79.5 15,5 131 250 181 177.7 34.5 231 44.1 53.6 31 82 178.6 c6.1 82 80.5 15.6 129.6 25.2 32 227.7 82 276,8 34.7 44-3 32 32 53. 06.3 33 228.7 32.4 83 81.5 15.8 130.6 83 179.6 83 277,8 34 9 33 25,4 44.5 33 54,C 06.5 84 180.6 84 82.5 16.C 34 229.7 44.6 33.4 131.5 25.6 84 278.8 35.1 34 54,2 34 06.7 85 181.6 83.4 16.2 85 279.8 34.4 1 32.5 25.8 35.3 35 230.7 44.8 35 54.4 35 236 231.7 186 182.6 84.4 16.4 06.9 35.3 86 136 286 280.7 133.5 25.9 35.5 45.0 36 54,6 183.6 37 38 281.7 36.3 07.1 85.4 16.6 26.1 232.6 45,2 134.5 35.7 54.8 37 37 88 184.5 26.3 38 37.3 86.4 16.8 07.3 88 38 35.9 233.6 88 282.7 135.5 45,4 55.0 38.3 185.5 87.4 26.5 89 283.7 36.1 07.4 89 17.0 136.4 89 39 234.6 39 45.6 39 45.1 186.5 88.3 07.6 36.3 40 90 284.7 39.3 17,2 26.7 90 235.6 45.8 90 40 137,4 40 55.3 89.3 241 236,6 17.4 138.4 187.5 46.0 40.2 07.8 26.9 191 36.4 291 285.6 141 91 41 55.5 08.0 92 188.5 36.6 46.2 11,2 17.6 42 42 237.5 92 286,6 139.4 27.1 92 55.7 08.2 42.2 189.4 43 238.5 91.3 17.7 36.8 46.4 93 287.6 140.4 27.3 93 93 43 43 55,9 08,4 43.2 46.6 94 288.6 92.3 17.9 141.3 27.5 94 190.4 44 239.5 37.0 56,1 08.6 93.3 18.1 46.7 142.3 191.4 95 289.6 27,7 95 37.2 45 240.5 56.3 45 45 08,8 94.2 18.3 143.3 196 246 241.5 290.5 46 45.2 146 27.9 192.4 37.4 47.0 296 56.5 18.5 46.1 09:0 28,0 37 6 95.2 18.5 47 97 98 47 48 193.4 242.5 97 98 56.7 47 144,3 47.I 291.5 145.3 194.4 09.2 28.2 37.8 243.4 292.5 47,3 56.9 38.0 97.2 18.9 09.3 28.4 195:3 99 49 99 49 244,4 293.5 49 47.5 99 57.C 98.2 19.1 28.6 38,2 49.1 09.5 100 147.2 200 196.3 250 245.4 150 47.7 300 294.5 57.2 Dift Lat Dep Lat Dift Dep. Lat Dift Dep Lat Dep Lat

for 79 Deg

Difference of Latitude and Departure for 12 Deg.

			A Sale															374
Ditt	Lat	Dep	Din	Lat.	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	
1	01.0		-	_	10.6		98.8	21.0	151	147.7	31.4	201	196.6	41.8	251	245.5	52.2	
2	02 0		52		10.8	02	99.8	21.2	52	148.7	31.6	02	197.6	42,0			52 4	
3	1 2 7 6 7	00.6	53		11.0	2 10 10 10 10	100.7	21.4	53	149.6	31.8	03		42.2	1000	247.4	52.6	
4	03.9	19 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	THE RESERVE OF THE PERSON NAMED IN	52.8		04	101.7	21.6	THE RESERVE OF THE PERSON NAMED IN	150.6	32.0	04	199.5	42.4	1/10/23/1950	248.4	52,8	
	04,9	13 27 0 1 1 1 V	54	53.8		05	102.	21,8		151,6	32.2	05	200.5	42.6	A COLUMN TWO	249.4		
5	-		55		The second second	-			55					-	55		53.0	
6		Service Control of the Control	56	54.2	11.6	106		22.0		152.6	32.4	THE REAL PROPERTY.	201.5	42.8	256	250.4	53.2	
7	06.8	01 5	57	55.7	11.9	07	104.6	22.3	57	153.5	32.7	07	202.4	43.1	57	251.3	53.5	
8	27.8	017	58	56,7		08	105.6	22.5	58	154.5	32.9	08	203.4	43.3	1 58	252.3	53,7	
9	08.8	01.9	59	57.7	12,3	09	106.6	22.7	59	155 5	33.1	09	204.4	43.5	59	253.3	53.9	-
10	09.8	02.1	60	58.7	12.5	10	107.6	27,9	6c	156.5	33.3	10	205.4	43.7	60	254.3	54,1	
11	10.8	02:3	61	59.7	12 7	111	108.6	23.1	161	157.5	33.5	211	206.4	43,9	261	255.3	54,3	
12	11.7	02.5	62	60.6	12.9	12	109.5	23,3	62	158.4	33.7	12	207.3	44.1	62	256.2	54.5	
13	12.7	02.7	63	61.6	13,1	13	110.5	23,5	63	159.4	33.9	13	208.3	44.3	- 1	257.2		1
14	13.7	02,9	64	52.6	13.3	14	111 0	23.7	64	160.4	34'1	14	209.3	44.5	64	258.2	54.9	
15	14.7	3.1	60	63.6		15	112.5	23.9	6:	161.4	34.3	15	1	44.7	6:	259.2	55.1	ı
	15 6		66	64.	-		112.6	24.1	166	162.3	34.5	216			266	-		1
16	16.6	1 3 3	67		13.7	116	113.4		67	163.3		2		44.9		260.1	45.3	
17		1 3 3	68	1 10 10		17	114.4	24,3	68		34.7	17	212.2	45.1	67	261.1	55.5	
13	17.6	THE RESERVE AND ADDRESS.						24.5	E		34 9	£		45,3	The state of the s	A COLOR STORY	55,7	
19	19.6	ALEX SERVICES	69	114 4		10	116.4	24.8	69	166.3	35.2	19	214'2	45,6		1 .		
20		-	70	-	-	20	117-4	250	70		35.4	30	-	45.8		264.1		
21	20.5	04.4	71	69.4	14.8	121	118.3	2512	171	167.2	35 6	221	216.1	46 0		265	56.4	
22	21.5		72	70,4	115.0	22	119.3	25,4	72	168 2	35.8	22	Control of the second	46.2		266.0		
23	22.5	04,8	73	71.4	15.2	23	120.	25.6	73	169.2	36.0	23	218.1	46.4	73	267.0	56 8	1
24	23.5	05.0	74	72.4	15,4	24	121.3	25.8	74	170.2	36.2	24	219.1	46.6	74	268.0	57.0	
25	24.5	05.2	75	73.4	1 5.6	25	122.3	260	75	171.2	36.4	25	120.1	46.8	75	269:0		
26	25.4	05.4	76	74.	15.8	126	123.2	26.2	176	172.1	36.6	226	221.0	47.0	276	-	-	18
	26.4		77	THE RESERVE OF THE PERSON NAMED IN		-27	124.2	26.4	77	173.1	36.8			1		270.0	31.	
27	27.4	1 0	78		16.2	28	125.2	26.6	78	174.1	37.0			3 4 5				
4 50 4	28,4		79	A 500 CO.			126.2	26.8	79	175.1	37.2					A CONTRACTOR		
29	29		80				127.1	27.0	80			1.10						
30	-		-	.	-	3	-	-		-	-		-	-		-/3	-	400
31	30.3		81		X	3	128.1	27.2	181	177.0		10.00				1 / 1		
32	31.3		82	Contract of the second	The second of	32	129.1	27.5	82		37.9	32				1 37		
33	32.3	1. 1. 1. 1. 1. 1.	83				130.1	27,7	83			100				276,	58.)
34	33.3		84				131.1		84	0		514 6-40 54-71		48.7		1 11		1
35	34.2	2 07.3	8 9	83.	1 17.7	35	132.0		85	180.0	1 3 3		229.8	48.9	85	278.	7 59,	3
36		2 07.5	86	84	1 17.9	136	133.0	28.3	186			236	230.8	49.1	286	279.	7 50.	20
37	1.6.	2 07.7	1 8	85.	1 18.0	37		28.5	87	182.9	38.9	37	231.8	49.	8 87	280.	7 59,	
38	100 May 140 May 179	2 07.9	88	8 86.	1 18.3	38	135.0	28.7	88	183.9	39.1		3 232.8	49,	88	281.	7 59.	
39	1.0	1 38.1	0	10-	-1.8				1 80	184.8	39.3		233.7			282.	6 60.	
	100	1 0	0	88.	0 18.	40					39.5		234.7			283.	6 60.	
41	1	-	-	180	0 18	74	107	تتحددهما أ	_	THE PERSON NAMED IN			235.7	-	-			-
41	40.	1 08.7	9	100	c 19.	141	137,9			187.8			2 2 3 6, 7			284.	6 60.	5
42	7 (2 8 8 8 8 8	108	9	90.	019.	42							3 237.7				6 60,	7
43	100	1 08,0	9	3 91.	9 19,	43	139.9		93	189.7		1 4	4 238.6	50.	9.	286,	6 60.	9
44	AND RESIDENCE	0 09.2	9	5 02	0110	44	140.8	30.2							0 0	4 287.		
45		0 09.4		3 92.	9 19.	4			-	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN			5 239.0					4
46	45.	0 09.6	9	6 93.	9 20.	14		30 4	1196	191.7	40,8	24	6 240.6					6
47	146.	0 09.8	9	7 94	9 20.	2 4	143.		97	192.7	41.0	4	7 241.6		4 9	7 290.	5 61.	8
48	3 46.	9 10.0	9	8 95	20.	4 4							8 242.		6 9		4 62.	0
49	47,	9 10.2	9	9 96	\$ 20.	6 4	9 145.	7 31,0		194.6			9 243.	51.	8 9		4 62.	2
50	1 0	9 10.	4 10	0 97	\$ 20. \$ 20. \$ 20.	8 150		7 31.2	100	195.6	41 6	25	0 244,	5 52	0 30			4
1=							Dep	The Real Property lies, the least	10:	ft Dep	Lat	Di	ft Lat	Lat				
Di	ItiDe	PLat	ועו	שעווו	p Lat	וועו	il Deb	Lat	Pi	in Dep	Lat	ID.	III Tal	Lat	וחו	ft De	o Lat	9
U. Carrie	100																100	100

for 78 Deg.

									12	2:0	Y	1 1		Sal	T ot	Dan	200	Lat	Dep
DittyL	at	Dep	Ditt	Lat	14	ep	Dift .	Lat	Dep	Dit	Lat	L	ep 1		Lat	-	Dift	Lat	-
	-	00.2	51	49.		1.5	101	98,4	22,7		147.	1 3	40		95.9	45,2	251	244.6	56.5
Control of the last	100000	00.4	52	50,		1,7	02	99,4	22,9	52	148.	1 3	4,2		196,8	45.4	52	245,5	56,7
March 1999	Marie Co.	00.7	53	51,	6 1	1.9	31	100.4	23.2		149,		4 4	03	197.8	45,7	53	246,5	56.9
4 03	3,9	00.9	54	52.	6 1	2.1		101.3	23,4	STATE OF THE PARTY OF	150.	5 (4) (4) (6)	34,6	13/10/10/10	198.8	45,9	54	247.5	57,1
50	4.9	01.1	55	53.		2.4	05	102.3	23,6	55	151,	0	34 9	05	199.7	46.1	55	248.5	57.4
60	5,8	01.3	56	54,	6 1	2,6	106	103.3	23.8	156	152.	0 :	35.1	206	200.7	46.3	256	249 4	57.6
700	6,8	01.6	57	55.	5 1	28	07	104.3	24 1	57	153	0	35,3	0/	201.7	46.6	57	250,4	57.8
	7,8	8.10	58		5 1	3.0	08	105,2	24.3	58	154.		35.5	00	202.7	46.8	58	251.4	58.0 58.3
	3,8	02,0	59	57,	40.5	3,3	09	106.2	24.5	59	154	9	35.8		203.6	47,0	59	252.4	58.5
100	9,7	02.2	60	158	5 1	3,5	10	107.2	24,7	60	155		36,0		204.6	47.2	60	253.3	
11 11	0,7	02.5	61	59		3.7	111	108,2	250	161	156	,9	36.2		205.6	47.5	100000000000000000000000000000000000000	254,3	58.7
12 1	1.7	02.7	62		40.00	3 9	12	109.1	252	62		,9	36.4		200.6	47.7	62	255,3	58.0
13 1	2.7	02.9	63		1.3	4.2	13	110,1	254	63		.8	36,7	13	207.5	47.9		256.3	59.2
	3.6	03.1	64			14.4	14	111,1	25.0	64			36 9	14		48.4	64	257.2	59.4
151	4,6	034	65	53		4.6	15	112,1	25.9	65	-	-	37.1	15	209.5			-	
	5,6	23,6		1. 140		14.8	116	113,0	26.1	166	10.00		37 3	216	210.5	48.6	266	259.2	59.8
17 1	6,1	03,8			,3	15,1	17	114,0	26.3	1 1 1 1 1 1	The second		37.6	17	211.4	The second second		261.1	60.3
W. W. C. C. C. C. C.	1.3	04.0			-	15.3	18	115.0	26.5		-		37.8	18	213.4	49.0	1 7 0.9	1.7	60.5
- 7	8.5	04,	20 11/18/	24.63		15.5	19	116.9	The second of		164		38.2	19	214.4	49,5		1 - 6	60.7
20	9 5	04,	79		- 1	157	20	-	I see the	-	1	-		20	-			264 1	61,0
21 2	20.5	04.		A. A. M. C. C.	,,-	16.0	121	117,9	27,2		2000	C00000	38.5	221	215.3	39.9		1-6-0	61.2
	21.4	04.9).2	16.2	22	118 9		72	167	6	38,7	22	217.3			1.66 -	61.4
-3	22 4			1	.1	16.6	23			100	168		39.1	23	218.3	50.		10600	61.6
1	23,4	1			,1	16,9	24				Service Co.	1000	39,4	24	219.2			106.0	619
	24,4	Contract of		_	3,1		-	-		_	-	-	-	-	220,2	-	-	1 10	
	25,3				4,1	17,1	126	1000000	-0				39 6	226	221.2		1100	1.6	2 2 19 17
	26.				5,0	17.5	. /		0				40,0	27	222.2				1 .
	27.3			200 100	6.0	17,8						27.25	40,3	29	223.1	1	- C - C - C - C - C - C - C - C - C - C		
	29.	1-6			7,0	18,0			Control of the Control of			- 100	40.5	the state of	224,1				63.0
-		-	-		8,9	18.2	-		The second second	-	-	-	40.7		225.1			273,8	
3	30,	and the same of	Section 1. A Visit	6.3	9,9	18.4		0	Children Control of the Control of t	0.19	100	7.3	40 9	CONTRACTOR OF THE PARTY OF THE	226	52.			
-	31,		The second second		0,9	18.7							41.2		227.0	The State of the S			
33	33.	9 5	6 8	4 8		18.9			A 10 50 500	1 8			41.4	33	228.0	52.			63.9
2,1	34,	1			2,8	19.1				4 8	5 18	0.3	41.6	35	229	52,	9 8		-
	35,		-		3,8	19.3	143	-	5 30.	6 18	6 18	1.2	41.8			53.	1 28	6 278.7	64.3
30	26.	1 08.	107313 0.78130	7 3		196	3'	133,		8 8	7 18	2.2	42 1				3 8	279.6	64,6
281	37.	0 08	5 8	8 8	5,7	98	3	8 134,		0 8	818	3.2	42.3		231.	53,	5 8	8 280.6	04.8
39	38,	0 08.	.8 8	39 3	6,7	20.0	3	9 135,	4 31.		9 18	4.2	42.5	39	232.	53		281.6	
40	39.	0 09	.0	0 8	7,7	20.	4		4 31.	5 9	0 18	5.1	42.7	40	233.		0 9	282.	
41		9 09	2 0	1 8	8.7	20.	5 14	1 137	4 31.	7 19	1 18	6.1	43.0	40	234.	8 54	2 29	1 283.	5 65.5
42		909	,4 6	2 3	9,6	20.			4 31.	9 9	2 13	7.1	43,2	42	235.	8 54	4 9	2 284,	3 65.7
43	41.	9 09	,7 9	13 19	10.6	20.	9 4		3 32	2 9	3 18	8.1	43,4	4 4:	236.	8 54	7 9	3 285	5 65.9
44	42,	9 09	.9	94 9	11.6	21.	1 4					9.0		6 44	1 237.	8 54	9 9	4 280,	5 66.1
45	43,	8 10	,1	95 9	12,6	21.	4 4			_	_	0.0	-	9 4	5 238.	7 55	_		4 66.4
46	44.	8 10	,3	96	3,5	21.		6 142			6 19	1.0	440	1 24	6 239.	7 35	3 29		4 66.6
47	45	8 to	.6	97 9	94,5	21.	8 4	7 143	2 33	I	7 39	2,0	44.	3 4	7 240.	7 55	.6 9		4 66.8
48	46	8 10	.8	98	95.5	22.	0 4	8 144	2 33	3 9	8 19	2.9	44.	5 4	8 241.	6 55		8 290.	4 67.0
49	47	7 11	,0	99	96.5	22.	3 4	9 145	.2 33			93.9		8 4	9 242.	50	.0 9	9 291.	3 67.
50	48	6 11	,2 1	00	97.4	22.	5 15	0 146	2 33	7 20	00 1	94,9	45.	0 25	0 243	6 56	.2 30	292	3 67.
		ep L	at C	ifi	Dei	La	t D	ift De	p L	it D	ift I	Dep	La	t Di	ft De	p La	t D	ift De	p Lat
1	1-	PI	TO SERVICE		-1														

14 Difference of Latitude and Departure for 14 Deg.

									1 4 4 1			depletion.					1-11-11
Ditt	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Dilt	Lat	Dep	Dift	Lat	Dep
1	0.10	00.2	51	19.5	12.3	101	98,0	24.4	151	146,5	36,5	201	195.0	-	_		-
2	01,9	00.5	52	50,5	12,6	02	99,0	24.7	52	147.5	36.8	STATE OF THE PARTY	196,0	48.9		243.5	61,0
3	02,9	00.7	53	51,4	12.8	03	99.9	24,9	53	148.5	37.0	Control of the last	197.0	49.1		245,5	61.2
4	03,9	010	54	52.4	13.1	04	100.5	25.2	54	149,4	37.3	04	197.9	49.4		246,4	61.5
5	04.9	01.2	55	53.4	13,3	05	101.9	25.4	55	150.4	37.5	05	198.9	49,6	55	247.4	61.7
6	05,8	01.5	56	54,3	13,6	106	102.8	25.7		151,4	37.6		199.9	49.9	256	248,4	62.0
7	06,8	01.7	57	55.3	138	07	103.8	25.9	57	152.3	38.0	27	200.8	50 9	57	249.3	62.2
8	07,8	01.9	58	56.3	14.0	08	104.8	26.1	58	153.3	38.2	08	201.8	50.3		250,3	62,4
9	03,7	02,2	59	57,2	14.3	09	105,8	26.4	59	154.3	38.5	09	202.8	50,6		251.3	62.7
10	09,7	02.4	60	58.2	14.5	10	106.7	26.6	60	155.2	38,7	10	203.8	50,8		252 3	62.9
11	10,7	02.7	61	59,2	14,8	111	107.7	26.9	161	156.2	39.0	211	204.7	51,1	-	253.2	63.2
12	11.6	02.9	62	60,2	15.0	12	108,7	27.1	.62	157,2	39,2	12	205.7	51.3		254,2	63.4
13	12.6	03.1	63	61.1	15.2	13	109.6	27,3	63	158,2	39.4	13	206.7	51.5	- 122	255,2	63,6
14	13.6	03 4	64	62,1	15.5	14	110,6	27.6	64	159.1	39,7	14	207.6	51.8	64	256.2	63.9
15	14,6	03.6	65	63,1	15.7	15	111,6	27.8	65	160.1	39.9	15	208.6	52.0	65	257.1	64,1
16	15,5	03,9	66	64,0	16.0	116	112,6	-28,1	166	161.1	40,2	216	209.6	52.3	260	258.1	64.4
17	16,5	04.1		65,0	16.2	17	113,5	28,3	67	162.c		17	210.5	52.5	67	259.1	64,6
18	17,5	04,4		66,0	16.5	18	114,5	28.6	Charles and a	163.0	and the second second	18	211.5	52.8	68	260,0	64.9
19	18.4	04,6	100	66.9	10.7	19	115.5	AND THE RESERVE	A COLUMN	164,0		19	212.5	53.0	69	261.0	65.1
20	19.4	04.8	70	67.9	16,9	20	116.4	29.0	70	164.9		20	213.5	53.2	70	262.0	65.3
21	20.4	05.1	71	68,9	17,2	121	117,4	29,3	171	165.9		221	214.4	53,5	271	262.9	65.6
22	21.3	05.3	A DESCRIPTION OF THE PERSON OF	69.9	17,4	22	118.4			166.9	STATE OF THE PARTY	22	215.4	53 7	72	263.9	65.8
23	22.3	05,6	1 3	70.8	17.7	23	119,3		73	167.9		23	216.4	54.0	The Contract of the Contract o	264.9	66.1
24	23,3	05,8	V . W . X . X . X	71,8	17,9	24	120.3		74	168.8	The state of the s	24	217 3	54.2		2659	66.3
25	24,3	06,0	75	72,8	_	25	121.3	1-	75	169.8		25	218.3	54,4	75	266.8	66.5
26	25,2	06,3	76	73,7	18.4	126	122,3		176	170.8		226	219.3	54.7	276	267.8	66.8
28	26.2	06,5	1000	74,7	18.6	27	123.2			171.7		27	220,3	54.9		268.8	67.0
29	27.2	06,8		75.7	19.1	28	124.2			172.7		28	221.2	55.2	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	269.7	67.3
30	29.1	07.3	79 80	76,7	19.4	29	125,2	-	79 80	173.7	43,3	29	222.2	35,4	79	270.7	67.5
-	-			78,6	19.6	30		31.5	-	174.6	-	30	223.2	55.7	80	271,7	
31	30,1	07.5	81	79,6	19.8	131	127,1		181	175.6	CONTRACTOR AND ADDRESS.	231	224,1	55,9		272,6	68.0
32	32,0			80,5	20,1	32	13.00		82	176.6		32	225.1	56.1		273,6	68,2 68 5
33	33.0	08.2	84	81.5	20.3	33	130,0		84	177.6	44.3	33	226 1	56.4		274.6	68.7
35	34,0	08.5			20.6	35	131.0		85	179.5		34	227.0	56,9		275.6	69.0
36		08.7		83,4	20.8	_	-		186	180.5		-		-	-		-
A COLOR OF THE	34,9	09.0	87	84,4	21.1	136		THE RESERVE AND THE PARTY OF TH		181.4	45.0	236	229.0			277.5	69.2
		09.2	88	85,4	21.2	37	132,9		88	182.4	45.3		230.0	57.4	88	278.5	69.5
39	37,8	09,4	80	86,4	21.5	39	134,9			183.4			231.9	57.8	89	280.4	69.9
40	38.8	09,7		87,2	21.8				90	184.4	46.0		232.9	58.1	90	281.4	70,2
41		09.9		88.3	22.0	141	136,8		191	185.3		-		58.3	B	282.3	
42		10,2	92	89,3	22.3	42	137,8	34,4	92	186.3			233.8	58.6	291 92	283.3	70.4
		10,5		90.2		43	138.7	34.6		187.3	46.7		235.8	58.8	93	284,3	70.9
44		10.6	04	91.2		44	139.7	34,8	94	188.2	46.9		236.7	59.0		285.3	71.1
45	43,7		95	92,2		45	140,7		95	189.2	47,2			59.3		286,2	71.4
46		11,1		93,1	23,2	200	141.7	The Real Property lies	-	190.2	AND DESCRIPTION OF THE PERSON NAMED IN		238.7			287.2	71.6
47	45.6	11,4	A Property of the Contract of		23,5		142.6			191.1		47	239.7	50.8	97	288.2	71.9
48	46,6	11,6	98	95.1	23.7		143,6		98	192,1	47.9	48	240.6	60,0	98	289.1	72.1
49	147,5	11.9	99		24.0	49	144,6	36,1		193.1	48,2	49	241.6	60.3	99	290.1	7.2.4
50	48.5	12.1		97.0		150	145	36,3	200	194,1		250	242.6	60.5	300	291.1	72.6
1=	Dep	Lat	Diff	Dep	Lat		Dep		Dif	Dep	Lat					Dep	Lat
1	- Inch	Lat	1211	тер		1DIII	Dep	Lat	Din	Deb	Lat	Join	Deb	Lat	Pin	Lep	Lat
					10000												

for 76 Deg.

													125.4				
Diff	Lat	Dep	Dift	Lat	Depj.	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep
-	01.0	SHOOT SHOT SH	51	49.3	13.2	101	97.6	26.1	151	145.9	39.1	201	194.1	52.0	251	242.4	65.0
2	31.9	A COLUMN TO SERVICE AND ADDRESS OF THE PARTY	52	the second line of the second	13.5	02	98.5	26.4	52	146.8	39.3	02	195.1	52,3	March Property lies	243.4	65.2
3		00.8	53	THE RESERVE OF THE PARTY OF THE	13.7	03	99 5	26.7	53	147.8		03	196.1	52.5	1440 (127)	244.4	65.5
4	23.9	01.0	54	53.1	14.0	04	101.4	27.2	54	149.7	39,9		198.0	53.1		246.3	66.0
_5	100000	01.6	-	54.1			102.4	27.4	156	150'7	40.4	Section 1	199.0	53.3	-	247.3	66.3
6		01.8			14.8	A PERMIT	103.4	27.7	57	151.6	40.6	1.30 Sec. 1869	199.9	53.6	57	248.2	66 5
8	4, 1, 5, 10, 10	02.1	58		15.0	-	104.3	28.0	. 58	152.6	40.9	08	200.9	53.8		249.2	66.8
9		02,3			15.3	09	105.3	28.2	1 STORM STORY	153.6	41.1	09	201.9	54.1		150.2	67.0
10	09.	02.6	60	58.0		10	106.2	28.5	60	154,5	41.4	10	202.8	54.3	-	251.1	67.3
11	10.0	02,8			15.8	111	107 2	28.7	161	155.5	41.7	211	203.8	.54 6	100	252.1	67,5
12	11.		62		16.0		108.2	29,0		156.5	41.9	12	204.8	54.9	62		68.1
13		503.4			16.6	13	110.1	29,2	63	157.4	42.2	21315	206.7	55.1		254.0	68.3
14	1 1 G 1 1 1	503.6	2		16.8	15	111.1	29.8	6:	159.4	42.7	15	207.7	55.6	6.	The state of the state of	68.6
15	-		7	63.7	-	116	112.0	-	_	160.3	43.0	-	208.6	55.9	266	256.9	
16	15	4 04.4			17.3	17	113.0	10 10 10 10 10 10 10 10 10 10 10 10 10 1	67	161.3	43.2	17	209.6	56.1	67	257.9	69.1
13		4 04.	1	The second second	176	18	114.0	1 37 25 11 17	68	162.3	43.5	9 0	210.6	56,4		258,9	69.4
119	13.	4 04.	69		17.9	19	114.9		6.6	11	43.7			56.7		259,8	
20	19.	3 05.	70	-	18.1	20	115.9		70	THE PERSON NAMED IN	-	and the same of	212.5	56.9	70	260.8	
21	A CONTRACTOR OF THE PARTY OF TH	3 05.		68.6	State Control of	121	116.9	The second second			A 1972 9 2 1 1 1	100000000000000000000000000000000000000		57,2	271	261.8	1
22	10000	2 05.	A	69.		22	117.0		T ROW		44.5			57.5	72		Sign of the late
23	1	2 06.0		70.	CONTRACTOR CONTRACTOR		119 8			100-	\$ 0 YOM 18 345	- A CONTRACTOR	C. 10	57.7	73		
24		1 06.	100 100 100 100	72			120.7	The second second		1			N. 162 1 1 2 1	58.2	75		
25	1	106.			1000	126	121.7	A 17 3 18 19		_						266.6	
27		107.			of Milesters	1000	122.7	2 10 13 70 70 132	A 100 M	THE PERSON NAMED IN	75 10 10 10 10 10		3 62 76 2 2 3	III II	77		71.7
28		0 27.					123.6	33,			46.1	28	220.2	59.0	. 78	268.	71.9
29		0 07.			3 20.4	29	124.6	A SECTION OF THE PARTY OF THE P		STATE OF THE PARTY	THE PARTY NAMED IN			1 2 2		269.	The second second
30	29.	0 27.	_			30	125.0		-			-	THE REAL PROPERTY.	323		270.	
31		9 08.		THE RESERVE AND ADDRESS OF THE PARTY OF THE			126.		2.3			ALL DESIGNATION	The second second second			271.	NO. OF REAL PROPERTY.
32		9 08.	3 82			100	127.		100			CALL STREET, TOWN	The state of the state of		All Bridge Co.	2 272.4	TO STATE OF SECULO S
33			-		2 21.5		129.	AL DESCRIPTION OF THE PERSON NAMED IN						The second second		4 274.	
34		.8 09.										7				5 275.	
20		.8 30.			1 22.3				-				_	61.		6 276.	
37	1.	.7 29.	3		0 22.	and the second		Call Control of the C	5 8	180.	6 48.	4 3	7 228.9	61.		7 277.	
38		7 09.		8 85.	0 22.8	38		3 35.	7 8	8 181.		C-11 10 10 10 10 10 10 10 10 10 10 10 10 1			8	8 278.	2 74,5
39	37	.7 10,	1 89	0.0	0 23.0					9 182.	6 48.		9 230.	61.		9 279	
40		.6 10.			9 23.		- Contractor						-			c 280.	
4	ALCO \$175.50	.6 10	6 9	87.	9 23.	141		2 36.	5 19	1 184.	5 49.		1 232,		4 29	1 281.	
4	100	.6 10			9 23.	42		2 36. 1 37.		2 185. 3 186,	5 49.		2 233.		9	3 283.	0 75,6
4	3 41	.5 1.1	1		8 24.		STATE OF SHIPS						4 235	Action of the second se	1 0	4 284	
4	5 42	.5	4 9		8 24.	6 46			CONTRACT OF SHIPLE	1 00		.5 4	5 236	6 63.	4 9	5 284	9 76.3
4	6 4		9		7 24.		-	CONTRACTOR MATERIAL		The second second		7 24	6 237	6 63,	7 20	6 285	9 76.6
4	7 4	4/12	2 9	7 93.	7 25	1 47	142.	0 38	0 9	7 190	3 51	.0 4	7 238	6 63.	9 9	7 286	.9 76.9
4	8 46	.4 12	4 9	8 94.	7 25.	4 48	143	0 38	3 9	8 191			8 239		2 9	8 287	.8 77.1
4	9 47	.3 12	.7 9	9 95	6 25,	6 4	143		.6	9 192	.2 51		19 240			9 288	
5	0 48	.3 12	9 10	96.	6 25.	915	144		,8 20			= =	50 241		= =	289	
D	ift D	epLa	t Di	it Dep	La	t Di	ft Dep	La	t ID	ift De	PIL	at D	ift De	p La	t D	iftl De	p Lat
1-						1	41/0/25										E-T-EVER

			legitor.	Alle, when		351.6											
Diff	Lat	-	Dil	-	Dep	Dift		Dep	Dift	Lat	-	Dift	Lat	Dep	Dift	Lat	Dep
1	01.0			The street of	14.1	101	97.1	27.5	151	145.1	41.6	201	193.2	55.4	151	241.2	69.2
2	31.9			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14.3	02	98 0	A CONTRACTOR	52	146.1	41.9	02	194.1	55.7	10000000	342,2	69.5
3	02.9				14.6	-	990		53	147.1	42.2	03	195.1	55.9		243.2	69.7
4	34.8	12 12 14 11	No. of Concession, Name of Street, or other party of the Concession, Name of Street, or other pa	The second second	14.9	04	100.0	28.9	54	149.0	42.4	04	197.0	56,5	Company of the last of the las	244.1	70.0
$\frac{5}{6}$	05.8		- 33		-		-	-	55				198.c	56.8	_	245 1	70.3
100000	1 2	100 A 18		54.8	15.4	105	101.9	29,2	156	149.9	43.0	206	199.0	57.0	DESCRIPTION OF THE PERSON OF T	246.0	70,6
7 8	07.7	02.2	31		16.0		103.8	298	57 58	151.9	43.5	State of the last	199.9	57,3		247.0	70.8
9	28.7	02,5			16.3	A STATE OF THE PARTY OF	104.8	30.0		152.8	43.8	09	200.9	57.6		248.9	71.4
10	09.6	02.8		57.7	16.5	10	105.7	30.3	60	153.8	44,1	10	201.8	57.9		249.9	71.7
II	10.6	03.0	61	58.6	168	111	106.7	30.6	161	154,7	44.4	211	202.8	58.2	-	250.9	71.9
12	11.5	03.3	62	59.6	17.1	12	107 6	30,9	62	155.7	44.6		203.8	58.4		251.8	72.2
13	12.5	100		60.6			108.6	31.1	63	156.7	44.9		204.7	58.7		252.8	72.5
14		03.9				E W.	109.6	31.4	64	157.6	45.2		205.7	59.0		253.7	72.8
15		04.1	65	A STATE OF THE PARTY OF THE PAR		15	110.5	31.7	65	158.6	45.5		206.6	59.3	65	-	73.0
16		04.4	66	63.4		116	111.5	32.0	166	159.5	45.7	100.75.000	207.6	59.5		255.7	73.3
17	16.3		67	66.4	18.5	17	112.5	32.2	67	160.5	46.0	-/	208.6	59.8		256.6	73.6
18	18.3	05.0		66.3	Control of the contro	19	114.4	32,8	60	162.4	46.6	0.0000000000000000000000000000000000000	210.5	60.4		257.6	73.9
19	19.2		70	67.3		20	115.3	33,1	70	163.4	46.9		211.4	60.6	70	259,5	74,4
21	20.2		-		19.6	121	116.3	33.3	171	164.4	47.1	-	212.4	60.9		260.5	74.7
21	21.1	06.1	72	69.2	The State of	22	117.3	33.0	72	165 3	47.4	22	213.4	61.2		261.4	750
23	22.1	06.3	73	70.2	20.1	23	118.2	33.9	73	166.3	47.7	E1 (90K) (1/5)	214.3	61.5	73	262.4	75.2
24	23.1		74	71.1	1.1	24	1192	34.2	74	167.2	48,0	24	215.3	61.7		263.3	75,5
25	24,0	J6.9	75	72 1	20.7	25	120.1	34.4	75	168.2	48.2	25	216.3	62.0	75	264.3	75.8
26	25.0	07.2	76	73.0	20.9	126	121.1	34,7	176	169.2	48.5	The second second	217.2	62.3	276	265,3	76.1
27		27.4		74.0	1 Party B	27	122.1	35,0	77	170.1	48.8	H.C.	218.2	62.6	77	266.2	76.3
28	26.9		78	75.0		1.00	123.0	35,3	78	171,1	49.1		219.1	62.8	N 200 CO	267,2	76.6
29.	27.9		79	75.9 76.9		29	124.0	35.6	79 80	172.0	49.3	-	220.1	63.1		268.2	76.9
30		08.5	-					36.1				-			-		77.2
31	29.8		81 82	77,9	22.3		125.9	36.4	181	174.0	49.9	3	222.0	63,7		270.1	77,4
32 33	31.7		83	79.8	Contract Charles	3-	127.8	36.7	83	175.9	50.4	The second second	223.9	64.2		271.0 272.0	77.7
34	F	39.4	84	80.7		33	128.8	36.9		176.8	50.7	ALMERICAN STREET	224.9	64.5		273.0	78,3
35		09.6	85	81.7	23.4	and the second	129.8	37.2	85	177.8	51.0		225.9	64.8	85		78.5
36	34.6	09.9	86	82.7	23.7	136	130.7	37,5	186	178.8	51.3	236	226.8	65.0	286	274.9	78.8
37	35.6	10,2	87	83.6	24.0	37	131.7	37.8	87	179.7	51.5	37	227.8	65.3		275.8	79.1
38	36.5				24.3		132.6		881	180.7	51.8	38	228.7	65.6.	88	276.8	79.4
	37.5			85.5	24.5		133.6		89	181.7	52.1		229.7	65 9	89	277.8	79.6
-	38.4	11.0	90	86.5	_		134.6	38.6	Contract of the Contract of th	182.6	52,4	N. Commission	230.7	66.1		278.7	79.9
41	39.4		91	87.5	25-1		135.5	38,9	191	183.6	52.6		231.6	66.4		279.7	80.2
2000 2014	40.4		92	88.4			136.5	39.1	92	184 5	52.9		232,6	66.7	92	280.6	80 5
	41.3		93 94	89.4 90.3			137.4	39.4	93	185.5	53.2		233.6	67.0	93	281.6 282.6	80.8
45	43.3	12,4	95	91.3	26.2		139,4	40.0	95	187.4	53.7		235.5	67,5	94	283.5	81.3
-	44.2		96	92.3	-		140,3	40.2		188.4	54.0		236,4	67.8		284.5	81.6
	45.2		97	93.2	26.7	47	141.3	40.5	97	189.3	54.3	47	237.4	68.1	07	285.5	81.9
	46.1		98	94.2		48	142.2	40.8		190.3	54.6	48	238.4	68.3	.98	286.4	82.1
49	47.1	13.5	99	95.2	27.3	49	143.2	41.1	99	191.3	54.8	49	239.3	68.6	99	287.4	82.4
50	48.1	3.8	100	96.1	27.6	150	144.2	41.3	200	192.2	55.1		240,3	68,9	300	288.3	82.7
==	Dep	Lat	Dift	Dep	Lat	Dift	De p	Lat	Dift	Dep	Lat	Dift	Dep	Lat	Diff	Dep	Lat
				- P	market of the		P.						- r			P	

for 74 Deg.

Difference of Latitude and Departure for 17 Deg.

Dep Dift Lat Dep Dift Lat Diff Lat | Dep Dift אטת 48.8 14.9 29 5 101 96.6 151 201 192.2 58.8 251 240,0 144.4 01.0 00.3 73.3 52 241.0 02 97.5 52 145.3 02 193.2 59.0 01.9 00.6 49.7 15.2 44.4 73.6 03 98.5 30 1 53 146.3 03 44.7 194.1 59.3 53 241,9 02.9 00.9 53 50.7 15.5 73.9 59.6 54 242.9 03.8 01.2 51.6 15,8 04 99 4 30.4 54 147.3 45.0 04 195.1 54 74.1 52.6 16.1 04.8 01.5 05 100.4 30.7 148.2 45.3 05 196.0 59.9 55 243.8 55 74.4 156 149.2 53.5 16.4 256 244.8 56 101. 45.6 206 197.0 60.2 05.7 01.8 Tot 74.7 310 6 102.3 60.5 57 150'1 245 8 57 58 54.5 16 7 07 45.9 07 197.9 06.7 02.0 31.3 750 31.6 58 151.1 60.8 58 246.7 103.3 46.2 08 198.9 07.6 02,3 55.5 17 0 75.3 59 59 152.0 46.5 59 247.7 28.6 02.6 56.4 17.2 09 104.2 31.9 09 199.9 61.1 75,6 46.8 10 200.8 60 248.6 17 5 105.2 32.2 60 153.0 61.4 09.6 02,9 57.4 75 9 10 61 17.8 154,0 201.8 61.7 261 249.6 58.3 111 106.1 32.4 161 47.1 76.2 10.5 03.2 13 59.3 13.1 107 1 202.7 62.0 62 250.5 76.5 62 12 32.7 62 154.9 47.4 12 11.503.5 13 108.1 63 60.2 18.4 63 47.6 13 203.7 62.3 63 251.5 76.8 12.4 03.8 13 33,0 155.9 13 156.8 14 204.6 13.404,1 64 61 2 18 7 14 109.0 64 47,9 62.6 64 252.4 77.1 33.3 14 157.8 15 205.6 14.3 04.4 62.2 19.0 15 110.0 33.6 65 48.2 62.8 65 253 4 77,4 15 216 206.5 166 . 58.7 48.5 266 254.4 66 110.9 15 3 04.7 63.1 19.3 33.9 63.1 77.7 16 111.9 48.8 64.1 19.6 159.7 17 207.5 16.305.0 67 17 34.2 63.4 67 255.3 77.9 17 18 112 2 160.6 18 208.5 68 256.3 68 63.7 78.a 65.0 19.9 49.1 17.2 05.3 34.5 18 19 209.4 66.0 20.2 161.6 113.5 34,8 69 69 257.2 49.4 78.5 18.2 05 6 19 19 78.8 20 114.7 162.6 20 210.4 70 258,2 66.9 20.5 35,1 19.105.8 70 49.7 64.3 70 20 163.5 06.1 221 211.3 67.9 20.8 121 115.7 50.0 259,1 20.1 171 646 271 35,4 79.1 71 21 164.5 21.0 06.4 68.8 22 116.7 22 212.3 64,9 35.7 36.0 50.3 21.0 260.1 72 72 22 73 79.4 1654 23 117.6 50.6 23 213.2 261.1 42.0 05.7 69.5 21.5 65.2 73 73 73 79.7 23 24 118.6 166.4 65.8 70.8 21.6 36.2 50.9 24 214.2 262.0 80.0 22.9 07.0 74 74 74 24 119 5 36,5 167.3 51.2 25 215.2 263.0 71.7 21.9 80.3 23.9 27.3 75 2: 75 25 75 168.3 226 216.1 36.8 24,9 07.6 72 7 22.2 126 120.5 176 51 4 66.1 276 263.0 80,6 26 169.3 66.4 264.9 121.4 27 217.1 73.6 22.5 37.1 51.7 80.9 2 25.8 07.9 77 77 27 52.0 26 8 08.2 28 122.4 28 218.0 78 74.6 22.8 37,4 78 170.2 78 265,8 81.2 28 79 266.8 79 8c 52,3 66.0 27.7 08.5 79 75.5 23.1 123.4 171,2 29 219 0 81.5 29 29 37.7 52.6 30 219,9 28.7 8.8 76.5 23.4 38.0 172.1 81.7 30 124.3 67.2 30 125.3 181 231 220.9 281 268.7 38.3 67.5 81 173.1 77,5 23.7 52.9 82.0 29.6 09.1 131 31 32 126.2 38.6 32 221.8 174.0 82 67.8 82 78.4 24 C 82 269.7 82.3 32 30.6 39.4 53.2 83 79.4 24.3 127.2 38,9 83 175.0 33 222.8 68.1 53.5 83 270.6 31 6 09.6 33 82.6 33 84 175,9 84 128.1 53.8 68.4 80.3 24.6 39.2 34 223.8 84 271.6 32.5 09.9 34 82.9 34 34.8 85 176.9 68.7 81.3 85 272.5 129.1 39.5 35 224.7 54.1 37 5 10,2 35 83.2 35 82.2 25.1 130.0 39,8 186 177.9 54.4 236 225.7 690 286 273.5 86 136 83.5 36 34.4 10 5 35.4 10.8 83.2 25,4 37 131.0 40.0 178.8 37 226.6 87 54.7 69 : 83.8 274.4 37 38 36.3 11.1 84.1 179.8 88 38 88 25.7 132.0 40.3 55.0 227.6 60.6 84.1 275.4 85.1 80 180.7 39 228.5 37.3 11,4 89 26.0 39 132.9 40.6 55.2 60 9 89 276.4 84.4 39 181.7 40 229.5 38.2 11.7 86.1 133.0 90 90 26.3 40 40 9 90 55.5 70.2 84.7 277.3 40 191 182.6 55.8 56.1 26.6 241 230.5 141 134.8 291 39.2 12,0 91 70.4 278.3 85.0 41 40.2 12.3 88 6 26.9 42 135.8 92 183.6 41.5 42 231.4 70.7 92 279.2 85.3 92 88.5 -7.2 41.8 93 184.6 56,4 136.7 71.0 85.5 93 43 43 232,4 93 280.2 56.7 89.9 27.5 94 185.5 137-7 44 233.3 94 281.1 42.1 12. 94 42.1 71.3 138.7 95 186,5 42.4 57,0 43.0 13.2 95 45 234.3 71,6 95 282.1 41:8 28.1 139,6 42.7 196 187.4 57.3 57.6 246 235.2 14 0 13.4 146 71.0 296 183.0 -96 46 92.8 28.4 93:7 28.6 94.7 28.9 95.6 29,2 97 188.4 47 236,2 48 237.1 140,6 97 47 43.0 72.1 86.7 44.9 13.7 97 284.0 48 141.5 98 189.3 285.0 57.9 98 45.9 14.0 43.3 72.4 87.0 43.6 142.5 99 190.3 49 238,1 72 7 46.9 14.3 99 49 99 43.8 200 191.2 58.5 250 239.1 143.4 150 100 73.0 Lat Dift Dep Lat Dift Dep Dift Dep Lat Dift Dep Lat Dift Dep Lat Dift Dep

39/516 0/132 126

for 73 Deg.

18 Difference of Latitude and Departure for 18 Deg:

12:01		12	Date	1	1200	D:Ai	T - 1	D 1	D:al	T at .	Don	D:41	Lat	Dan I	Dial	1	11
Diff	Lat	Dep	Dist.	Lat			Lat	Dep	Dift	Lat	Dep	Din	Lat	Dep			Dep
1	01.0	00.3	51	48.5	15,8	101	96.1	31 2	151	143.6	46.7	201	191.2	62.1	251	238.7	77.6
2	01.9	00.6	52			02	97.0	31.5		144.6	47.0	02	192.1	62.4	400000000000000000000000000000000000000	239.7	77.9
2	02.9	00.9	53	50.4		03	98.0	31.8	BURNING ST	145.5	47.3	03	193.1	62.7	53	240,6	78.2
4	03.8	01.2	54	51.4		04	98.9	32.1		140.5	47.6	04	194.C	63.0		241.6	78.5
3	100	01 5	55	52.3	100000000000000000000000000000000000000	0;	99 9	32.4		147.4	47,9	05	195.0	63.3	55	242.5	78.8
5	+				-					148.4	48.2	206	195.9	63.7	256	-	-
6	05.7	1000	56	53.3		106	100.	32,8	The state of the state of	1	48.5			64.0		243.5	79.1
7	06.7	02.2	57		176	07	101.8	33,1		149.3	48.8	c7	197.	64.3	57	244.4	79.4
8	9	02,5	58			08	102.7	33.4	-	(See 20) 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		1 1 1 2 2 1	0.0	64.6	J. B. T. A. S. T.	145 4	79.7
9		02.8	59		18.2	09	103.7	33.7		151.2	49.1	09	PERSONAL PROPERTY.		59	246.3	80.0
10	09.5	03.1	60		18.5	10	104.6	34.0	-	152.2	49.4	10	199.7	64,9	_		80.3
II	10.5	03.4	61	58.0	188	111	105.6	34.3	161	153.1	49.7	211	200.7	65.2		248.2	
12	11.4	03.7	62	59.0	19.2	12	106.5	34.6	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	154.1	50.1		201.6	65.5			4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
113		04,0			19.5	13		34,9	63	155.C	50.4	The second		65.8		250.1	81.3
14		04.3		60.9	19.8	14	108.4	35,2	64	156,0	50.7	14	203.5	66.1		251.1	
115	14.3	04.6	65	618	20.1	15	109.4	35,5	64	156.9	51.0	15	204.5	66.4	65	252.0	81.9
16	15 2	04.9	66	62.8	20.4	116	110.3	35.8	166	157.9	51.3	216	205.4	66.7	266	253.0	82.2
17		05.3		-	20.7	17	111.3	36.2	67	158.8	51.6		206.4	67.1	100 march 200		
18	The same and a	05.6			21.0	18	112.2	36.5		159.8	51.9	18	207.3	67.4		254.9	
119		05 9			21.3	19	113.2	36,8	69	160.7	52.2	19	208.3	67.7	and the same	255.8	A STATE OF THE STA
20		06.2	100		21.6	20	114.1	37.1	70	161.7	52,5	20	209.2	68.0		256.8	
1-	-	06.5	-	62.	21.9		115.1		171	162.6	52.8	221	210.2	68.3			
21		06.8		68 6	22.2	121	116.0	37,4	72	163.6	53.1	22	211.1	68.6	72		84.0
22		07.1			22.6	22	117.0	38.0	73	164.5	53.5		212.1	68.9	73	1	
23		37.4			22.9	24	117.9	38.3	74	165.5	53.8				74		
24		07.7		4:55 A 3 (A 10)	23.2	25	118.9	38.6	75	166.4	54.1	25		69 5	75		
25						-		-	-				-	69.8	_	-	-
26		38.0	The state of the s	1 1 20 A 10 C 1 8 7 A	23.5	126	1198	38,9	176	167.4	54.4	226		CO OF CASE	276		
27		08.3		The state of the s	23.8	27	120.8	39.2	77	168.3	54.7	10 P / 10 P	215.9	70.1	77		
28		38.7			14	28	121.7	39.6		169.3	55.0	B			ALC: YES SHOW	264.4	12 (10 - 10 - 10 - 10 - 10 - 10 - 10 - 10
29		09.0			24.4	29	122.7	39,9		170.2	55.3		217.8			266.3	
30	28.	39.3	-	70.1	24.7	30	123.0	40.2	80	171,2	55.6	_			-	-	
1 31	29.	509.6	81		25.0	131	124.6	40.5	181	172.1	55.9			71.4	100000000000000000000000000000000000000		
32	30.4	109.	82		25,3	32	125.5	40.8		173.1	56.2		220.6		The state of the s	268.2	
33	31.	10,1	2 83	78.9	25.6	33	126.5		83	174.c	56,5					269.1	
34	32.	10	84		26.0		127.4	41.4		175.0	The second second second second	110000000	The state of the s			270.1	
35	33.	10.8	85	80.8	26.3	35	128.4	41.7	85	175,9	57,2	35	223.5	72 6	85	271.	
36	34.	2 11.	86	81.8	26.6	136	129.3	42.0	186	176.9	57,5	236	224.4	72.9	286	272.0	0 88.4
37		2 11,	4 87		26.9	37	130.3		87	177.8	57.8	37	225.4	73.2	87	272.	9 88.7
38	136.	111.		83.7	1 27.2	38	131.2	42.6	88	178.8	58.1	38	226.3	73.5	88	3 273.	9 89.0
39		1 12,	474 17 (10.00)		27.5			43.0	89	179.7	58.4	39	227.3	73.9	80	274.	8 89.3
40		12.4		85.6	6 27.8	40	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -				58.7	40	228.2	74.2			
-	-	12.	The state of the s		28.1		134.1	Name and Address of the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner, wh	101	181.6		No. 1277	ALC: NAME AND POST OF	100000000000000000000000000000000000000	-	276.	
41	75,000			87.	28.4	42				182.6	59.3		2 30.1		0:	2 277.	
42		9 13.		88	4 28.7	43				1 0			3 231.		0	278.	6 90.5
43	7 S C C C C C C C C C C C C C C C C C C	8 13.			129,0			44.5			59.9		232,0		94		
44	1.10	8 13.			3 29 4						60.	4	233.0				
45								177							-		
46		7 14.		91.3	3 29.7	146	130.6	45.1		State of the state	60.	240	233.			231.	
47		7 14.			30.0			45.4	97	188.	61.					7 282.	4 91.8
48	45.	14.	98		30.3			45.7	90		61.		235.				
49		6 15.			30.6			46.0	99	100	61		236,	8 77.		9 284	
50		-	5 100	-	30.9	_	NAME OF TAXABLE PARTY.		-	190.						285.	
Dif	De	Lat	Dil	Dep	Lat	Dif	Dep	Lat	Dif	l Dep	Lat	Di	d Dep	Lat	Di	itl Der	Lat
-																	

Difference of Latitude and Departure for 19 Deg.

Dift	Lat	Dep	Dift	Lat.	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	
-	00.9	:0.3	The same of	48.2	16.6	101	95.5	32.9	151	142.8	49.2	201	190.0	65.4	251	237.3	81.7	
2	21.9	20.7	52		16.9	02	96.4	33.2	52	143.7	49.5	Designation of the last	191.0	65.8	52	238.3	82.1	-
3	02.8	010	53	Bearing Street, Square, and the same of th	17.3	03	97.4	33.5	53	144,7	49,8	03	191.9	66.1		239.2	82.4	
4	03.8	01.3	54		17.6	04	98.3	33.9	54	145.6	50.1	04	192.9	66.4	54	240.1	82.7	
5	04.7	01.6	55	52.0	17.9	05	99.3	34.2	55	146.5	50,5	05	193.8	66.7	55	241.1	83.4	
6	35.7	02.0	56	52.9	18.2	106	100.2	34.5	156	147-5	50,8	206	194.8	67.1	256	242.0	83.4	
7	06.6	02.3	57		18.6	07	101.2	34.8	57	148.4	51.1	07	195.7	67.4	57	243.0	83.7	
. 8	14. A. C. C. S. M.	02,6	58		18 9	08	102.1	35.2	58	149.4	51.4	80	196.7	67.7	58	243.9	84.0	
9	08.5	02.9	59		19.2	09	103.1	35.5	59	150:3	51,8	09	197.6	68.1	59	244,9	84,3	
10	09.5	03.3	60	56.7	19,5	10	104.0	35.8	60	151,3	52.1	10	198.5	68.4	60	245.8	4.7	ı
11	10.4	03.6	61	57-7	19.9	111	104.9	36.1	161	152.2	52.4	211	199.5	68.7	261	246.8	85.0	ı
12	11.3	03.9	62	58.6	20.2		105.9	36.5	62	153.2	52 7	12	200.4	69.0	62	247.7	85,3	ı
13	12.3	04.2	63	59.6	20.5	13	106.8	368	63	154.1	53.1	13	201.4	69,4	63	248.7	85.6	
14	13.2	4	64		40.8	14	107.8	37.1	64	155 1	53,4	14	202.3	69.7	64	249.6		1
15	4.2	24.9	65	61.5	212	15	108.7	37.4	65	156.0	53.7	15	203.3	700	65	250.5	86.3	
16	15 1	05.2	66		21.5	116	109.7	37 8	166	156:9	54,0	216	204.2	70.3	266	251.5	86.6	100
17	16.1	05.5			21,8	17	110.6	38.1	67	157.9	54,4	17	205.2	707	67	252.4	86.9	
18	17.0		12			TO BE THE STATE OF	1116	38,4	68	158.8	54.7	18		71.0	The second	253.4	87.3	1
19		06.2			22.5	19	112.5	38.7	69	159.8	55.0	19	207.1	71.3	(Sec.) 9	A PROPERTY OF THE PARTY OF THE	87.6	
20		06.5	-	-	22,8	20	113.5	39.1	70	160.7	55,4	20		71.6	-	255.3	87,9	
21	19.9	A COLOR	/			121	114.4	39.4	171	161.7	55.7	221	208.9	72.0	Mark Comments	256.2	88.2	
22	20.8				23.4	100	115.3	39.7	72	162.6	56.0					257 2	88.6	
23	1	07.5	4 15.6.		23,8	1 P. James	116.3	40.0	73	163.6			210.8	S 1007 C - 27 7 100 C 1			88.9	
24		07.8	A	CONTRACTOR OF THE PARTY OF THE	24.1	100000	117.2	40.4	74	164.5	THE RESTAURT OF THE PARTY OF TH		211.8	72.9		259.1	89.2	1
25	-	-		-	24,4			40.7	75	165.5	-	25		73.3	-	260.0	89.5	-
26		08.4			24.7	126	119.1	41.0	176	166.4	57.3	226		73.6				
27		08.8			2 5.1		120,1	41.4	77	167.3			214.0			261.9		
28		109.4	C. C. C. C.	Will be the second	1 -5-4	700	121.0		78	169.2		A 12 (1)	215.6	A COLOR	and the same		1	-
29	0				25,7	100	122.9	42.3	79			20	210.5	CONTRACTOR AND AND		264.7		
30					-		-								-	-	-	-1
31		3 10.	CALL STREET	10 March 10 2	5 26.		123.9	42.7	181	THE RESERVE AND THE PERSON		100	Sec. 33. 2	ALL REPORTS AND ADDRESS.				~ 1
32		The second			5 27.0		Marie St.		. V . A. V . C. P. P.	120.76								100
33		-/ LANGE	-	1000000	100000		1 1	43.6		A STATE OF THE STA		100				268.		
35							1					0.47	CONTRACTOR OF THE PARTY OF THE					7
36		0 11.	_		3 28,			100,000	186		-		-	-	-	270.	-	4
37		0 12.		7 82.	3 23.	3 37	A SECTION OF THE PARTY OF	100000000000000000000000000000000000000		176.8			224.1	77.2	8-	271,	93.4	
38	35.	9 12,	4 8	8 33.	2 28.		130.			177.7		38	225.0	77.5	88	272.	93.	8
39		9 12.			1 29.		131.4	45,3		178.	61.9	39	226.0	77.8	8	273.	94.	
40	1000		0 9	0 85.	1 29	3 40	132.4	45.6	The late of the la			40	226.	78.1	1 90	274.		
4	-	8 13.	Marie Control	-			THE PERSONS NAMED IN	THE RESERVE OF THE PERSON NAMED IN	all languages		62.1	24	1 227.	78.			-	-
4:	. *				c 30.	C 42			92	181.	62,		2 228.	78.8		276,		
4:		7 14.	0 9	3 87.	9 30.	3 43	135.	46.0	9	182.	62.8		3 229.			277		
44		6 14	3 9	4 88.	9 30.	6 44	136.	46.9	94	4 183.4	1 63.	2 4	4 230.		4 94	4 278.	95.	
4.	5 42.	5 14.	7 9	5 39	8 30.	9 4	137.		9	5 184.	4 63.	5 4	5 231.		8 9	5 278.	9 96.	
4	6 43.	5 15			8 31.				19	6 185.	3 63.		6 232.	6 80.		6 279.		-
4	7 44.	4 15	3 9		7 31.	6 4	139.	0 47,1	9 9	7 11 30.	3 64,	1 4	7 233.	5 80.	4 9	7 280.	8 96,	7
4	8 45.	4 15	6 9	8 92	731.	9 4	8 139	9 48	2 9	8 187.	2 64.	5 4	8 234.	5 80.	7 9	8 281.	7 97	c
4		3 16	0 9	9 93	6 32.	2 4	140	9 48.	9	9 188.		8 4	9 235.	4 81.	1 9	9 282.	7 97.	
5	0 47	3 16	3 10	0 94	1 32.	6 150	141.	8 48.	8 200	189.	65.	1 25	0 236,	4 81.	4 30	283.	6 97.	
i	ft De	pLa	t D	A De	La	t Di	A Der	Lat	Di	ft Der	Lat	Di	ft Der	Lat	Di	R De		
-																	- Ja	-

for 71 Deg.

19

2	20	Di	iffe	ren	ce c	of I	Lati	tude	a a	nd I	Depa	rtu	re f	or 2	20	Deg.	
int	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	De
1	00.9	00.3			17.4	101	94.9	34,5	151	141.9	51.6	201	188.9	68 7	251	235.9	85
2		00.7		48.9	17,8	02	95.8	34 9	52	142.8	52.0	02	189.8	69.1		235.8	86
		0.10		49.8	18.1	03	96.8	35,2	53	143,8	52.3	03	190.8	69.4	53	237.7	86
275	34.7	31.4	100000	50,7 51,7	18.5	04	97.7	35.6	54	144,7	52.7	04	191.7	69.8		238 7	86
-	-	02,1	55 56	52.6		-	-	36,3	55 156	145.7		05		70,1	55	239.6	87
		02.4	57	53.6	19.2	106	99.6	36,6	57	147.5	53,4	206	193.6	70,5	256	240.6	87
2		32.7		54,5	19.8	08	101.5	36.9	58	148.5	54.0	08	195.5	71.1	57	241.5	87
	08,5	03.1	and the second of	55.4	20,2	09	102.4	37.3	59	149,4	54.4	09	196,4	71.5	59	243.4	88
10	9,4	034	60	56.4	20.5	10	103.4	37.6	60	150.4	54,7	10	197.3	71.8		244.3	88
11	10,3	03,8		57,3	20.9	111	104 3	38.0	161	151,3	55.1	211	198.3	72.2	261	245,3	89
10	11.3	04.1		58.3	21.2	12	105,2	38.3	- 62	152.2	55,4	12	199.2	72.5	62	246,2	89
13	12.2	24,4		59,2	21.5	13	106.2	38.6	63		55.7	13	200.2	72.8	63	247.1	89
14	13.2	04,8		61.1	21.9	14	107.1	39.0	64	154.1	56.1	14	201.1	73.2		248,1	90
15	14,1	05.1	-	-	-		-	39,3	9.5	155.1	-	15	202.0	73 5	-	249 0	90
16	15,0	05,5	1 1 1 1	62,0	22.0	4 .	109,0	39 7		156.0 156.0	56.8		203.0	73.9		250,0	91
18				63,9	23,3	17	110,9	40,4		157.9	\$7.5		203.9	74.2	The same of the same	250,9	91
19	17,9	26,5			23,6		111,8	40.7	69	158,8	57.8	10	205.8	74.9	69	251.8	91
20	18.8	06,8	70	10	23.9		112,8	410	70	159.7	58.1	20	2067	75 2	70	253.7	92
21	19.7	07,2	71	66 7	24.3	121	113,7	41.4	171	160.7	58.5	221	207.7	75.6	-	254,7	92
22	20.7	7.5	72	67.7	24,6		114,6	41.7	72	161.6	58.8		208.6	75.9	100 - F 11 - 5	255,6	93
23	21.6	27.9	73	68,6	25 C		115.6	42 1	73	162,t	59.2	23	209.6	76,3		256.5	93
24	22 6	1 0 .	74				116.5	42.4	74	163.5	59.5	24	210.5	76.6		257.5	93
25	23,5	-	1-3	-	25 7	_		42.8	7.5	164,4	59.9	25	211.4	77.0		258.4	94
26	1	28.9	76		26.0			43.1	176	165.4	60,2	226	212.4	77.3		259.4	94
27	1	39.2		72,4	26.7		119 3	43,4	77	166.3	60.5	27	213.3	77,6		260,3	94
20	-	1			100	1 1 1 1 1	1 1 1 1 1 1 1	43,8		168.2	60.9	28	214.3	78.0		261.2	95
30	1 0				A		1 1 1 7 7 7 1 1 1	44.5		169.1	61.6		216.1	78.7		262.2	95
31	-		-	-	-	-	123.1	44.9	181		61.9	231	217.1	79.0	-	-	95
32	1			77.1				45.1		171.0			218.0	79.3	82	264 1	96
33			83	78,0	28 4	33				172.0	A COLUMN TO SERVICE	33	219.0			265 9	96
34	31.9	11.6	84	78,9	28.7	34	125.0	45,8	84	172.9	62.9	34	219.9	80,0	84	266.9	97
35		12.0			29.1	35	126,9	46.2	85	173.8	63,3	35	220,8	80,4	85	257.8	97
36	33.8	12,3		30,8			127,8	46.5	186	174.8	63.6	236	221.8	80,7	286	268.8	97
37	134,8	12.7		81.8		37	128,7	46.9	87	175.7	64,0	37	222.7	81,1	87	269.7	98
38		13.0			30,1		129.9	47.2	88	176.7	64.3		223.6	81.4		270.6	98
39		13,3	80	83,6	30.8		130,6	47.5		177.6	64.6	39	224,6	81.7		271,6	98
40							-		100	A STATE OF THE REAL PROPERTY.		40	126.5	82.1	-	272,5	99
41	38.5	14.0			31.		132,5	48.2	191			241	226 5			273,5	99
42	39.5	14.4		87,4	31.	42		48.9	92		65.7	43	227.4	82.8		274.4	99
44	41.3	15.0	94	188.3	32.1		135,3			182.7	66.3	44	229.3	834	93		100
4		15.4			32.	45	136,3	49.6	95		66.7	45	230.2	83,8		277.2	100
46	43,2	15.7				146	137,2	49.9		184.2	67.0	246				278.2	101
47	44.2	16.1	97	91.2	133.2	47	1138.1	50.3	97	185.1	67.4	47	232.1	84,5	97	279.1	101
48	45.1	16.4	98	92,1	133,	48	139.1	50.6	98		67.7	48	233.0	84,8	98	280.0	10
49	46,0	16,8	99	93,0	33.5	49	140,0	51,0		187.0	68.1	49	234.0	85,2	99	281.0	102
50	47,0	17,1			34 2		141.0	51.3	200					85,5	300	281.9	102
Dit	Dep	Lat	Dif	Dep	Lat	Dif	Den	Lat	Diff	Dep	Lat	Dia	Dep	Lat	D:/	Dep	L

for 70 Deg.

Dift	Lat	Dep	Dift	Lat.	Dep	Dittl	Lat	Dep	Dift	Lat	Dep	Din	Lat	Dep	Dift	Lat	Dep	
1	00.9	00.4	51	47,6	-	101	94.3	36.2	151		54,1	201	187.6		251	234.3	90,0	11
12	Course of the	00.7		48.5		02	95.3	36.6	52	141.9	54,5	02	188 6	72,4		235.3	90.3	1000
3	02.8	E-12 (150)	53	49.5	The state of the s	03	96.2	36.9	53	142.9	54.8	03	189.5	72,8	53	236,2	90.7	
4	03.7	01.4	54	50.4		04	97.1	37.3	54	143.8	55.2	04	190.4	73.1	54	237.1	91.0	
5	04,7	31.8	55	51.3	19,7	05	98.1	37.6	55	144,7	55,6	05	191.4	73.5	55	238.1	91.4	
-6	05.6	02.2	56	52.3	20.1	106	99.0	38.0	156	145.7	55.9	206	192.3	73.8	256	239.0	91.8	
7	26.5	02.5	57	53.2		07	99.9	38,3	57	146.6		07	193.2	74.2	57	239.9	92.1	
8	07.5	02,9	58		100	08	100.9	38.7	58	147.5	A STATE OF THE STATE OF	the state of the state of	194.2	74.5	58	240.9		
9	08.4	03.2	59	55.1		09	101.8	39.1	59	148.5	57.0	09	195.1	74.9	59	241.8	92.8	
10	09.3	-	-	-	21.5	10	102.7	39.4	60	-	57.3	10	196.0	75.3	60		93.2	1
11	10.3				21,9	13 1 1 1 1 1	103.7	39.8	161			211	197.0	756	261	A CARLO MANAGEMENT	93.2	
12	11.2		100		22 2	12	104.6	40.1	62				1 00	76.0	62			
13	13.1			59.7	1	13	106.5	40.9	64				0	76.7	63			
15	14.0	1 -	VIII.			15	107.4	41 2	65		Contract of the Contract of		7. 100	77,1	65	The state of the	100	
16	14.0	-			- 3 3	116	-	-			-	-	-	77.4	266			-
17	150				1 3,1	2	109.3	41.9	67				1		67			
18	16.8			1	5 24,4			1000000	16					1 10 10 10 10 10 10 10 10 10 10 10 10 10	68		1 00	
19	17.7	06.8	69			2.30				157.8	60.6			78.5	60	251.1		
20	18.7	07.	70	65.	3 25.1	20	112.1	43.0	70	158.7	60.0	20	205.4	78.8	70	252.		
2 1	19.6	07.	71	66.	3 25.4	121	113.0	43.4	171	159.	61.	22	206.	79.2	27	253.0	97,	1
22	20.		72	67.		22	113.9	43.7	72		CONTRACTOR OF STREET	100		796		1		
23	21.										The second of	2.1		1			9 97.	8
24	22.		1				1 - 1		1 1 1									2
25	23.	3 39	-			-	-	44.8	-	-	-	- 1					-	
26	24.			The same of			0			1			1 1 1 1 1 1	The second second			7 -98.	9
27	11	7 7 7 1					and the second second	1										7
2.8	1	1 3 5			8 28,		The state of	5 45.9	7	1						100		
29	0						1 300		7 8	1							4 100	
30	.0	-	-	_	-	-	-	-	-	_	-			-	-	_	-	
31									4.0		2 2 2 2 2						3 100	.7
32	1.0				-										5 8	3 264		
33				4 78.	4 30.	1 3	,	1 0		4 171.					9 8	4 265	1 101	
3.5		7 12,		5 79		1000 750		1 48.	4 8	5 172.			5 219.		2 8	5 266	100	100
36		6 12.	9 8	6 80.	3 30.			0 48.	7 18	6 173	7 66.	7 23	6 220.	3 84,	6 28	6 267	0 102	-
3		5 13,	3 8	7 81	2 31,	2 3	7 127.	9 49.	1 8	7 174.	6 67	0 3	7 221.	2 84	9 8	7 267	.9 102	
38	35.	5 13.	6 8	8 82	1 31.	5 3	8 128.	9 49.	5 8	8 175.	5 67	4 3	8 222.	2 85.	3 8	88 268	.5 10:	2.3
39	36.				1 31.	9 3	9 129.	8 49,		9 176.			9 223			39 269	8 103	3.6
40	37.		3 9	0 84				7 50,		0 177			0 224			0 270	17 103	19
4	1 38.			1 84	.9 32.	6 14	1 131.	50,			3 68		1 225		4 29	271	,7 10	1.5
4	2 39.			2 85	.9 33	0 4				2 179			2 225		1.0	92 272	,6/104	4.7
4		1 15	4 9	3 86	8 33	3 4	3 133			3 180			13 226				15 10	
4		0 16		4 87	7 33	4	4 134	5 51.		181		.5	44 227				-5 10	
4	5 42	-	-		7 34		5 135						_	-	-		14 10	-
4	6 42	9 16	5 9	6 89	.6 34	4 14			3 19	6 183	.0 70		46 229			96 276	,3 10	6,1
4	7 43	.9 16	2	8 91	·5 34	1 4	7 1:37 8 138	3 52		8 184	9 70	6	47 230			97 277		
4		7 17		9 92	4 35	.5	9 139	·2 53	4	9 185	.8 71		48 231	.5 89		99 279	3.2 10	
4 5				0 93	.4 35	.8 1		.1 53	8 20	00 186	.7 71		50 233	.4 89		00 280	0.110	7.2
	_ =		= =		THE REAL PROPERTY.	adverse Batterie	-	CONTRACTOR OF THE PERSONS NAMED IN	_	ift De		-	-	-				
D	IN DO	ep L	at D	IND	chira	IL ID	ft De	p La	t II	חוון של	p La	1 4	itt De	p La	t IL	Diff D	ep I L	at

22 Difference of Latitude and Departure for 22 Deg.

Ditt	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep	Din	Lat	Dep	Dia	Lat	1 Dep
I -	-	00.4	51	-	19.1	101	-	37.8	-	-	56.6			-			-
2	01,9	00.7	52	48.2	19.5	02	93,6	37.0	151	140,0	56.9		186.4	The second second		232.7	9 D 10 May 17 At 17 A
1 3		01.1	53	49.1	19 9	03	95 5	38.6	52 53	141.9	57.3	02	188.2	75.7			94.4
1 4		01.5	54	50,1	20.2	04	96.4	39.0	54	142.8	57.7	04	189.1	76.4	53	234.6	95.2
5	300	21.9	55	51,0	20.6	05	97.4	39,3	55	143,7	58.1	05	190.1	76 8		236.4	95.5
6	-	02.2	56		21.0	106	98,3	39 7	156	144,6	58.4	206	191,0			-	THE RESERVE AND ADDRESS OF THE PERSON NAMED IN
7	1 :		57	52.9	21.4	07	99.2	40,1	57	145.6	58 8	27	191.9	77.2		237 4	95.9
8	The Standard Co.	03.0	58	53.8	21.7	7 27	100.1	40,5	58	146,5	59 2	D 3/1-21	192,9	77,5		239.2	96.6
9		03 4	59	54,7	22.1	00	101.1	40.8	59	147.4	59.6	09	193.8	78.3		240.1	97.0
10	The state of the state of	03,7	60	55.6	22.5	10	102.0	41 2	60	148.4	59.9	10	194,7	78.7		241.1	97.4
11	10,2	04.1	61	56.6	22,9	111	102.0	41.6	161	149,3	60.3	211	195.6	79.0		242.0	97,8
12	11.1	04,5	62	57.5	33,2	12		42 0	62	150.2	60.7	45.00	196,6	79.4	The state of the state of	342.9	98.1
13	12 1	04,9	63			13	104 8	42.3	63		61,1	1	197.5	79,8	ALCOHOLDS O	243.9	98.5
14	13.0	05.2	64		24 0	14	105,7	42.7	64	152.1	61.4	100	198.4	80,2		244.8	98.9
15	13 9	05,6	65	60,3	24,3	-15	106.6	43.1	65	153 C	61.8	15	199.3	80,5		245,7	99.3
16		06,0	66	61.2	:4.7	116	107.6	43,5	166	153.9	62,2	216	200.3	80,9	266	246,6	99,6
17	3,	06,4	67	62,1	25.1	17	108,5	43,8	67	154.8	62.6	17	201.2	81,3		247.6	100.0
18	1		68	63,0	25.5	18	109,4	44,2	68	155.8	62.9	18	202.1	81.7	68	248.5	100.4
119		07,1		4	25.8	19	110,3	44 6	69	156.7	63,3	19	203.1	82.0	69	249 4	100,8
20	18.5	07.5	70	-	26.2	20	111,3	45.0	70	157,6	63.7	20	204.0	82 4	70	250,3	101.1
21	19.5		71	65,8	26.6	121	112,2	45,3	171	158,6	64,1	221	204.9	82.8	271	251.3	101,5
22		1 0 0	72	66 8	27.0	22	113,1	45,7	72	159.5	64.4	22	205.8	83,2	72	252.2	101,9
23		1	73	67.7	27.3		114,0	46.1	73		64 8	23	206.7	83.5	73	253.1	102 3
24		09.0	74		27,7	24	115.0	46.5	74	161.3	65.2	24	207.7	83,9	74	254,1	102 6
25		39.4	75	69.5	28,1	25	115.9	46.8	75	162.3	65.6	25	268.6	84'3	75	255,0	103.0
26		09,7	76		28 5	126	Places Countries	47-2	176	163.2	65.9	226	209.5	84,7	276	255,9	103.4
	25,0		77	71,4	28.8	27	117,8	47.6	77	164,1	66.3	27	210.5	85,0	77	256.8	103.8
28		10,5			29.2	100000	118,7	47.9		165.0	66.7		211.4	85,4		257.8	104.1
29		10.9		A CONTRACTOR OF THE PARTY OF TH	29,6	29	10. 5 9	48.3		166.0	67.1	29	212.3	85,8	79	258.7	104.5
30	-	11,2	-	-	30.0	30	120.5	48.7		166.9	67.4	-	213.3	86.2	80	259.6	104.9
31					30,3	131	121.5	49.1	181		67.8	231	214.2	86.5	281	260,5	105.3
32	29.7	12.0		76,0	30.7	32	122,4	49.4	College College	168.8	68.2		215.1	86 9	82	261.5	105.6
33		12,4		77.0	31.1	33	123.3	49.8		169.7	68,6	33	216.0	87,3		262.4	
34	The state of the s	12.7	85	77,9	31.5	34	124.2	50.2	85	170.6	68 9		2170	87 7		263.3	106.4
35		-	-	-	-	35	125,1		-	-	69.3		217.9	88,0		264.3	106.8
36	33.4	13,5	86		32.2		126.1	50.9	186	172.5	69.7		218.8	88 4	286	265.2	107.1
1 37	34,3	14.2	90	80,7 81.6	32.0	37	127,0		07	173.4	70,1	37	219.7	88.8	87	266.1	107.5
30	35,2	14.6	80	82,5	33.0		128,0	51.7 52.1	80	174:3			220,7		88	267.0	107 9
40	36.2	15.0	90	83,4	33.7	39 40	129.8	52.4		175.2 176.2	70.8		221.6	89,5	89	268.0	108,3
	3/3-		-				-		90	THE RESERVE OF THE PERSON NAMED IN	71.2	-		89.9	-	268.9	
41	38.9	15.4	91		34.5	141	130,7	52.8	191	177.1	71.5		223.5			269.8	109 0
42	39.9	16.1	92	86,2	34.8		131.9	53,2	92	178.0	71.9		224,4	90,7		270.7	
43	40.8	16.5	94		35,2		132,6	53.9		179.8	72.3		225.3 226 2	91,0	93	271,7	109.8
45	41.7	16,9	95	88.1	35.6	45	133,5	54,3		180.8	72.7	V W. A. L. A. V.	227.2	91.4		272,6	\$525 F S - (96.5) \$514.00
-	-	_	96	89.0		746		The second	95		73.0	-				273,5	110,5
46		17,2	97	89,9	26.2	146	135,4	54.7		181.7 182.7	73.4	246	228.1			274.5	
48	44.5		08	90.9	36.7	47	130,3	55.1	97 98	183.6	73.8	47	229 0			275 4	
40	45.4	18.4		91.8		49	138.2	55.8	99	184.5	74.2	49	229.9	92.9		276,3	
50	46,4	18.7	100	92,7	37.5	150	139.1	56.2	200	185.4	74:0	250	231.8	93,3	200	277.2	112.0
		=	=		=	=	=	=		185.4		==		93,7			
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1 100-9 00-4 51 46-9 19-9 101 93.0 39.5 15.1 33.0 59.0 10 185.0 78.5 251 23.0 98.1 30.8 01.2 53 48.8 10-7 03 91.8 40.5 31 40.8 99.8 10 185.9 78.9 3 1 23.0 98.5 40.6 10.6 1.2 53 48.8 10-7 03 91.8 40.5 31 40.8 99.8 10 185.9 78.9 3 1 23.0 98.5 40.6 10.6 1.2 55 50.6 11.5 03 95.7 41.0 15.1 41.8 60.2 04 187.8 79.7 54 123.8 99.8 10.7 7 05.4 02.7 57 53.5 12.3 0.9 0.9 5.7 41.0 15.1 10.0 47.0 53 51.5 11.9 106 97.0 41.0 15.1 41.8 60.2 04 187.8 79.7 54 123.8 19.9 10.0 10.0 11.0 11.0 11.0 11.0 11.0	D	ift La	at	Dep	10	It L	It D	PD	It La	t De	PD	litt	Lat	De	PO	iff L	at L	ep	Dift	Lat	De	n
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1			200			edi Belis	12000	6000000000	period (Carlotti Carlot	Company of the second	120	53		59	~ 1	3 180				NAME OF TAXABLE PARTY.		
S S S S S S S S S S					THE RESERVE OF			459				54	141.8	60.	Total Control		0	COLUMN TO SERVICE AND ADDRESS OF THE PERSON NAMED IN COLUMN TO SERVICE AND ADDRESS OF		12.75		
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2 51.3 3 52.7 5 54.6 6 55.5 7 06.4 8 57.3 9 08.2 10 09.1 11 10.0 12 11.0 13 11.9 14 12.8 15 13.7 1* 14.6 17 15.5 18 16.4 19 17.4 20 18.3 21 19.2 22 20 1 23 21,0 25 22 8		STATE OF THE PERSONS ASSESSED.		THE RESERVE AND ADDRESS OF THE PERSON NAMED IN	DIII	Lat	Dep		STREET, SQUARE, SALES	STREET STREET, SQUARE,		itt La	- 12 ES 1/				
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5 04.6 6 05 2 7 06.4 8 07.3 9 08.2 10 09.1 11 10.0 12 11.0 13 11.9 14 12.8 15 13.7 1 4.6 17 15.5 18 16.4 20 18.3 21 19.2 22 20 1 23 21,0 24 21 9 25 22 8	31.5	53	48.4		03	94.1	41.9			Section of the section		3 185	4 82	.6	53 23		
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9 08.2 10 09.1 11 10.0 12 11.0 13 11.9 14 12.8 15 13.7 1 14.6 17 15.5 18 10.4 20 18.3 21 19.2 22 20 1 23 21,0 24 21 9 25 22 8	102,8	57	200 100	33.2	07	97.7	43.5		70	1 3		100			56 23		104,1
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13 [1.9] 14 [2.8] 15 [3.7] 1. [4.6] 17 [5.5] 18 [6.4] 20 [8.3] 21 [9.2] 22 [20 [23 [2],0] 24 [21 [9.2] 25 [2.2] 8	04.5	61	55.7	24 8	-	101.4	45,1	-		65,	-			_	0 237		105.7
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20 18.5 21 19.2 22 20 1 23 21,0 24 21 9 25 22 8	27.3	PARTY TO SERVICE	52 1	7.7	18	07.8	48.0	68	CONTRACTOR OF THE PARTY OF THE		17	and the second second	4		7 243	0	08.6
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22 20 1 23 21,0 24 21 9 25 22 8	08.5	-	3.9		-1-	09.6	48.8	70	155,3	69,1	The second second	201,0		50.0	0 246		09.4
24 21 9 25 22 8	03.0		5,82			10.5	49 2	171	156,2	69,5	100	201.9	10 10 10 10	27	1 247	6 1	10.2
25 22 8	09.4			9.7	1.0	124	50.0	72	157,1	70.4	The stage of	202,8	1 3-7.		To a long of the	5 1	10.6
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-0123.81	10.2	National St.	8.53	-	5 1	14.2	50.8	75	159,9	71 2	5. B. S. S. S. S. S.	205,5	91		The state of the s		11.4
	11.0		9.43	1000	75 7 8 8 7 7	15.1	51,2		160,8	71.6	226	206.5	91.9	-			12,2
28 25.6				100 25 20	- A	16.0	51.7		161,7	72.0	27	207,4	92.3		Sales Sa	100	12.7
29 26.5	8.11				30 30	17.8	52.1		163,5	72.4	28	208,3	92.7	100	Contraction of the Contraction o	197 E. E.	3.1
	12.2	to ment to	3 1 3	2.5	30 1	18.8	52.9		164.4	73.2	30	209,2	93,1	86	Company Street	0	3,5
2	12.6	Stanford Williams	A			19.7	53.3	181	165,3	73.6	231	211.0	93.9	281		-	3.9
32 29.2 33 30.1	13.0	82 7	4 9 3 5.8 3	3.3		- 15	53.7		166,3	74.0	32	211,9	94,4		257.	23 14 22 1	4.7
24 21.1	12.8		6.7 3	4.2	33 12		54.1	83	68	74.4		212,8	94,8	83	258.	5 11	5.1
35 32.0	14.2		7.6 34				54,5	85	68,1	74.8 75.2	34 35	213,8	95.2 95.6	84	259.4	11	5.5
36 32,9 1	14.6	86 7	8.6 3	0.0 13	6 12	4,2	55.3		69.9	75.6		215,6	96.0	286	260,	11	
37 33.8 1	50	7 7	9.5 35	,41 3	7 12	5.1	55,7	87 1	70,8	76.1	37	216,5	96 4		261 3	11	6,3
38 34,7 1		88 86	1.3 36	J. A. G. 188		6.1	56.1	88 1	71,7	76 5	38	217,4	90.8	88	263.1	II	7.1
0 36.5 1		90 82	2.2 36			7.9	56.5		72,7	76.9		218,3	97.2	89	264.0	11	7.5
1 37.51	6,7	Control of the last	3.1 37	_		8 8			74,5	77.3		219,2	97:6		264.9		
2 38.4 1	7.1	92 84	.0 37	.4 4		9.71	7.81		75,4	77.7 78.1		220,2	98.0	291	265,8	11	8.3
3 39.3 1		93 85	c 37		3 13	0.6	8.2	93 1	76,3	78,5		222.0	98,8	92	266.7	111	0,8
4 40.2 1		85	,9 38 .8 38		4 13	1.5 5		94 1	77,2	78.9	44	222,9	99.2	94	268.6	110	9.6
6 42.0 18	8.7	6 87	.7 39			5 5 5	9,0	95 1	78,1	79.3		223.8	99.6	95	269.5	120	0.0
7 4 . 9 19	9.1 0	7 88	6 39	4 .4		5	9.4 1	96 I	79,0	9.7	246.	24.7	0.001	296	270.4	120	0.4
8 43.8 19	9,5 9	8 89	.5 39.	48	3 13	5.2 6		98 1	80.9	80.5	47 2		100,5	97	271,3	126	8.0
9 44.8 19	9.9 0	9 90	4 10.	3 49		6.1 6	A CONTRACTOR OF THE PARTY OF TH	991	81,8	80.9	70	27.5	00.9	98	272.2	121	1.2
0 45.7 20					1 3	1000		221-			4914	2/.51	01,71	00	272 1	110	6
t Dep L	0.3 10		4 10.	7 150	137	.0 6	0.0	ift I	82,7	0	49 2		101,3		273.1 274,1	121	The second second

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Difference of	Latitude	and	Departure	for	20	Dec
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Ditt	Lat	Dep	DIII	Lat	Dep	Ditt	Lat	Dep	Ditt	Lat	Dep	Diff	Lat	Lep	Dut	Lat	Dep
	30.4	00.4	51	46.2	21.6	101	91.5	42.7	151	136.9	63,8	201	182,2	84.0	251	227.5	106.1
2		30,8		47.1	22.0	02	92.4	43.1	52	137.8	64.2	02	183.1	85,4	52	228,4	106 .
	1000	31.3	53		22.4	03	93.	43.5		138.7	64,7	03	184,0	85.8			
3		31.7	Strain Strain		22.8	04	20 · 10 · 10 · 10 · 10 · 10 · 10 · 10 ·		53				184,9			2.9,3	Section 1997
4	2 2 2 2	PE Chic 72 19	54	100 100	X		9 . 3	44.0	54	139 6	65,1	04		86.2		230.2	0.00
5	04.5	02.1	55	49.8	-	05	95 2	44.4	55	140.5	65.5	05	185,8	86,6	55	231.1	107.8
6	05 4	02.5	56	50.8	23.7	100	96.1	44.8	156	141.4	65.9	206	186,7	87.1	256	232.0	108.2
7	06.3	03.0	57	51.7	24.1	07	97.0	45,2	57	142.3	66.3	.07	187,6	87.5		232,9	108.6
8	C 1341 1841	03,4	58		24 5	08	97 9	45.6		143.2	66.8		00	87.9		233.8	109.0
	08.2		5.9		24.9	09	98.8	46,1		144.1	67.2	09	189,4	88.3	7 5 1	234.7	109.5
9	09.1	04,2	60	10.2	25.4	10	99.7	46,5	60			10	190.3	88,7			10 St. Sec. 20
10			_	54,4	-	_	39.7	-	-		67,6		90.3		-	-	109.9
11	10.0	04.6	61			III	100.0	46,9		145.9	68.0	211	191,2	89.2	261	236,5	110.3
12		35.0	62	56.2	26.2	12	101.5	47.3	62	146.8	68.5	12	192,1	89.6	62	237,5	110.7
13	11.8	05.5	63	5.7.1	26.6	13	102.4	47.8	63	147.7	68.9	13	193.0	90.0	63	238.4	111.1
14	12.7	05.9	64	58.0	270	14	103.3	48.2	64		69,3		193,9	90,4		239.3	111.6
15	13.6	26.3	65		27.5	15	104.2	48.6	65	149.5	69.7	15	194,9	90.9		240.2	112,0
-	-	-	66	-	-		_		-			-	-	-	-	-	-
16	14.5	06.8	66		27.9	116	105.1	49.0			70.2	216	195,8	91.3		241.1	112.4
17	15.4	07.2	67		28,3	17	106.0	49.4	67	151,4	70:6		196,7	91.7	67	the state of the s	112.8
18		07.6	68	61.6		18	106.9	49,9	68	152,3	71.0	18	197,6	92.1		242.9	113,3
19	17.2	08.0	69		29.2	19	107.8	50.3	69	15322	71.4	19	198.5	92.5	69	243.8	113.7
20	18.1	08.5	70	63.4	29.6	20	108.8	50.7	70	154,1	71.8	20	199,4	93,0		244,7	114,1
-	100	08.9	71		30.0	121	109.7		-			221	200,3		-	-	
21		A-0.5	Des Strange				20000	51,1	171	1550	72.3	221		93,4		245,6	114.5
22		29.3	72		30.4	22	110.6	51.6		155,9	72.7	22	201,2	93.8	Pr. 79	(F) (F) (F) (F)	114.9
23	1 0	09-7	73		30,8	23	111.5	52.0	73	156,8	73.1	23	202,1	94,2			115.4
24	.1 3	10.1	74		31.3	24	112.4	52.4	74	157.7	73.5	24	303,0	94,7	74	248.3	115.8
25	22 7	10.6	75	68.c	317	- 5	113.3	52.8	75	158.6	74.0	25	203,0	95.1	75	249.2	116,2
26	123 €	11.0	76	65.0	12.1	126	114.2	53.2	176	159,5	74.4	226	204,8	95.5	276	250.1	116.6
27		11.4	77		32.5	27	115.1	53.7	77	160,4	74.8	27	m 3 - 1 3 5 5	95,9	77		117.1
28		11.8	78	70,7	1000	28	116.0	54.1	78	161,3	75.2	28	206.6	964		N	117.5
1	6	Page 100	1000	1		PH 13	116.9		3 3	162,2	A COLUMN TO A	100	1		200	The State of the last	
29		12.3	79		33,4	29		54.5	79	E 21 21	75.6	29	207,5	90.8	79	52.9	
10	27.2	12.7	-	72.5	33.8	30	117.8	54.9	- 8c	163,1	76 1	30	200,4	97.2	80	253 0	118.3
31	28,1	13.1	81	73.4	34.2	131	118.7	55,4	181	164.0	76.5	231	209,4	97.6	231	254.7	118,8
32	29.6	1 3.5	82	74 3	34.7	32	119.6	55.8	82	164.9	76.9	32	210,3	98,0	82	255.6	119.2
1 33	1	13.9	83	75.2		33	120.5	56.2	83	165,9	77.3	33	211,2	98.5			119.6
34	1 6	14.4	84	76.1	W. T L.D.	34	121.4	56.6	84		77,8	34	212,1	98.9	82		120.0
	2 2 2 2	1 0	85	77.0		35	122.4	57.1	85		78.2	35	213,0	99.3	85		120
35	-	-		-	-				-	-	-	-	-	-	-	A STATE OF THE PARTY OF THE PAR	-
36	32.6	152	86	77.9	36.3	136	123.3	57,5		168,6	78.6	236	213.0	99.7	286	259-2	120.9
1 37	133.	15.6			36,8		124,2	57 9	87	169,5	79.0	37	214,8	100.2	87	260,1	
38	34,4	16,1	88	79.8	37.2		125.1		88	170,4		38	215,7	100.6	88		121.7
39	The second second	16,5	89	80.7	37.6	39	126.0	58.7		171,3				101.0			122.1
40		16.9		81.6	38,0	40	126.9	59.2	90	172,2	80.3	40	217,5	1014	90	262.8	1226
-	-					-	127.8	59,6	-	-	80.7	-	-	ior.8	-	-	
41		L7-3		8 -	38,5	1.41	129.0							102.3			123.4
42		17.7	92		38,9		128.7			174,0							
43	39.0	18.2	93		39 3		129.6		Sec. 100	174.9	81.6			102.7			123,8
44		18,6			39-7	44			94	175,8	82.0	DESK. THE		103,1			124.2
45	10	19.1	95	86.1	40 1	45	131.4	61,3	95	176,7	82.4	45	232.0	103.5	95	207.4	124.7
46	diam'r.	19,4	1 06	87.0	40.6	146	132.3	61.7	106	177,6	82,8	246	222,9	104,0	296	268.2	125.1
1 1 1		19.9			41.0	47	the formation of the same	62,1		178,5				404.4			125.5
47	1000				41.4	4.8		A		179.4		48		104.8			125.9
48	100 775 7	5 20.3	E 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			100 5 5 5		and the second	0.000	B	84,1			105,2			126.4
49		1 20.7			41.8	49			99	181,3			226.6	105.7	39		126.8
50		3 21.1			42.3	150	135,9		10000	- Charles - Ch	Company of the company	St. Contraction		The second second		-	
Dif	De	Lat	Diff	Der	Lat	Dif	Dep	Lat	Dift	Dep	Lat	Diff	Dep	Lat	FDiff	1 ep	Lat
-	-					-		12	10 2.18	HALL	9-6-17	1111	BUI O	544 10	NOTE	Call dot	
			-					AND ASSESSED OF THE OWNER, THE OW		11 M			and the same of the same of	Value of the latest and the latest a		The state of the last	The state of the state of the

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Dist	Lat	Dep	Dift	Lat	Dep	Dift	La	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Diff	Lat	Dep
1	00.9	00.4	51	45.8	22.4	101	90.8	44.3	151	135.7	66.2	201	180.7	83.1	251	225.t	110.0
2	31.8		52	46.7	22.8	02	91.7	44.7	52	136.6	66.6	02	181.6	88.6	52	226.5	
3	02.7	01.3	53	47.6	23.2	03	92.6	45.2	5.3	137.5	67.1	03	182.5	89.0	53	227.4	
4	03.6	3.10	54	48.5	23.7	04	93.5	45.6	54	138.4	67.5		183.4	89.4	54	228.3	111.4
1 5	04.5	02.2	55	49.4	24.1	05	94,4	46.0	55	139,3	68.0	05	184.3	899	55	229.2	111.8
6	05.4	02.6	56	50.3	24.6	106	95,3	46.5	156	140,2	68.4	206	185.2	90.3	256	230.1	112.2
. 7			57	51.2	25.0	07	96.2	46.9	57	141.1	68.8	07	186.1	907	57	231.0	1127
8	07.2		58	52.1	25.4	08	97.1	47.3		142.0	69.3	08			2 753.00	231.9	and the second
9	1 . 1	03.9	59	53.0	25.9	10	98.0	47.8	59 60	142.9	70.1	09	187,8	91.6	59	232,8	
10	-	04,4	-	53.9	-	-	-		-	-		-			-		
11	10.5	04.8	61 62	54.8	260	111	99.8	48.7	161	144.7	70.6	211	189.6	92.5	261	234.6	
12		85.7		55.7	27.6	12	101.6	49.1	62	145.6	71.0	12	190.5	92.9		235.5	
13		06.1		57.5	28.1	14	102.5	50.0	64	147.4	71,9	14	192.3	93.8		237.3	
15		06.6		58.4	28.5		103.4	50.4	65	148.3	72.3	15	193.2	94.3	65	238.2	
16	-	07.0	1-	59.3	28.9	_	104.3	50.9	166	149.2	72.8	-	194.1	94.7	-	239.1	-
17	15 3	07.5	9	60.2	29,4	17	105.2	51.3	67	150.1	73.2	17	195.0	95.1		240,0	
18	1 -			61.1	29.8		106.1	51.7	68	151.0	73.7	18	195.9	95.6		240.9	property of the second
119	17.1	08.3		62.0	30.2	19	107.0	52.2	69	151.9	74.1	19	196.8	96.0	69	241.8	117.9
20	18.0	38.7	70	62.9	30.7	20	107.5	52,6	70	152.8	74.5	20	197.7	96.4	70	242.7	118.4
21		09.2		63.8	31 1	121	108.8	53.0	171	153.7	75.0	221	198.6	96.9	271	243.6	118.8
22	19.8	09.6		64.7	31.6	22	109.7	53.5	72	154.6	75,4	22	199.5	97,3	72	244.5	ALL THE STREET
23	1	10,1	73	65.5	32.0	23	110.6	53.9	73	155.5	75.8	23	200.4	97.8	1. 3. 7. 1	245.4	
24	Land S. C.	10 5		66.5	3214	24	111.5	54.4	74	156,4	76.3	24	201.3	98.2	74	246.3 247.2	
25	22.5			67.4	32,9			54.8	75	157.3		25	102.2		75		
26	23.4			68.3	33,3	126	113.2	55.2	176	158.2	77.2	226	203.1	99.1	276	and the second	121,0
27	24,3	11.8		69.2	33.8	27	114.1	55.7 56.1	77 78	160.0	77,6	27	204.0	99.5	77	249.0	title and a
29		12.7	79	71.0	34,6	29	115.9	56.6	79	160.9	78.5	100 12	205.	100.4		250.8	
30	27.0	13.2		71.9	35,1	30	116.8	57,0	80	161.8	78.9	0.000	206.7			251.7	
31	-	-		728	35,5	131	117.7	57,4	181	162.7	79.4		207.6	101.3		252.6	
32	28.8	14.0	82	73.7	35-9	32	118.6	57.9	82	163.6	79.8	32	208.5		200	253.5	
33	29.7		83	74.6	36.4	33	119 5	58.3	83	164.5	80.2		209.4			254.4	
34	30.6	14.5	84	75.5	36,8	34	120.4	58.7	84	165.4	80.7	34	210.3	102.6	84	255.3	124.5
35	31.5	15.3	85	76.4	37.3	35	121.3	59.2	85	166.3	81,1	35	211.2	103.0	85	256.2	124.9
36	32.4		86	77,3	37.7	136	122.2	59.6	0.20	167.2	81.5			103.5	286	257.1	125.4
37	33.3	16.2	87	78.2	38.1	37	123.1			168.1	82.0	37	213.C	103,9	87	258,0	125.8
38	34.2	16.7	88		38.6		124.0	60.5		169.0	82.4		213.9	104 3		258.9	
39	35.1 36.0		89	80.0	39.0	39	124.9	61.9	89	169.9	82.9			104.8	09	259,8 260.7	12.7.1
40	-	-		81.8	39,5	40	-	61.8	90		-	-					
41	37.7	18.0	91	82.7	39.9	141	126.7	62.3	191	171,7	83.7	241	210.0	105.7	92	261.6 262.4	128.0
42	37.7	18 0	92	83.6	40.8	42	128.5	62.7	92	173.5	84.6	42	218.4	106.3	92	263.3	128.5
44	39.5			84.5	41.2	44	129.4	63.1	94		85.0	44		107.0	94	264.2	128.9
45	40.4		95	85.4	41.6		130.3	63.6	95	175.3	85.5			107.4	95	265,1	129.3
46	41.3	-	96	86.3	42.1	_	131.2	64 0	196	176.2	85.9	246		107,8		266.0	
	42.2			87.2	42.5	47	132.1		97	177.1	86.4			108.3	97	266.9	130.2
48	43.1	21.0	98	88.2	43.0	48	133.0	64.9	98	178.0	86.8	48	222.9	108.7	98	267,8	130.6
49		21.5		89.0	43.4	49	133.9	65.3	99	178,9	87.2	49	223.8	109,2	99	268.7	1311
50	44.9	21.9	100	89.9	43.8	150	134.8	65.8	200	179.8	87.7	250	224 7	109.6	300	200.6	131.5
Duft	Dep	Lat	Ditt	Dep	Lat	Diff	Dep	Lat	Diff	Dep	Lat	Dift	Dep	Lat	Dif	Dep	Lat
		1			1 11 1		/ 1219	April 1									

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Will!	La	Jep	Din	Lat	Dep	Ditt	Lat	Dep L	Dift	Lat	Бер	Dift	Lat	Dep	irit	Lat	Gep	
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2	-	00.9	52	46.3	23,6	02	90,9	46.3	A STATE OF THE REAL PROPERTY.	1354	69.0		180.0	91.7	_		114,4	
3		01.4			24,3	03	91.8	46.8		136.3	69.5		180,9	92.2	53	225,4	114.9	
4	9 T A S	01.8	1 21	48.1	(B)	04	92.7	47.2		137.2	70.4	05	181.8	92.6	54	226.3	115.3	
_5	04.5		55		25,0	05	93.6	47.7	-		_			93.1	55	-	115.8	
6	05,3		56	49 9	25.4	106	94 4	48.1		139.0	70.8-		183,5	.93,5	256	228.1	116,2	
7		03,2	57	50.8	25.9	07	95.3	48.6		139.9	71,3	08	185,3	94.0	57	229.0	116,7	
8	1 4	03.6	58	52.6		09	97.1	49.5		141.7	72,2	09	186,2	94.9	59	230.8	117.6	-
9	1	04 5	59		27.2	10	98.0	49 9	60	142,6	72.6	10	187.1	95.3	60	231.7	118.0	-
10	-	05.0	61	54,4		III	98.9	50.4	161	143 5	73.1	211	138.0	95.8	261	232,6	118.5	1
11	1 7	05.4	62	55.2	28,1	12	99.8	50.8	62	144.3	73.5	12	188,9	96.2	62	233.4	118.9	1
12	1	05,9	63	56,1	28.6		100.7	51 3		145.2	74.0	13	189.8	96.7	63	234.3	1194	1
14	12.5		64		29.1	14	101.6	51.8		146.1	74.5	14	19017	97.2	64.	235 2	119.9	1
15	13.4	06.8	65	_	29.5	15	102,5	52.2	65	147,0	74.9	15	19176	97.6	65	236.1	120.3	1
16	14,3	07-3	66	58.8	30.0	116	103.4	52.7	166	147.9	75,4	216	192.5	98.1	266	137.0	120.8	1
17	15.1		67		30.4		104,2	53.1	67	148.8	75.8		1	98.5	67	237.9		1
18		08,2			30.9		105.1	53.6		149 7	76.3	18		99.0	68	238.8	1 1 1 1 1 1	1
19		08,6			31.8		106.0	54,0		150.6	76.7	19	1	99.4	70	239.7		1
20	-	09,1		-	-		-	54.5	70		-	-	-				-	1
21		09.5			32.2	121	107.8	54.9	171	152.4	77.6	221	1 0	100.8	72	241.5	1 2.2	1
22		10.4		65.0	32.7	22	109.6	55.4	72	153.3 154.1	78,5	23	0	101.2	73	243.2	1 0.0	1
23		109			33.6	24	110.5	56.3		155.c	79.0	24	1 .	101,7	74	244.1		1
24	22.	Maria de la	/ / / /	166 0		25	1114	56.8	75	155,9	79.5	25		102,2	75	245,0		1
$\frac{25}{26}$	-	11.8				126	112.3	57.2	176	156.8	79.9	226	201.4	102.6	276	245.9	125.3	1
27		12.3		68.6			113.2	57.7	77	157.7	80.4			103.1	77	246.8		1
28,	1	12,7			35.4		114,0	58,1	78	158.6	80.8		203 1	103.5	78	247.7		1
29	25.	3 13.2			35.9		114.9	58.6	79	159 5			the state of the state of	104,0	79	248.6	100	1
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31		6 14.1		100000000000000000000000000000000000000			116.7	59,5	181	161,3				104.9	281	250.4		- 0
32		5 14,5				32	117.6	59.9	82	162.2				105.8	82	251.3		
33	29.	The State of	-		37.7		119.4	60.8	84	163.9			0	106.2		253.0		
34	30.				0 6		120.3	61,3	85					106.7				
35	-				6 39.5		121.2	61.7	186	165.7	-	-	210.3	107.1	286			
36	32.	16,		1	39.0		122,1	62.2	87	166,6	84.9	37	211.2	107,6	87			1
37		9 17.		78.	4 40.4		123.0	the same of the same		167,5	85.4	1 38		108.1	88		5 130.8	1
39	134	7 17.7	89	19,	3 40,9	39	123.8	63,1	89		85.8	39	212,9	108,5		257.	5 131.2	1
40		6 18,	2 90	80.	2 40,	40	124.7	63,6	90	169.	-		213,8	109.0	90	258.4	4 131.7	
40	36.	5 18.	6 91		141.		125.6	64.0		170.2			214.7	109,4		259.	3 132.1	
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39 34 4 18.3 89 78.6 41.8 39 122.7 65.3 89 100.9 82.7 39 211.0 112.2 85 255.2 135.7 40 35.3 18.8 90 79.5 42.3 40 123.6 65.7 90 167.8 89.2 40 211.9 112.7 90 256 1 136. 41 36.2 19.2 91 80 4 42.7 141 124.5 66.2 191 168.7 89.7 241 212.8 113 1 291 257.0 136.6 42 37 1 19.7 92 81.2 43.2 42 125.4 66.7 92 169.5 90.1 42 213.7 113.6 92 257 8 137.1 43 18.0 20.2 93 82.1 43.7 43 126.3 67.1 93 170 4 90.6 43 214.6 114.1 9 258.7 137.6 44 38.9 20.7 94 83.0 44.1 44 127.2 67.6 94 171.3 91.1 44 215.5 114.6 9. 259.6 138.0 45 39.7 21.1 95 83.9 44.6 45 128.0 68.1 95 172.2 91.9 45 216.3 115.0 95 260.5 138.5	37	32.7	17.4	87							165.1					87	253.4	134.7
40 35.3 18.6 90 79.5 42.3 40 123.0 65.7 90 107.8 89.2 40 211.9 112.7 90.2 50 1136.0 41 36.2 19.2 91 80 4 42.7 141 124.5 66.2 191 168.7 89.7 241 212.8 113 1 291 257.0 136.6 42 37 1 19.7 92 81 2 43.2 42 125.4 66.7 92 169.5 90.1 42 213.7 113.6 92 257 8 137.1 43 18.0 20.2 93 82.1 43.7 43 126.3 67.1 93 170 4 90.6 43 214.6 114.1 9 258.7 137.6 44 38.9 20.7 94 83.0 44.1 44 127.2 67.6 94 171.3 91.1 44 215.5 114.6 9. 259.6 138.0 45 39.7 21.1 95 83.9 44.6 45 128.0 68.1 95 172 2 91.9 45 216.3 115.0 95 260.5 138.5	38	177 8	18.2	82	77	641.3	38					88.7	30			80	255.3	135.2
41 36,2 19.2 91 80 4 42.7 141 124.5 66.2 191 168.7 89.7 241 212.8 113 1 291 257.0 136.6 42 37 1 19.7 92 81.2 43.2 42 125.4 66.7 92 169.5 90.1 42 213.7 113.6 92 257 8 137.1 43 18.0 20.2 93 82.143.7 43 126.3 67.1 93 170 4 90.6 43 214.6 114.1 9 258.7 137.6 44 38.9 20.7 94 83.0 44.1 44 127.2 67.6 94 171.3 91.1 44 215.5 114.6 9. 259.6 138.0 45 39.7 21.1 95 83.9 44.6 45 128.0 68.1 95 172.2 91.9 45 216.3 115.0 95 260.5 138.5			18.8	00								89.2				90	256 1	135.7
42 37 1 19.7 92 81.2 43.2 42 125.4 66.7 92 169.5 90.1 42 213.7 113.6 92 257 8 137.1 43 18.0 20.2 93 82.1 43.7 43 126.3 67.1 93 170 4 90.6 43 214.6 114.1 9 258.7 137.6 44 38.9 20.7 94 83.0 44.1 44 127.2 67.6 94 171.3 91.1 44.215.5 114.6 9. 259.6 138.0 45 39.7 21.1 95 83.9 44.6 45 128.0 68.1 95 172 2 91.9 45 216.3 115.0 95 160.5 138.5	40		-				_		-			Contract Con	200 A	-	-	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		-
43 18.0 20.2 93 82.1 43.7 43 126.3 67.1 93 170.4 90.6 43 214.6 114.1 9 258.7 137.6 44 38.9 20.7 94 83.0 44.1 44 127.2 67.6 94 171.3 91.1 44 215.5 114.6 9. 259.6 138.0 45 39.7 21.1 95 83.9 44.6 45 128.0 68.1 95 172.2 91.6 45 216.3 115.0 95 260.5 138.5			10.7								160.5	90.1		212.7		02	257 8	130.0
44 38.9 20.7 94 83.0 44.1 44 127.2 67.6 94 171.3 91.1 44 215.5 174.6 9. 259.6 138.0 45 39.7 21.1 95 83.9 44.6 45 128.0 68.1 95 172 2 91.6 45 216.3 115.0 95 260.5 138.5			:0.2	9	82.	1 43.7	43	126.2	67.1	92	170 4	90.6	43			9	258.7	137.6
45 39.7 21.1 95 83.9 44.6 45 128.0 68.1 95 172 2 91,9 45 216.3 115.0 95 260.5 138.5		1 0			1 83.	0 44.1	44	the state of the s			171.3	91.1	44	215.5		9.	259.6	138.0
					5 33	9 44.6	45	128.0	68.1	4				216.3			260.5	138.5
46 40.6 21,6 96 84,8 45 1 146 128.9 68.5 196 173.1 92.0 246 217.2 115.5 296 261,4 139.0				-	6 84	8 45.1			68.			-	-		-	-	261,4	130.0
47 41.5 22.1 97 85.7 45.5 47 129.8 69,0 97 174.0 92.5 47 218.1 115.9 97 262.3 139 4		41.	22.1	9	85.	7 45.5	47	129.8	69,0	97	174.0	92.5	47	218.1	115.9	97	262.3	139 4
48 42 4 22.5 98 86.5 46.0 48 130.7 69.5 98 174,8 93.0 48 219.0 116.4 98 263.1 139.9	48	42	22.		8 86.	5 46.0	48	130.7	69.5	98	174,8	93.0	48	219.0	116.4	98	263.1	139.9
49 43 3 23.0 99 87 4 46.5 49 131.6 70.0 99 175.7 93.4 49 219 9 116.9 99 264.0 140.4			3 23.0	99	9 87	4 46.	49	131.6	70.0	99	175.7	93.4	49			99	264.0	140.4
50 44.2 23.5 100 88.3 47.0 150 132.5 70.4 200 176.6 93.9 50 220.8 117.4 300 264.9 140.9	. 50	44.	2 23.5		88.	3 47.0	150	132.	70.4	200	170.6	93.9	50	220.8	117.4	300	204.9	140.9
Dift Dep Lat	Di	R De	Lat	Di	ft De	p La	Dif	Dep	Lat	Dif	Dev	Lat	Dif	Dep	Lat	Diff	Dep	Lat

for 62 Deg.

Difference of Latitude and Departure for 29 Deg.

216 6120

29

N. T.													A STATE				
Dift	Lat	Dep	Dift	Lat	mep	Dift	Lat	Dep	Dift	Lat	Dep	Ditt	Lat	Dep	ilt	Lat	Dep
1	00,9	00.5	51	44.6	24 7	101	88.3	49,0	151	132,1	73,2	201	175.8	97.4	251	219.5	121.7
1000	01,7				25.2	02	89.2	49.4		132.9	73.7	02	176.7	97.9	52	220.4	122.2
2	02.6	The second	1 1 2 1 1 1 1 1		25.7	03	90.1	49.9	53	133.8	74.2	03	177.5	98.4		221,3	122.7
3	5.571 3.78		53	47.2		04	91.0	50.4	1 1/2 1 1			04	178.4	98.9	53	222,2	
4	03,5	1 1 1 1 1 1 1	54		26.7		91.8	50 9	54	134,7	74.7	05		A CONTRACTOR OF THE PARTY OF TH	54		123.1
5	04.4	-	55	-	-	05		-	55	135 6	75.1		179,3	99 4	55	223,0	123.6
6	05,2	02,9	56		27,1	106	92.7	51,4	156	136 4	75,6	206	180,2	99.9	256	223.9	124.1
7	06,1	03.4	57	49.9	27.6	07	93,6	51,9		137.3	76 I	07	181.0	100,4	57	2248	124.6
8	07.0	039	58		28.1	08	94.5	52.4	58	138.2	76.6	08	181.9	100.8	58	225,6	125.1
9	07.9		59	51.6	BERTHAMPIN	09	95.3	52.8	59	139.1	77.1	09	182.8	101.3	. 59	226.5	125.6
10	08,7	04,8	60	52.5	29,1	10	96.2	53.3	60	139.9	77,6	10	183,7	101.8	60	227,4	126.0
11	09.6	05.3	61	53.4	29.6	III	97.3	53.8	161	140 8	78.1	211	184.5	102.3	261	228.3	126,5
12	10 5	0	62		30,1	12	98,0	54.3	62	141.7	78,5	12	185,4	102,8	62	229,1	127.0
13		06.3	63		Marie Control of the Control	13	98.8	54.8	63		79.0	13	186,3	403.3	63	2300	127.5
14		06.8	64		31.0	14	99.7	55.3	64	143 4	79,5	14	187 2	103 7	64	230.9	128.0
15		07.3	65	56.8	31,5	15	100.6	55.8	65	144.3	80,0	15	188,0	104.2	65	231,8	128.5
-	-	a y residence de	-			116	IOI	56,2	-		80.5	-	188,9		-	400	-
16	14,0	07.8	66	57.7		1	101.5		166	145.2	81.0		189.8	104.7	266	232,6	129,0
17	14.9	08.2	67	58,6			7 11 2 3	56.7	67				A 124 18	105,2	67	233 5	129.4
18		08,7	68	10	33,0	18	103.2	57.2	68	146.9	81.4		190.7	105.7	68	234.4	129.9
19	1	09,2	69		33.5	19	104,1	57.7	69	147,8	81,9	19	191.5	106.2	69	235.3	130.4
20	17,5	-	70	51.2	33,9	20	105.0	58.2	70	148.7	82.4	20	192.4	106.7	70	236.1	130.9
21	18.4	10.2	71	62.1	1	121	105.8	58.7	171	149 6	82 9	221	193,3	107,1	271	237.0	1314
22	19,2	10.7	72	53.0	34.9	22	106.7	59.1	72	150.4	83.4	22	194.2	107.6	72	237.9	1319
23	20.1	11.2	73	63.8	35.4	23	107.6	59.6	73	151 3	83.9	23	195.0	108.1	73.	238.8	132,4
24	21.0	11.6	74		35,9	24	108.5	60,1	74	152.2	84.4	24	195,9	108.6	74	239.6	132.8
25	21,9	12.1	75	65.6	36.4	25	109.3	60.6	75	153.1	84.8	25	196,8	109.1	75	240.5	133.3
26	22.7	12.6	76	66.	36.8	126	110.2	61.1	176	153.0	85.3	226	197,7	109.6	276	241.4	133.8
27		13,1	77		3 37.3	27	111.1	61.6	77	154 8	85.8	27	198.5	110.0	77	242,3	134.3
28	24,5		78		37.8	28	111.9	62.1	78	155,7	86.3	28	199,4	110,5	78	243.1	134.8
20,	25 4	1	79		38.3		112.8	62.5	79	156.6		29	200,3	111,0	79	244.0	135.3
	1 -	14.5	80	70.0	38.8	30	113.7	63 0	80	157.4	87.3	Dec. 100	201.2	111.5	80	244,9	135,7
30	-	-	-			-		-	-		-	30			_	-	-
31	1:7.1		81				114,6	63.5	181	158.3		231	202.0	112,0	281	245,8	136.2
1 3-	128.C	1	82				1154	64.0	82	159.2	88.2	32	202 9	112.5	82	246.6	136.7
1 33		16.0		de la constitución de	6 10.2		116.3		83	160.1	88.7	33	203.8	113.0	83	247.5	137,2
1 34	29.7				5 40.7		117.2	65.0	84	160.9	No. of Contract of	34	204.7	113.4	84	248.4	
35	30,1	17.0	85	14.	3 41.2	1 33	118 1	65.4	85	161.8	89.7	35	205.5	113,9	85	249.3	138,2
36	31.5	17.5	86		2 41.7		118.9		186	162,7	99.2	236	206,4	114.4	286	250.1	138,7
37	32 4	17.9		76,	1 42,2	37	119.8	66.4	87	163.6	90.7	1 27	1207.3	114.9	87		
38	33 2	18.4	88	177.	0 42.7	38	120.7	66.9	88	164.4	91.1	1 38	208,2	115,4	88	251.9	139.6
39	34.	1 18.9	89	77.	8 43.1	39				165.3		39		115.9	1 89		
40		19.4		78.	7 43.6	40	122.4	The state of the s		166,2		40	1			253.6	
41	-	19.9	-	- Inches	6 44,		123.3	-	-	-	-	-	0	-		254,5	-
		20.4			5 44,		T24.2			167 9	93.1	241	1 - 3 - 2 - 3 -				141,6
42	30.	6 20.8	92	81	3 45.	43		The state of the s		168.8	93.6	A 15 TO 1		117 8			142.0
43					2 45.	43			93	169.7	93.0		March State of State	118.3	93		
44		5 21,3			1 46.	44	120.8	70.3		A		1		118.8		258,0	142.0
45	-	21.8	-					-				-			-		
46	40	2 22.3	96	84.	0 46.	5 146	127.7	70.8		171.4	95.0		215,2	119.3		258.9	143.5
47	41.	1 22,8		84,	8 47,	47	128	77.	97	172.3	95.5	47	216.0	119.7			144.0
48	42.	0 23.3		85.	7 47.					173:2	96.0	48	210.0	120.2			
49	42.	9 23.8	99	186,	6 48,					174.0	96.	1 40	217,8	120.7		261,5	145.0
50		7 24.2	100	87.	5 48.	150	131.				97.0	250	218.7	121.2	300	262.4	145.4
0	+ 100	I at	D:	(De	p La	-	t Dep	Tat	Die	Den	Lat	Die	Dep	Lat	Dif	Den	Lat
DI	CIAJE	plLat	Juli	(IDE	PLLa	וועון	прер	Lat	Jun	(Joeb	Lat	1011	il och	Lat	TON	H Dep	, Lat
												1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1		Mark to the Contract of			T. Alisan

Ditt	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep	Dik	Lat	Dep	Dift	Lat	Dep
1	00.9	00 5	51	44.2	25.5	101	87 5	50.5	151	130.8	75.5	201	1741	100.5	251	2174	125.5
2	01.7	01.0	52	45.0		02	88.3	51.0	52	131.6	76.0	C2	174 9	101.0		218.2	126.0
3	1. 1. 1.1	01.5	53	45.9		03	89.2	51.5	53	132.5	76.5	03		101.5		219.1	126.5
1 4	3.5	02,0	54		27.C	04	90,1	52.0	54	133 4	77.0	04	175.7	102.0	54	1 2 2 3 1 1 1	127.0
5	04.3	2.5	55	47 6	-	05	90,9	52.5	55	134.2	77.5	.05	177.5	102,5	55	220.8	127.5
6	1	03 0	56	48.5		106	91.8	53.0	156	135.1	78,0	206	178.4	103.0	256	221.7	128.0
8	06 0	03,5	57	49 4	28,5	07	92.7	. 53.5	57	136.c	78.5	07	179 3	103.5	57	222.6	128.5
	07.8	04.0	58	50.2	29.0	80	93,5	54.0	58	136.8	79.0	Carl Carl	180.1	104.0	58	223.4	129.0
10	0.7	05.0	60	52 0		10	94.4	54.5	59 60	137.7	79.5	09	181.0	104.5	59	224.3	129 5
11	09 5	-	61	52.8	-	-	-			-	-	-	_	-	-	225.2	130.0
12	10.4	06.0	62	53.7	31.0	111	96.1	55.5	16 ₁	139.4	80.5	211	182.7	105.5	261	226.0	130.5
13	11.3	06.5	63	54.6		13	97.0	56.5	63	141.2	81,5	12	183 6	106.5	A PART OF	226.9	1310
14	12.1	07,0	64	55 4	32.0	14	98.7	57 0	64	142.0	82.0	14	185.3	107.0		227 8	131.5
15	13.0	27,5	65	56.3	32.5	15	99.6	57.5	65	142.9	82.5	15	186.2	107,5	65	229.5	132.0
16		08.0	66	57.2	330	116	100.5	58.0	166	143.8	83.0		187.1	-	266	-	-
17		08.5	67	58.c	33.5	-17	101.3	58.5	67	144.6	83.5	17		108.5	67		133.0
18	1	09.0	68	58.9	34,0	18	102.2	59.0	68	145.5	84.0	18		109.0		232,1	133.5
19	16.5	9.5	69	59 8	34 5	19	103.1	59 5	69	146,4	84.5	19	189.7	109.5		233.0	1 34.5
20	17.3	10,0	70	00,t	35.0	20	103.9	60.0	70	147.2	85.0	20	190.5	110.0	70	223.8	135,0
21	18.2	10.5	71	61.5	35.5	P2 1	104.8	60.5	171	148.1	85.5	221	191.4	110.5	271	234.7	135.5
22	19.1	0.11	72	62.4	36.0	22	105.7	61.0	72	149.0	86.0		192 3		72	2356	36.0
23		11.5	73	63.2	36.5	23	106,5	61.5	73	149.8	86.5	23	193.1	111.5	73	236.4	136.5
24	20.8	12.5	74	64.1	37.0	34	107.4	62.0	74	150,7	87.0		194.0	112.0	74	237.3	137,0
25	-		75	65,0	37.5	25	108.3	62.5	75	151.6	87.5	25	194.9	1 1 17 17	75	238.2	137,5
26	23.4	13.0	76	65.8	38,0 38.5	126	109,1	63,0	176	152.4	88.0	226	195.7		276	239.6	138.0
28	24.2		77 78		39.0	27 28	110.0	63.5	77 78	153.3	88. ₅ 89.0	27	196,6	113.5	77	239.9	138.5
29	25.1		79	68.4	39.5	29	111.7	64.0	79	154.1	89.5	28	197.4			240.7	139.0
30	1 2	1000	80		40.0	30	112.6	65.0	80	155,9	90.0	20	199.2		1 79 8c	241.6	139.5
31	26.8	15.5	81	70,1	40 5	131	113.4	65 5	18	156.7	90.5	-	200.0		281	-	
32		16.0	82	71.0		32	1143	66.0	82	157.6	91.0	32	200.9		82	243.3	140,5
33	28.6	16.5	83	71.9	41.5	33	1152	66.5	83	158,5	91.5	33	201,8		83	245.1	1
34	29.4	17.0	84	72 7		34	116.0	67.0	84	159.3	92.0	34	202.6	117.0	84	245.9	142.0
35	303	17.5	8 =	73,6	42.5	35	116.9	67.5	85	160.2	92.5	35	203.5	-	85	246.8	142.5
36	31.2		86		43.0		117.8	68.0	186	161.1	93.0	236		118.0	286	247.7	143.0
37		18.5	87	75.3	43.5		118.6		87	161.9		37		118.5	87	248.5	143.5
38	32.9	19.0	88		44 0	2.5 6	119.5	69.0	88	162.8				119.0	88	249.4	144.0
39	34.6	20.0	90		44.5	39	120.4	69,5	89	163.7	94.5		207.0	119,5		250.3	144.5
40	_		-			40	121.2	70.0	90	164.5	95.0	40	-	120.0	90	251.1	145.0
42	35·5 36.4	21.0	91	79.7	45.5		122.1	70.5	191	165.4	95.5	241		120.5		252.0	145.5
43	37.2		93	80.5	46.5	42	123.8	71.0	92	166.3	96.0			121.0		252.9	146.0
44	38.1		94	81.4	47,0	44	124,7	72.0	93 94	168.0	97.0	43		122.0		253.7	146.5
	39 0		95	82.3	47,5	45	125.6	72.5	95	168,9	97.5	45		122.5		254.6	147.0
45 46	39.8	-		83.1	48.0	146	126.4	73,0	196.	169.7	98.0	246	213.0		-	255.5	147 5
47	40.7	23.5	97	84.0	48.5	47	127.3	73.5	97	170.6	98.5	47	213.9			256.3	148.0
48	41.6		98	84,9	49.0	48	128.2	74.0	98	171,5	99.0	48	214.8	124.0	98	258.1	149.0
49	42.4	24.5	99	85.7	49.5	49	129.0	74.5	99	172.3	99 5	40	215.6	124.5	99	253.9	149.5
50	43 ·3	25.0			50.0		129.9	75.0		173.2	100.0	250	216.5	125.0	300	259.8	150.0
Dift	43.3 Dep	La	Dift	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat		Dep	Lat
N. F				1.00													Dat

		78000	(X:04)	Lati	Land	Sal	Latt	Dep	Dift	Lat	Den	Dift	Last	Doub	v:al	1 1	De
Ditt	Lidi	Dep	Dift	-	Dep	Dill	Lat	-		Lat	Dep	Din	Lat	Dep	Oilt	Lat	Dep
1	00,9	00.5	51		26.3	101	86,6	52.0	151	129	77,8	201	172.3	103.5	251	215,1	129.3
2	1. 2.	01.0	52	44.6	26.8	02	87.4	52.5	52	130.3	78.3	02	173.1	104.0	52	216.0	129.8
	22.6	76. 77.		45.4		03	88.3	53.0		131.1	78,8	03	174.0	104.5	53	216.8	130.3
3	03,4		33	46.3	27.8	04	89.1	53.6		132,0	79.3	04	174.8	105,1	54	217,7	130.8
4		02,6	54	47.1		05	900	54.1		132.8	79,8	05	175.7	105.6	55	218.5	131,3
5 6		-	55	48.0								_		-		-	Fifth Committee of
6	05,1		3			106	90.8	54.6	156	133.7	80,3		176.5	106.1	256	219.4	131,8
7	06,0		31	48.8		07	91.7	55.1	57	134,5	80.9		177.4	106.6	57	220.2	132.4
8	06.9		58	49.7		08	92.6	55.6	58	135 4	81.4	08	178.3	107,1	58	221,1	132.9
9	07.7		59	50.6	30,4	09	93,4	56,1	59	136.3	81.9	09	179,1	107.6	59	222,0	133.4
10	08,6	05.2	60	51.4	30,9	10	94.3	56.7	60	137.1	82.4	10	180,0	108.2	60	222.8	133.9
-	09.4	05.7	61	52.3	31.4	111	95.1	57.2	161	138.0	829	211	180.8	108.7	261	223.7	134.4
11		06.2	62	53.1	31,9	12	96.0	57.7	62	138.8	83.4	12	181.7	109.2	62	224 5	134.9
12		06.7	63	54 0	32.4	13	96.8	58.2	63	139.7	83.9	13	182.5	109.7	63	225,4	135.4
13	124	27.2	64	1		14	97.7	58.7	64	140.5	84.5	14	183,4	110.2	64	226.2	136.0
14		07.7		55.7	33,5		98%	59.2	65	141.4	85.0	15	184.3	110,7	65	227,1	136.5
15		-	65	-	-	15			-		-	-	-		-		
16	13.7	28.2	66	56,6		116	99.4	59.7	166	142,3	85.5	216	185,1	111,2	266	228,0	137,0
17	14,6	08,8	67		34.5	17	100.3	60,3	67	143.1	86 0	17	186,0	111.8	67	228.8	137,5
18	15.4	29,3	68		35.0	18	101.1	60.8	68	144.0	86.5	18	186.8	112,3	68		138,0
119	16,3	09.8	69	59.1	35,5	19	102,0	61.3	69	144.8	87.0	19	187.7	112.8	69	230.5	138,5
20	17,1	10.3	70	60.0	36.1	20	102.8	61.8	70	145 7	87.6	20	188,5	113.3	70	231,4	139,1
	18.0	10,8	71	60 8	36.6	121	103.7	62.3	171	146 5	88.1	221	189.4	113.8	271	232,2	139.6
21		11.3		61.7		22	104,t.	62.8	72	147,4		22	190.3	114.3	72	233.1	140.1
22	19,7	1 0	72.	200	37.6		105.4	63 3	73	148.3		100	191.1	114.8	73	234 0	140.6
23			73		38.1		106.3	63.9		149 1	89.6	24	192.0	115,4		234.8	141.1
24		12.4	74	64 3	0 1	24	107.1	64 4	74	150 0	90.1	25	192,8	115.9	74	234.0	1 8 1
25	21.4	12.9	75	-	-	25			75			-3		_	75	235 7	141,6
26	22.3		76	65.1		126	108.0	64.9	176	150.8	90.6	226	193,7	116.4	276	236.5	142.1
27		13.9	77		39.7	27	108.8	65.4	77	1517	91.2	27	194.5	116.9	77	237.4	142.7
28	134,0	14.4	78		40.2	28	109.7	65.9	78	152.5	91.7	28	195.4	117.4	78	238.2	143,2
29	24,9	14,9	79	67,7	40.7	29	110.6	66.4	79	153.4	92,2	29	196,3	117.9	79	239.1	143.7
30	25 7	1		68.6	41.2	30	111.4	67.0	80	154 3	92,7	30	197,1	118.5	80	240.0	144.2
		16.0	81	69.4	41.7	131	112 3	67.5	181	155,1	93.2	231	198,0	119.0	281	240.8	144.7
31		16.5			42,2		113.1	68,0	82	156.0	93.7	32	198.8	119.5	82		145.2
1 32	1000	17.0	A STATE OF		42.7		114,0		83	156.5	94.2		199,7	120.0	183	242,5	
33		1		4	3700	33	114.8	69.0	84	157.7	94,8	33	200,5	120.5	84		146.3
34	29.1	0				34	115.7	69.5	1 0	158.5	06.2	34	201.4	121.0	85	243 4	146.8
35	30,0		- 3		-1-3	-	_		-	The second second		35			-	244.2	-
36		18.5	86	73.7	44,3	136	116.6	70.0	186	159.4		236	202 3	121.5	286		147,3
37	31.7	19.1	87	74.	6 44,8	37	117.4		87	160 3	96.3		203.1	122.1	87	246.0	147,8
38	32 6	19.6		75 4	4 45.3		118.3					38	204.0	122.6		246,8	148.3
39	33 4	20.1	89	76,	3 45.8	39	119.1					39	204.8	123.1	89	247.7	148.8
40		20.6	90		146.4	40	120.0	72.1	90	162,8	97.9	40	205.7	123.6	90	248.5	149.4
-		21,1	-	0	46.	-	120.8	72,6			98.4		206,5	124.1		249.4	
41	26.0	21.6	91	78	8 47,4	42	121,7		92	164.5			207 4				150,4
42	26.0	22.1	92	70	7 47.9	43	122.6							125.1		251 1	
43	30,9	22,6			6 48,	1 43	123.4			1	99.9			125.6	1 1	252.0	
44	1 0 /			10	4 48.	45	124.				100,4			126.2		252,8	
45		23.2	25 STREET, 198	-	-	-		-	-				0	-	-		
46	39.4	33.7			3 49,4	146	125.1				100.9	246		126,7	296	253.7	
47	40.3	3 24.2	97	83.	1 50.6		126.0	75.7	97		101.5	47	211.7	127.2		254,5	
48	41.1	1 24.7			50	48			98	109.7	102.0	48	212,5	127.7			153.5
49		25.2	99	84,	8 51,0	49	127.	76.7	99	170.5	102,5	40	213,4	128.2			154,0
50		25.8	100	85.	7 51,5	150	128.6	77.3	200	171.4	103.0	250	214,3	128.8	300	257,1	154.5
=										Dep			Dep	Lat		===	
Dil	timet	plLat	וועוי	tine	pi La	וועוו	tl Dep	Lat	וועו	и Бер	Lat	1011	прер	Lat	Diff	l Dep	Lat
2 2 2 2		1 74 17 17															

1.700																J	10.5
Dift	Lat	Dep	Dift	Lat	Dep	Ditt	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep
1	00.8		51	43,2	27.0	101	85.6	53.5	151	128.0	80,0	201	170.4	106.5	251	212.8	133.0
2	01.7		52		27.6	02	86.5	54.1	52	128.9	80.6		171,3			213.7	133.6
3.	02.5			44.9	28.1	03	87.3	54.6	53	129.7	81.1	03	172.1		53	214.5	134.1
4	03.4	1 137				04	88.2	55.1	54	130.6	81,6		17.3.0			215.4	134.6
_5	04.2		55	46.6	-	05	89.0	55.7	55	131.4	82.2	05	173.8			216.2	135,2
6	05.1	199	56	47 5 48.3	29.7	106	89,9	56.2	156	132.3	82.7		174 7			217.1	135.7
7 8	05.9			48.3	30.2	07	90,7	56:7 57 2	57	133.1	83.2 83.7	08	175.5			217.9	136.2
9	07.6			50.0	31.3	co	92.4	57.8	58 59	134.8	84.3	100	177.2			218.8	136.7
10	08.5		60			10	93,3	58.3	60	135.7	84.8		178.1			220.5	137,3
11	09.3		61	517	32.3	111	94.1	58.8	161	136.5	85.3	211	178.9	111.8	-	221.3	138.3
12	10.2			52 6	32.9	12	95.0	59.4	62	137.4	85.9	12	179.8			222.2	138.9
13	0.11	6.9	63	53 4	33 4	13	95.8	59 9	63	138.2	86.4	13	180.6				139.4
14	11.9		64	54.3		14	96.7	60.4	64	139.1	86.9	14				223.9	139.9
15	12.7		65	55.1	34,5	15	97.5	61.0	65	139.9	87.5	15	182.3		65	224.7	140.5
16	13.6		200	55.9	35.0	116	98 4	61.5	166	140.8	88.0	216	183 2			225.6	141.0
17	14,4	A SKIP AND	67	56.8		17	99.2	62.0	67	141.6	88.5		1,200		- / /		141.5
18	16.1		68	57·7 58.5	36.0	18	100.9	62.5	68	142.5	89.6	18	184.9			227.3	142 0
19	17.0		70	59 4	37.1	20	101.8	63,1	7	143.3	90.1	20	186.6			228.1	142.6
-	17.8	-		60,2	-	-	102.6	64.1		-	90.6	-	187.4	-	_		143.1
21	18.7		71 72	61.1	38,2	121	103.5	64.7	72	145.0	91.2		188.3			229.8	143.6
23	0.0	12.2	73	61.9		23	104.3	65.2	73	146,7	91.7					230.7	144.2
24	1 N 10 10 10 10 10 10 10 10 10 10 10 10 10	12.7	74	62.8	39.2	24	105.2	65 7	74	147.6	92:2	24	190.0		10.00	232,4	145.2
25	21.2	13.3	75	63.6	39,8	2.5	106,0	66.3	75	148.4	92.8	25	190.8	119.3		233.2	145.8
26	22.0	13.8	76		40.3	126	106.8	66.8	176	149.2	93.3	226	191.6	119,8	-	234.0	146.3
27	22.9		77	65,3		27	107.7	67.3	77	150,1	93.8	27	192 5	120.3		234.9	146.8
28		14.8		66 1		28	108.5	67.8	78	1 50.9	94.3		1 Sec. 128. 128. 128.	120.8		235.7	147.3
29		15.4	79	67.0		29	109,4	68.4	79	151.8	94.9	29	194.2			236.6	147 9
30	-	15.9		-	-	30	110.2	-	80	152.6		20	-	121.9	8c	237.4	148.4
31	-	16.4	81		42.9	131	111.1	69.4	181	153.5	95.9	-		122.4	1000000	238.3	148.9
32	28.0	17.0	82		43.5	32	111.9	70.0	82 83	154.3	97.0			123.0			149.5
34	28.8		84	71.2	44.5	34	113.6	71.0	84	156,0	97.5			124.0	84	240.0	150.0
35	1	18.6	85	72.1	45.1	35	114 5	71,6	85	156.9	98.1	35	199.3	124.6		241.7	150.5
36	-	19.1	86	72.9	45.6	136	115 3		-	157.7	98.6			125.1			-
37	31.4	19.6	87	73,8	46.1	37	116.2		87	158,6	99.1	37	201.0	125.6	87	243.4	152.1
38	32.2	20.1	88	74.6	46.6	38	117.0	73,1	88	159.4	99.6	38	201,8	126.1	88	244.2	152.6
39	33.1	20.7		75.5			117 9	73.7		160.3			202.7		89	245.1	153,2
40	33.9	21.2	90		47,7		118.7	74.2	90		100.7		203.5	127.2	90	245.9	153.7
41	34.8	21.7	91	77 2	48.2		119.6	74.7	191		101.2				291		154,2
42	35.6	22,3	92	78.0	48.8	42	120.4			162.8	101.8		205.2			247.6	154.8
43	36.5 37·3	22.2		70.7	49.8		121.3	75.8		163.7	102,8		The Market State of the Control of t	128.8		248.5	155.3
2.5	38.2	23.0	94	80.6	50.4	44	123.0		94	165.4	103.4	44		129.9		249.3	155 8
45	38.2			-	50.9				-	166.2			208.6		1	250.2	
47	39.9		96	82.2	51.4	47	123.8	77.4		167.1	104.4	47	209.5				156.9
48	40.7	25.4	98	82 1	51.9	48	125.5				104.9		210.3			251.9	157.4
49	41.6		99	84.0	52.5	49	126 4		99	168.8	105.5	49	211.2			253.6	158.5
50	42.4				53.0		127.2	79.5		169.6	106.0	250	212.0			254.4	
-	Dep	La	Dift	Den	Lat	Diff	Dep			Dep	Lat	Ditt	Dep	Lat		Dep	Lat
			-				r		12/11			12.110	- 47	1 2500	,Dill	Тер	1 Lat

Difference of Latitude and Departure for 33 Deg.

33

			-														77
Ditt	Lai	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Din	Lat	Dep	ifi	Lat	Dep
1	00,8	20.5	51	42.8	27.8	101	84.7	55.0	151	126.6	82.2	201	168.6	109.5	251	210.5	136,7
2	01,7		52	43,6		02	85,5	55.5		127.5	82.8	02	169.4	110.0	52	211.3	137,2
100		01.6	53	44.4	28.0	03	86,4	56,1	53	128.3	83.3	03	170.2	110,6	53	212,2	137,8
3	03,4		C	45.3		04	87.2	56.6	54	129.1	83.9	04	171.1	111,1	54	213,0	138,3
4		02,7	54	46.1	30,0	05	88.1	57.2	55	130.0	84.4	05	171.9	111.6	55	213.8	138,9
5			55	_	-	_	88.9	-	156	-	_	-	-	-			
6		03.3	56	47.0	30,5	106	89.7	57.7		130.8	85.0	206	172.8	112,2	256	214,7	139,4
7	05,9	The state of the state of	57	47.8		07	90.6	58.8	57	131.7	85.5	08	1736	112 7	57	215,5	140.0
8	1	04.4		10	10000	08	91.4		1 P. C. M.	132,5	86.6	1000	174.4	113.8	58	216.4	140.5
9		04,9	59	49.5		09	92.2	59.4	59 60	133.3	87.1	09	175.3		59 60	217,2	141.1
10	-	05.4	60	50.3		10	-	59.9	-	134,2		10		114.4	-	-	141,6
11		26.0	61		33.2	III	93.1	60.5	161	1350	87.7	211	176.9	114.9	261	218.9	142.1
12		06.5	62		33,8	12	93,9	61.0	62	135 9	88.2	12	177.8	115,5	62	219.7	142.7
13		07.1	63	1000	34.3	13	94.8	61.5	63	136 7	88.8	13	178.6	116.0	63	220.6	143,2
14		07.6	64		34.9	14	95.6	62.1	64	137.5	893	14	179,5	1165	64	221,4	143.8
15	-	38.2	65	_	35.4	15	96.4	62.6	65	138.4	89.9	15	180,3	117.1	65	222,2	144.3
16		08,7	66		35,9	116	97.3	63 2	166	139.2	90.4	216	181.1	117.6	266	223.1	144.9
17		09,3	67		36.5	17	98,1	63.7	67	140,0	90.9	17	182.0	118.2	67	223.9	145.4
18		09.8	68		37.0	18	99.0	64.3	68	140.9	91.5	18	182.8	118.7	68	224.7	146.0
119	15.9	10.3	69		37.6	19	99.8	64.8	69	141.7	92,0	19	183,7	119.3	6.9	225,6	146.5
20	16,8	10.9	70	58,7	-	20	100.6	65.4	70	142,6	92,6	20	184.5	119.8	70	226 4	147,0
21	17,6	11.4	71	59.5	38.7	121	101.5	65.9	171	143 4	93.1	221	185,3	120.4	271	227,3	147,6
22		12.0	72	60.4		22	102,3	66.4	72.	144.2	93.7	22	186,2	120 9	72	228,1	148.1
23	19,3	12.5	73	61.2	39.8	23	103.1	67.0	73	145.1	94 2	23	187.0	121.4	73	228.9	148.7
24	20.1	13,1	74	62.1	40.3	24	104.0	67.5	74	145.9	94,8	24	187.8	122.0	74	229,8	149.2
25	21.0	13.6	75	62 9	40 8	25	104,8	68,1	75	146.8	95.3	25	188,7	122.5	75	230.6	149.8
26	21.8	14.2	76	63.7	41.4	126	105.7	68.6	176	147,6	95.8	226	189.5	123.1	276	231,5	150,3
127	The same of	14.7	77	64 6		27	106.5	69.2	77	148.4	96.4	27	190.4	123.6	77	232,3	150.9
28	123.5	15.2	78		42.5	28	107.3	69.7	78	149 3	96.9	28	191.2	124.2	78	233.1	151.4
20	24,3		79	66.2	13.0	29	108.2	70.3	79	150.1	97.5	29	192.0	124.7	79	234 0	151.9
30	25 2	-	80	67,1	43.6	30	109.0	75.8	80	150.9	98.0	30	192.9	125.3	80	234.8	152.5
31	-	16 9	81	67.0	44,1	131	109.9	71.3	181	1518	98.6	231	193,7	125.8	281	235 6	153.0
32		17.4	82		44,7	32	110.7	71.9	82	152.6		32	194.6	126.3	82	236.5	153.6
33		18.0	83		45.2	33	111.5	72 4	83	153.5	99.7	33	195.4	126,9	83	237.3	154,1
34	28.5		84	70.4	1.2.24	34	112.4	73,0	84	154 3	100,2	34	196,2	127.4	84	238.2	154.7
35	29.4	19.1	85		1 .	35	113.2	73.5	85	155,1	100.8	35	197,1	128.0	85	239.0	155.2
-	-	19.6			46.8	136	114,0	74.1	186	156.0	101.3	236	197,9	128.5	286	239.8	155.8
36		20.2			47,4	37	114.9	74.6	87	156.8	101.8	27	198.7	129.1	87	240.7	156.3
37		20.7	88	72.8	47.9	38	115.7				102.4			129.6	88	241.5	156.8
39		21,2	80	74.6	48,5	39	116.6			158.5	102,9	39		130.2			157,4
40	32 5	218	90	75 5	49,0	00	117.4		90	159.3	103.5	40	201.3	130.7	90	243 2	
40			-	1		-	118 2	-			104.0		5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	131,2		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10
41		22.3	91		49.6 50.1		119.1	77.3	92	161.0	104.6	241		131,8	291 92	244.0	
42		22,9	92		50 6		119.9		02	161.8	105,1	42	203.8	132.3	93		159.6
43				1 0 0	51,2		120.8	78.4	94	162.7	105.7		204.6	132.9	94	246.5	160.1
44		24.0					121,6		95		106.2	44	205.5	133 4	95	247 4	
45		-	95		No. of Concession, Name of Street, or other party of the Concession, Name of Street, or other pa			-				45					
46		25.1	96	8-	52.3	146	122.4			165.2	106.7	1000	200,3 207 I	134.0	296	240.2	161.2
47	39.4	25.6	97	8-1.3	52.8	47	123.3			166.0	107,3		1 0	134.5	97		161.7
48	40.3	26.1	98	82.2	53.4	48	125.0	81.1	99	166.0	108.4		208,8	135.6	98	1250 7	162.3
49		26.7	99	83.0	53.9	49		81.7	200	167.7	108.9	1 77	209.7	136.2	300	251 6	
50	1 9	27,2	100	3.9	24.2	-			-		-	3			=	3:0	
Ditt	Dep	Lat	Dift	Dep	Lat	Diff	ll Dep	1 Lat	Diff	l Dep	Lat	Diff	Dep	Lat	Dif	l Dep	Lat
-				1			1 1 1 1				A. W. Art		4.954	C	20 1	197	

for 57 Deg.

34 Difference of Latitude and Departure for 34 Deg.

1					and the same							7,0138	17 7			The second		
1	ditt	Lai	Dep	Ditt	Lat	Dep	Ditt	Lat	Dep	Dilt	Lat	Dep	Diff	Lat	Dep	Dilt	Lat	Dep
1	1	00.8	00 6	51	42.3	28.5	101	83.7	56.5	151	125.2	84.4	201	166.6	112.4	251	208.3	140.4
1	2	31.7	1 3 3 7 A	52	43.1	29.1	02	84.6	57 0	52	126.0	85.0	G2	167.5	DOMESTIC STATE OF THE PARTY OF		208.9	140.0
1	3	32.5		53	43.9		0;	85.4	57.6	53	126 8	85.6	01	168.3	113.5	53	209.7	141.
1	4	13.3	32,2	54	44.8	30.2	04	86.2	58.2	54	127.7	86.1	04	169,1	114.1	54	210.6	142 0
1	5	04.1	02.8	55	45.6	30.8	05	870	58.7	55	128 5	86.7	05	169.9	1146	55	211.4	142.6
1	6	050	-	56	6.4	31.3	106	87.9	59,3	156	129.3	87.2	206	170.8	-	256	212.2	-
2			33.9	57	47 3	31.9	07	88.7	59 8	57	130.2	87.8	07	171,6	- 0	57	213.1	143.2
1	7 8		04 5	58	48.1	32.4	08	89.5	63.4	58	131.0	88.4	08	172.4		58		143.7
1	9	2 2 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	05.0	59		33.0	cg	90,4	61.0	59	131.8	88.9	09	173.3		59	214.7	144 8
1	10	08.3	05.6	60	1000	33.6	10	91.2	61.5	60	132.6	89.5	10		117.4	60	*	145.4
1	-		26.2	61	50.6	34,1	111	92.0	62.1	161		90.0	211	1749	118.0	261	2164	146.0
1			06.7	62	51 4		12	92,8	62.6	62	133.5	90.6	12	175.7	01	62	2172	146.5
1	12		07,3	63		35.2	13	93 7	63.2	63	135.1	91.1	13		119.1	63	218.0	147.1
1	14		27,8	64	53 1	35.8	14	94.5	63.7	64	136.0	91.7	14	177.4		64	218.9	147 6
1	15		08.4	65	53 9		15	95:3	64:3	65	136 8	92.3	15	178.2	120.2	65	219.7	148.2
1	16	-	28.9	66	-	36.9	116	96.2	-	_		92.8	-	-	-		220.5	-
1			09.5	67		37.5	17	97.0	64 9	166	137.6	2 4 4 1 1 1 1 1 1 1	216	179.1		67	100	148.7
1	17		10,1	68	20.0	38,0	18	97.8	660	68	139.3	93.4			121 9	68		149.
1	19		10.6	69	57.2	38.6	19	98.7	66 4	69	140.1	91.9	10	181.6	122.5		223.0	149.9
	20		11.2	70	58.c	39.1	20	99.5	67.1	70	140.9	95.1	20	182.4	123.0	-	223.8	151.0
İ	-	17.4	-	-	-	-	-	-					-	_	-	70	224.7	
1	21	18.2		71	100	39.7	121	100.3	67.7 68.2	171	141.8	95.6	221	183 2 184.c	123,6	271	A second	151.5
1	22	19.1	12.9	72	59 7	40 8	22	102.0	68.8	72	142.6	96.2	22		124.7	72	225.5	151
1	23		13.4	73		41.4		102.8	69.3	73	143.4	96.7	23	185.7	125.3	73	227 1	152.7
I		20.7	14.0	74	62.2	41.9	25	103.6	69,9	74	145.1	97.9	24	186 5		74	228.0	153.2
1	25	21.6		75	-	42.5	-			75		-		187.4	126.4	75	228.8	153.8
1		22.4	14.5	76	63.5	43.1	126	104.5	70.5	176	145.9	98.4	226	188.2	126.9	276	229.6	154.3
1	27		15.7	77		43.6	27	105.3	71.0	77	146,7	99.0	27	The second second	127.5	77		154.
1	29		16.2	79		44.2	29	106.9	72.1	1. 2	148.4	99 5			128.1	78	131.3	153.5
1	30		16.8	80		44.7	30	107.8	72.7	79	149.2	100.7	29	190.7	1286	79 8c	The state of the state of	156.6
1		-		81		1000	-	108.6		-	1			-	1	-	-	-
1	31	25.7		82	57,1 58.C	45·3 45·9	131	109,4	73.3	181	150.0	101.2	231	191.5		281	232.9	157.1
1		27.4	18.5	83	68.8	46.4	32	110.3	73,8	83	154,9	101.8	32	193.2	1	83		157.7
1	33	28.2	19.0	84		47,0	33	1111	74.9	84	152.5	102,9		194.0	12000	84	2354	158.3
1	35	29.0		85	40,5		35	111.0	75 5	85	153.4	103.5		194.8		85	236.3	
1	36	-	20.1	86	71.3			-		-		-	35		40	-		159.4
1			20.7		72-1	48.7	136	112.7		186 87		104.0			132.0	286	237.1	15949
-	37 38		21.2	88	73.0		37	114,4	76.6	88	155.0	104.6	37	107.2	132.5	07	237 9	161.0
1	39	12.7	21.8	. 89	73,8	49.8	39	1152	77.2	89	155,9	105.7		108.1	133.6	00	239.6	161,6
1	40		22,4	90	74.6	50.3	40	116.1	78,3			106.2	39		134.2	90	-40.4	162 2
I	41	-	22.9	_	75.4		_	116 9	78.8	90				199.1				
1	42		23.5	91	76.3	51.4		117 7		191	150,3	106.8	241	200 6	134.8	the state of the state of	The state of the s	162.7
1	43	35.6	24.0	93	77.1	52.0	43	118.5	79.4	92	160.0	107.4			135.9	92	242.9	103.3
-	44		24.6		77.9			119.4	80,5	93 94		108.5			136.4		243 7	164.4
1	45		25.2	95	78 8	53.1	45	120.2	81.1	95		109.	44	203.1			244.6	165.0
1	45	38.1			-								47			-		
1	47		26.3	97	79.6	54.2		121.0	81,6		162.5	109.6	246	204.8	137,6	296	245.4	165.5
1	48	10 8	26.8	98	81.2	54.8	47	122.7		97 98		110.2			138.7	97	246.2 247 0	166.1
1	49		27.4	99		55.4		123.5				1 m.3	49	106.4	139.2		247.9	
1	50	41.5	28.0	100		55.9		124,4	83.9	200	165.5	111.8			139.8	99	245 7	
1				=			=				=		1=		==	=	==	=
1	וווע	Dep	Lat	Dift	Dep	La	Diff	Dep	Lat	Dilt	Dep	Lat	Dift	De,	Lat	Ditt	Dep	Lat
1									d. 15.74	1. 11		1111111111		300 2 32 00	34	1 11 11	PART WAR	21 5 10 2 18

for 56 Deg.

Difference	of Latitude and	Denarture	tor	-	Dom
Dillerence	of Latitude and	Departure	101	3.5	DCE.
				00	0

	ט	ittei	ren	ce o	OI !	Lat	itua	e ai	10	Dep	artu	ire	for	35 L	reg.		35
Din	Lat	Dep	Din	Lat	Dep	Din	Lat	Dep	Dift	Lat	Dep	Vill	Lat	Dep	ilt	Lat	Lep
1	3,00	-	51	41 8	29.2	101	82 7	57.9	151	123.7	86.6		164.6	115,3	251		143.9
	21,6		52	42.6	29,8	02	83.5	58.5	52	124.5	87.2	C2		The second second	52		144.5
3		31.7	53	43,4	30,4	03	84.4	59.1	53	125.3	87.7	03	166,3	1164	53		145.1
4	03,3	1.0		44:2	31.0	04	85,2 86,0	59.6	54	126.1	88.3	04	167,1	117.6	54	and the same of the same	145.7
_5	04.1		55		31,5	05			55	120.9		05		-	55		-
6	04,9		56	45.9	32.1	106	86.8	60.8		127.8	89.5	4. 7.	168.7	118.1	256		146.8
7	05,7		57	46.7	22.2	08	87.6	61.4	57	128.6	90.6	08	169.5	119.3	57 58		147,4
8	06.6		10.00		33,8	00	89.3	62.5	1	130.2	91.2	09	100000000000000000000000000000000000000	119.9	59		148.5
9	08,2		59 63	49.1		10	90.1	63 1	30	131.0	91.8	10	172.0	120 4	60	A 10 K A 37 L 63	149.1
10	0g.c	-	61	_	35.0	111	90,0	63.7	161	131.9	92,3	211	172.8	121.0	261	-	149.7
11		26.9	62		35,6	12	91.7	64.2	62	132,7	92,9	100	173.6	121.6	62	214.6	100000000000000000000000000000000000000
12		07.6	63	51.6	36.1	13	92.5	64.8	63	133.5	93.5	13	A CONTRACT OF THE PARTY OF	122.2	63	215.4	150.8
14	11.5	28.0	64	52 4	36.7	14	93.4	65.4	64	134,3	94 3	14	175.3	122.7	64		151.4
15	12.3	08,6	65	53.2	37-3	15	94.2	66.0	65	135 1	94,6	15	176.1	123.3	65	217.0	152.0
16	13,1	39,2	66	54.1	37.9	116	95.0	66.5	166	136 0	95.2	216	176.9	123.9	266		152.6
17	13.9	09 7	67	54.9	38.4	17	95.8	67.1	67	136.8		17	177.7	EL CARLO DE	67		153.I
18	14,7	10.3	68	55.7	39.0	18	96.6	67.7	68	137.6		18	178.5	125.0	68		153.7
19	1 2	10,9	69		39.6		97.5	68,2	69	138.4	96.9	19	179,4	125.6	69	220.3	154,3
20	10.4	11.5	70	57.3	-	20	98,3		70	139.2	97.5	20			70	221,1	154.8
21	1	12.0	71			121	99.1	69.4	171	140,0	98.1	221	181.0		271		155.4
2.2		12.6	72	59.0	41.9	22	99.9	70.0	72	140.9	The same of	22			72		156,0
23		13,2	73	60.6	42.4	23	101.t	71.1	73	142,5	99.8	24	183,5		73		157,1
24	1	14.3	74 75		+3.0	25	102,4	71.7	75	143 3		25	184.3	129.0	75	225,2	157.7
25	-		76	-	43.6	126	103.2	72.3	176	144.1		226	185,1	129.6	276	236.0	158.3
26		14.9	77		44,2		104.0	72.8	77		101.5	27	185.9		77	4000	158 0
27		16.1	78		44,7	28	104,8	73,4	78		102.1	28	186,7	130.8	78	227,7	159.4
29		16.6	79		45.3	29	105.6	74.0	79		102,7	29	187 5	131,3	79		160.0
30		17.2	80		45.9		106.5	74.6	80	147,4	103.2	30	188,4	131,9	80	229,3	160.6
31	:5.4	17.8	81	66.3	46.5	131	107.3	75.1	181	148.2	103.8	231	189.2	132.5	281	230.1	161.2
32		18.4	82	67,2	47.0	32	108.1	75,7	82		104.4	32	190.0	133.1	82	2310	161.7
33	47.0	18 9	83	58.0	47,6	33	108.9	76.3			105,0	33	190,8	133 6	83		162.3
34	1. 1.	19.5	84	68.8	48,2		109.7	76.8	84			34	191.6	134.2	84	232,6	162.9
35	1	20.1	85		48.7	35	p.011	77.4	85		106.1	35	192.5	134.8	85	233 4	163.4
36		1000	86	70.4	49,3	136	111.4	78,0			106.7	235		135.3	286		164.0
37	30,3	21,2	87	71.3	49.9	37	112 2	78.6			107,2		194.1	135.9			164.6
38		21.8		72.1	50.5 51,c	38	113.0	79.1		154.8	107.8	The second second	194,9	136.5	88		165.2
39		22.4	90	72.7	51,6	39 40	114,6	80,3	90	155.6	109.0	39	196,6	137,6	89	236.7	
40		-	-	3.7	52.2	1			-		109.5	-		138,2	90	237.5	-
41	100	23.5	91	75 3	52.2 52.8	141	115.5	80.9	92		110.1	42	197,4	138,8	291	238 3	
42 43		24.1	92 93	76.2	53.3	43	117.1	82,0	93	158.1	111,7		199,0		92 93	240.0	167.5
44		25.2	94	77.0	53.9	44	117.9			1 0	111.3		199,8		94	240.8	168.6
45		25.8	95	77.8	54.5	45	1188		95	159.7	112,8	45	200,6		95	241.6	
46	-	26.4	96		55.1		119.6	-	-		112 4				296	242,4	
47		27,0	97	79.4	55.6	47			97	161,3	118,0	47	202 3		97	243.2	170.3
48	39.3	27.5	98	30.3	50,2	48	121.2	84.9	98	162.2	113.6	48	203 1	142.2	98		170.9
49	10 1	28.1	99	81,1	50.8	49			99	163.0	114.1	19	203.9	142.8	99	244 9	171/5
.50	41.0	28.7	100	31.9	57.4	150	122.8	86 0	200	103.8	114.7	250	204.7	143,4	300	245,7	172 I
Diff	Dep	Lat	Dift	Dep	Lat	D	Dep	Lat	Ditt	Den	Lat	Diff	Dep	Lat	Dil	Dep	Lat

for 55 Deg.

1																	
2 01.6 01.2 32 42.1 50.1 0 8.5 5 60.6 52 123.6 89.9 0 1 165.4 118.7 52 20.9 48.1 13 01.4 13 01	Diff		Dift	-		Din		-	-	Lat		-			-		Dep
3 0.4, 01.8 5 3 2.9, 31.2 03 83 5 60.5 53 12.8 89.9 03 164.2119.3 55 20.4,7 148.2 14.4 1 51.1 54 12.6 12.6 11.9 54 14.5 11.5 54 12.6 12.6 11.9 54 14.5 11.5 54 12.6 12.6 11.9 54 14.5 11.5 54 12.6 12.6 12.6 11.9 54 14.5 11.5 12.5 12.5 55 12.6 11.9 54 14.5 12.6 12.6 12.6 12.6 12.6 12.6 12.6 12.6	1		- 1			100				. 87 - 1					District Control	Control of the Contro	
4 3.2 02.4 0.4 0.5 0.5 4 4.5 1.7 0.4 8.4.7 61.1 54 12.4,6 90.5 0.4 165.0 11.9.9 54 20.5.5 14.9.0 56 0.4 90.5 5 56 45.3 14.9.0 84.0 56.7 0.4 1.5 5.7 0.4 1.5 5.6 14.9.0 5.5 10.5 5.5 12.5 5.5 14.9.0 5.7 0.4 1.5 5.7 0.4 1.5 5.7 0.4 1.5 5.7 0.7 86.6 6.2 9.5 7.5 12.5 5.5 12.5 5.5 12.5 5.5 12.5 5.5 12.5 5.7 0.4 1.5 5.7 0.4 1.5 5.7 0.7 86.6 6.2 9.5 7.5 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12			52				82.5		-		89.3						148.1
S	1000						83 3	100000000000000000000000000000000000000			C. 14	5 S F S F S F S F S				The state of the s	the state of the
6 04 9 03.5 56 45.3 32.9 106 85.8 62.3 156 120.2 91.7 206 166.7 121.1 156 20.7 1 150.5 7 05.7 04.1 37.7 46.1 33.5 07 86.6 62.9 57 127.6 93.3 07 167.5 121.7 57 207.9 1150.5 9 07.3 95.3 59 47.7 14.7 12.9 28.8 26.4 11 59 128.6 93.5 09 169.1 122.8 99.0 81 168.3 122.3 58 282.8.7 151.7 9 07.3 95.3 59 47.7 14.7 12.9 28.8 26.6 14.1 59 128.6 93.5 09 169.1 122.8 99.0 122.4 127.5 124.8 16.2 127.8 128.9 128.9	2.7			Page 1	100	11.11	84.1	100000000000000000000000000000000000000	5.2.2 C X X						2.0		A CONTRACTOR OF THE PARTY OF TH
7 05.7 04.1 57 46.1 23.5 0.7 85.6 62.9 57 127.6 92.3 07 167.5 12.7 57 207.9 151.7 9 07.3 95.3 59 47 7 13.4 7 05 87.4 663.5 38 12.8 92.9 08 169.1 122.8 59 109.5 152.2 10 08.1 05.9 66 48.5 55.3 10 89.0 64.7 66 129.4 94.0 10 169.5 122.4 66 21.0 3 152.8 11 89.6 65 8 62 131.1 10.5 07.6 63 51.0 37.0 13 91.4 65.4 65 131.9 95.8 13 17.3 125.2 63 121.8 131.1 12.4 65.4 11.3 05.8 65 52.2 16.4 12 90.6 65 8 62 131.1 17.3 125.2 63 121.8 131.1 12.4 12.1 05.8 65 52.2 15.4 12 90.6 65 8 62 131.1 17.3 125.2 63 121.8 152.2 15.1 12.1 12.1 12.1 12.1 12.1 12.			-	-							-	-			-		-
8 06 5 04 7 58 6.65 341 0 58 87 4 63.5 \$\$ 1.27.8 92.9 08 168.3 122.8 59 19.5 15.2.2 0 9.109.5 13.2.2 58 12.8.7 15.7.9 19.					10 m	11 11 15000			2	3,50	4600	the state of the s	Contraction Contraction			1 1 1 2	
9 0,7,3 0,5 0,5 0,6 0,4 8,5 3,5 3,5 10 8,9,6 64,7 66 129,4 94,0 10 169,5 121,4 66 210,3 152,8 12 0,9,7 0,7,1 62,5 0,6 14 9,3 35,5 111 89 8,6 65,8 62 131,1 95,2 12 17,75,1 124,6 6 62 121,2 154,6 13 1,0 5,0 6,6 63 8,0 64,7 8,0 8,0 6,5 8,6 64,7 8,0 8,0 8,1 1,1 1,1 1,1 1,1 1,1 1,1 1,1 1,1 1,1									58	127.8							
10			59	47 7	34 7		88.2				93.5	09	169,1	122.8	59	209.5	152.2
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32 25.9 18.8 82 66 348.2 32 106,8 77.6 82 147.2 107.0 32 187.7 136.4 82 228.1 165.5 33 26.7 19.4 83 67.1 48.8 33 107.6 78.2 83 148.0 107.6 33 188.5 137.0 83 228.9 166.3 34 27.5 20.0 84 68.0 49.4 34 108.4 78.8 84 148.9 108.2 34 189.3 137.5 84 229.8 166.3 36 29.1 21.2 86 69.6 50.6 136 116.0 79.9 186 150.5 109.3 236 190.9 138.7 296 231.4 168.7 38 30.7 22.3 88 71.2 51.7 38 111.6 88.152.1 110.5 38 192.5 139.9 88 233.0 169.9 39 31.6 22.9 89 72.0 52.3 39 112.5 81.7 89	-		-		-	-		-			-	-	-	- 33	-	-	
33 26.7 19.4 83 67.1 48.8 33 107.6 78.2 83 148.0 107.6 33 188.5 137.0 83 228.9 166.3 427.5 20.0 84 68.0 49.4 34 108.4 78.8 84 148.9 108.2 34 189.3 137.5 84 229.8 166.3 5 29.1 21.2 86 69.6 50.6 136 110.0 79.9 186 150.5 109.3 236 190.9 138.7 286 231.4 168, 38 29.9 21.7 87 70.4 51.1 37 110.8 80.5 87 151.3 109.9 37 191.7 139.3 87 232.2 168.3 30.7 22.3 88 71.2 51.7 38 111.6 181.1 88 152.1 110.5 38 192.5 139.9 88 233.0 169.3 39 31.6 22.9 89 72.0 52.3 39 112.5 81,7 89 152.9 111.1 39 193.3 140.5 89 223.8 169.4 32.4 23.5 90 72.8 52.9 40 113.3 82.3 90 153.7 111.7 40 194.2 141.1 90 234.6 170.4 133.2 24.1 91 73.6 53.5 141 114 1 82.9 191 154.5 112.3 241 195.0 141.7 291 235.4 171.4 234.0 24.7 92 74.4 54.1 42 114.9 83.5 92 155.3 112.9 42 195.8 142.2 92 236.2 171.4 34.8 25.3 93 75.2 54.7 43 115.7 84.1 93 156.1 113.4 43 196.6 142.8 93 237.0 172.4 34.8 25.9 95 76 9 55.8 45 117.3 85.2 95 157.8 114.6 45 198.2 144.0 95 238.7 173.4 38.8 28.2 98 79.3 57.6 48 119.7 87.0 98 160.2 116.4 48 200.6 145.8 98 241.1 175.4 93 39.6 28.8 99 80.1 58.2 49 120.5 87.6 99 161.0 117.0 49 201.4 146.4 99 241.9 175.5 0 40.5 29.4 100 80.9 58.8 150 121.3 88.2 200 161.8 117.6 250 202.2 146.9 300 242.7 176.		000				10 M	1 1 1 1 1 1 1 1	1 1 1	A STATE OF THE PARTY OF THE PAR	the same of the same	7 1 1 2 2 2				1		
34 27.5 20.0 84 68.0 49.4 34 108.4 78.8 84 148.9 108.2 34 189.3 137.5 84 229.8 166.6 35 28.3 20.6 86 69.6 50.6 136 110.0 79.9 186 150.5 109.3 236 190.9 138.7 296 231.4 168.7 38 30.7 22.3 88 71.2 51.7 38 111.6 88.5 151.3 109.9 37 191.7 139.3 87 23.2,2 168.7 39 31.6 22.9 89 72.0 52.3 39 112.5 81.7 89 152.9 111.1 39 193.3 140.5 89 223.8 169.4 40 32.4 23.5 90 72.8 52.9 40 113.3 82.3 90 153.7 111.1 40 194.2 141.1 90 234.6 170.4 41 33.2 24.1 91 73.6 53.5 141 114.1 82	The second second		The state of the state of						The state of the s				188.5	137,0		The second of the	
35 28.3 20.6 85 68.8 50.0 35 109.2 79.4 85 149.7 108.7 35 190.1 138.1 85 230.6 167. 36 29.1 21.2 86 69.6 50.6 136 116.0 79.9 186 150.5 109.3 236 190.9 138.7 296 231.4 168. 37 29.9 21.7 87 70.4 51.1 37 110.8 80.5 87 151.3 109.9 37 191.7 139.3 87 232.2 168. 38 30.7 22.3 88 71.2 51.7 38 111.6 181.1 88 152.1 110.5 38 192.5 139.9 88 233.0 169. 39 31.6 22.9 89 72.8 52.3 39 112.5 81.11.1 38 152.1 111.1 39 193.3 140.5 89 223.8 169. 40 32.4 23.5 90 72.8 52.9 40 113.3 <td></td> <td>27.5 20.0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>and the same of the same of</td> <td></td> <td>148.9</td> <td>108.2</td> <td>34</td> <td>189.3</td> <td>137,5</td> <td></td> <td></td> <td></td>		27.5 20.0						and the same of the same of		148.9	108.2	34	189.3	137,5			
36 29.1 21.2 86 69.6 50.6 136 110.0 79.9 186 150.5 109.3 236 190.9 138.7 286 231.4 168.7 37 29.9 21.7 87 70.4 51.1 37 110.8 80.5 87 151.3 109.9 37 191.7 139.3 87 232.2 168.7 38 30.7 22.3 88 71.2 51.7 38 111.6 181.1 88 152.1 110.5 38 192.5 139.9 88 233.0 169.9 40 32.4 23.5 90 72.8 52.3 39 112.5 81.7 89 152.9 111.1 39.193.3 140.5 89 223.8 169.9 40 32.4 23.5 90 72.8 52.9 40 113.3 82.3 90 153.7 111.1 10.5 89 223.8 169.9 41 33.2 24.1 91 73.6 53.5 141 114.1 82.9 191		1-1 21					10 10 10 10 10 10 10 10 10 10 10 10 10 1	1 1 1 1 1 1 1 1					9.00				
37 29.9 21.7 87 70.4 51.1 37 110.8 80.5 87 151.3 109.9 37 191.7 139.3 87 232,2 168. 38 30.7 22.3 88 71.2 51.7 38 111.6 J81.1 88 152.1 110.5 38 192.5 139.9 88 233.0 169. 39 31.6 22.9 89 72.c 52.3 39 112.5 81.7 89 152.9 111.1 39 193.3 140.5 89 223.8 169. 40 32.4 23.5 90 72.8 52.9 40 113.3 82.3 90 153.7 111.7 40 194.2 141.1 90 234.6 170. 41 33.2 24.1 91 73.6 53.5 141 114.9 82.9 191 154.5 112.3 241 195.0 141.7 291 235.4 171. 42 34.0 24.7 92 74.4 54.1 42 114.9	26		-	69.6	-	136	110.0	79.9	186	150,5	109.3	236	190.9	138.7	286	231.4	168,1
38 30.7 22.3 88 71.2 51.7 38 111.6 J81.1 88 152.1 110.5 38 192.5 139.9 88 23.0 169.3 39 31.6 22.9 89 72.6 52.3 39 112.5 81,7 89 152.9 111.1 39 193.3 140.5 89 223.8 169 40 32.4 23.5 90 72.8 52.9 40 113.3 82.3 90 153.7 111.7 40 194.2 141.1 90 234.6 170. 41 33.2 24.1 91 73.6 53.5 141 114.1 82.9 191 154.5 112.3 241 195.0 141.7 291 235.4 171. 42 34.0 24.7 92 74.4 54.1 42 114.9 83.5 92 155.3 112.3 42 195.0 141.7 291 235.4 171. 43 34.8 25.3 93 75.2 54.7 43 115.7	1 37	29.9 21.7	87	70,4	51.1	37	110 8	80,5	87	151.3	109.9	37	191.7	139.3	87	232,2	168.7
39 31.6 22.9 89 72.6 52.3 39 112.5 81,7 89 152.9 111.1 39 193.3 140.5 89 223.8 169 40 32.4 23.5 90 72.8 52.9 40 113.3 82.3 90 153.7 111.7 40 194.2 141.1 90 234.6 170. 41 33.2 24.1 91 73.6 53.5 141 114.1 82.9 191 154.5 112.3 241 195.0 141.7 291 235.4 171. 42 34.0 24.7 92 74.4 54.1 42 114.9 83.5 92 155.3 112.9 42 195.8 142.8 93 236.2 171. 43 34.8 25.3 93 75.2 54.7 43 115.7 84.1 93 156.1 113.4 43 196.6 142.8 93 237.0 172. 44 35.6 25.9 94 76.0 55.3 44 116.5	138	30.7 22,3	88	71.2	51.7	38	111.6	181.1	88	152.1	110.5	38	192.5	139.9	88	233.0	169.3
40 32.4 23.5 90 72.8 52.9 40 113.3 82.3 90 153.7 111.7 40 194.2 141.1 90 234.6 170. 41 33.2 24.1 91 73.6 53.5 141 114.1 82.9 191 154.5 112.3 241 195.0 141.7 291 235.4 171. 42 34.0 24.7 92 74.4 54.1 42 114.9 83.5 92 155.3 112.9 42 195.8 142.2 92 236.2 171. 43 34.8 25.3 93 75.2 54.7 43 115.7 84.1 93 156.9 113.4 43 196.6 142.8 93 237.0 172. 44 35.6 25.9 94 76.0 55.3 44 116.5 84.6 94 156.9 114.0 44 197.4 143.4 94 237.8 172. 45 36.4 26.5 95 76.9 55.8 45 117.3	39	31.6 22.9	89	72.0	52.3	39	112.5	81,7	89			39	193.3	140.5	89		
41 33.2 24.1 91 73.6 53.5 141 114 1 82.9 191 154.5 112.3 241 195.0 141.7 291 235.4 171.4 34.4 34.0 24.7 92 74.4 54.1 42 114.9 83.5 92 155.3 112.9 42 195.8 142.2 92 236.2 171.4 14.4 14.4 15.6 25.9 94 76.0 55.3 44 116.5 84.6 94 156.9 114.0 44 197.4 143.4 94 237.8 172.4 15.4 15.4 15.4 15.4 15.4 15.4 15.4 15	40	32.4 23.5	_			-	THE RESERVE	-			-		E 18 10 10 10 10				
42 34.0 24.7 92 74.4 54.1 42 114.9 83.5 92 155.3 112.9 42 195.8 142.2 92 236.2 171. 43 34.8 25.3 93 75.2 54.7 43 115.7 84.1 93 156.1 113.4 43 196.6 142.8 93 237.0 172. 44 35.6 25.9 94 76.0 55.3 44 116.5 84.6 94 156.9 114.0 44 197.4 143.4 94 237.8 172. 45 36.4 26.5 95 76.9 55.8 45 117.3 85.2 95 157.8 114.6 45 198.2 144.0 95 238.7 173. 46 37.2 27.0 96 77.7 50.4 146 118.1 85.8 196 158.6 115.2 246 199.0 144.6 296 239.5 174. 47 38.0 27.6 97 78.5 57.0 47 118.9	41	33.2 24.1			53.5	8	and the second			154.5	112.3	241		141.7		235.4	171.0
44 35.6 25.9 94 76.0 55.3 44 116.5 84.6 94 156.9 114.0 44 197.4 143.4 94 237.8 172. 45 36.4 26.5 95 76 9 55.8 45 117.3 85.2 95 157.8 114.6 45 198.2 144.0 95 238.7 173. 46 37.2 27.0 96 77.7 50.4 146 118.1 85.8 196 158,6 115.2 246 199.0 144.6 296 239.5 174. 47 38.0 27.6 97 78.5 57.0 47 118.9 86.4 97 159.4 115.8 47 199.8 145.2 97 240.3 174. 48 38.8 28.2 98 79.3 57.6 48 119.7 87.0 98 160.2 116.4 48 200.6 145.8 98 241.1 175. 49 39.6 28.8 99 80.1 58.2 49 <	42	34.0 24.7	92	74.4	4 54.1		The second second	83.5	92	155.3	112.9	42	195.3	142 2			171.
45 36.4 26.5 95 76 9 55.8 45 117.3 85.2 95 157.8 114.6 45 198.2 144.0 95 238.7 173.4 46 37.2 27.0 96 77.7 50.4 146 118.1 85.8 196 158.6 115.2 246 199.0 144.6 296 239.5 174. 47 38.0 27.6 97 78.5 57.0 47 118.9 86.4 97 159.4 115.8 47 199.8 145.2 97 240.3 174. 48 38.8 28.2 98 79.3 57.6 48 119.7 87.0 98 160.2 116.4 48 200.6 145.8 98 241.1 175. 49 39.6 28.8 99 80.1 58.2 49 120.5 87.6 99 161.0 117.6 49 201.4 146.4 99 241.9 175. 50 40.5 29.4 100 80.9 58.8 150								84.6		156.0	114.0	43		142.4			172.
46 37.2 27.0 96 77.7 50.4 146 118.1 85.8 196 158,6 115.2 246 199.0 144.6 296 239.5 174, 47 38.0 27.6 97 78.5 57 0 47 118.9 86.4 97 159.4 115.8 47 199.8 145.2 97 240.3 174. 48 38.8 28.2 98 79.3 57.6 48 119.7 87.0 98 160.2 116.4 48 200.6 145.8 98 241.1 175. 49 39.6 28.8 99 80.1 58.2 49 120.5 87.6 99 161.0 117.c 49 201,4 146.4 99 241.9 175. 50 40.5 29.4 100 80.9 58.8 150 121.3 88.2 200 161.8 117.6 250 202.2 146.9 300 242.7 176.	144	36.4 26.5					Carlotte Control of the Carlot		and the second	157.8	114.6	44		144.0	10000	238.	7 172
47 38.0 27.6 97 78.5 57 0 47 118.9 86.4 97 159.4 115.8 47 199.8 145.2 97 240.3 174. 48 38.8 28.2 98 79.3 57.6 48 119.7 87.0 98 160.2 116.4 48 200.6 145.8 98 241.1 175. 49 39.6 28.8 99 80.1 58.2 49 120.5 87.6 99 161.0 117.6 49 201.4 146.4 99 241.9 175. 50 40.5 29.4 100 80.9 58.8 150 121.3 88.2 200 161.8 117.6 250 202.2 146.9 300 242.7 176.	13	27.2 27.0		777	-	146					115 2	246		_	-	- Commission	
48 38.8 28.2 98 79.3 57.6 48 119.7 87.0 98 160.2 116.4 48 200.6 145.8 98 241.1 175. 49 39.6 28.8 99 80.1 58.2 49 120.5 87.6 99 161.0 117.c 49 201,4 146.4 99 241.9 175. 50 40.5 29.4 100 80.9 58.8 150 121.3 88.2 200 161.8 117.6 250 202.2 146.9 300 242.7 176.	40	18.0127.6		78	57.0	40	The second second			150.4	115.8	47	199.8	145.2			
49 39.6 28.8 99 80.1 58.2 49 120.5 87.6 99 161.0 117.6 49 201.4 140.4 99 241.9 175. 50 40.5 29.4 100 80.9 58.8 150 121.3 88.2 200 161.8 117.6 250 202.2 146.9 300 242.7 176. 17	48	38.8 28.2		79.3	3 57.6	48				160.2	116.4	48	200.6	6 145.8	98	241.	1 175
50 40.5 29.4 100 80.9 58.8 150 121.3 88.2 200 161.8 117.6 250 202.2 146.9 300 242.7 176.	40	39.6 28.8	99	80.1	1 58.2	49	120.5	87.6	99	161.0	117.0	49	201,4	4 146.4	99	241.	9 175.
	50	40.5 29.4	100	80.9	58.8	150			200			250	202.5	146.9	300		
La	D:0		_							4							= =
	Dill	. ibepi bat	Ditt	1Del	La	12)III	Тъср	Lat	Din.	- Бер		1211		Lat	1011	Dej	Ld

for 54 Deg.

Difference of Latitude and Departure for 37 Deg. 37

2 3 4 5 6 7 8 9 10	00.8	Carrier Comment	51 52	40.7	-	101	Lat	Dep	-		Dep				-	-	
2 3 4 5 6 7 8 9 10	02.4	01.2	52				80.7	60.8	151	120.6	90.9	201	160,5	121.0	251	200.4	151.0
3 4 5 6 7 8 9 0	02.4	8.10		41.5	31.3	02	81.5	61.4	EE-45	121.4	91.5	02	161.3	121.6	111	201.2	NOT THE RESERVE
4 5 6 7 8 9 0	03,2	Carrier Comment	52		31.9	03	82.3	62.0	53	122.2	92.1	03	162.1	122.2	53	202.0	152.2
5 6 7 8 9 10	04,0	02.4		State of the Control	32.5	04	83.1	62.6		123 0	92.7	04	162.9	122.8	54	202.8	152.9
6 7 8 9 10	_	03.0	THE RESERVE AND ADDRESS.	\$10.00 p.s.	33.1	05	83.9	63.2	55	123.8	93.3	05	163.7	123.4	55	203.6	153.5
7 8 9 10	24.8	03.6		44.7		106	84.7	63.8	156	124.6	93.9	206	164.5	124.0	256	204.4	154.1
9 8		04.2	10 1 1 1 1 1 N	Street Street, Street	34.3	07	85,5	64.4	57	125.4	94.5	07	165,3	124.6	57	205.2	154,7
10	06.4	04.8			34.9	08	86.2	65.0		126.2	95.1	08	Section 1997	CONTRACTOR OF THE PARTY OF THE	N. 15.75	206.0	
10	07.2	05.4		47.1	35.5	09	87.0	65.6		127.0	95.7	09	196 9	Contract to the contract of the	20	206.8	ALTERNATION OF THE
+	08.0	06.0	60	47.0	36.1	10	87.8	66.2	-	127.8	96.3	10	_	126.4	60	107.6	156.5
		06.6	61	48.7	36.7	111	88.6	66.8		128.6	96.9	211	168.5	127.0	261	208.4	157 1
12		07.2	62	49.5	37.3	12	89.4	67.4		129.4	97.5	12	Company of the Company		62		157.7
13		07.8	63		37,9	13	90,2	68.0	1	130.2	98.1	13	The second second	128.2			
14		08.4		A SA CHARLES	38.5	14	910	68.6	Total Control of	131.0	98.7	14	170.9	129.4	65	210.8	
15		090	65		39.1	15	91.8	69.2		131.8	99.3	15					159.
		09.6	66		39.7	116	92,6	69.8		132.6	99 9	216	172.5	130.0	266	212.4	160.7
	4 9	10.2	67		40.3	17	93.4	70.4	68	133.4	100.5	17	173 3	131.2	68	213.2	161.3
45	200	10.8	69		40,9	18	94,2	71.6	69	134.2	101.7	19		131.8	69	214.8	161.0
	16.0	11,4	70	There was	41.5	19	95.8	72.2	70	135.8	102.3	20	175.7	132.4	70	214.6	
20	-	12,6		-	-	-	96.6		171	136.6	102.9	221	176.5		271	216.4	163.1
21		1000	71	56.7		121	97.4	72,8 73.4	72	137.4	103.5	22	177.3			217.2	
22	18.4	13,2	72 73		43.9	22	98.2	74,0	73	138.2	104.1		178.1		73		164.3
23	19.2		74		A STATE OF THE PARTY OF THE PAR	24	99.0	74.6	74	1 4	104.7	W. Ch. C.		134.8		218,8	164.9
24 25	Section of the section of	15,0		59.9		25	99.8	75.2	75	139.8	105,3	25	179.7	135,4	75		165,5
-	-	15.6	76	-	-	126	100.6	75.8	176	140.6	105.9	226	180.5	136.0	276	220.4	166.1
26		16 2	77	1.547	46.3	27	101.4	76.4	77	141.4	1000	25-45-7.4	181.3	136.6		221.2	166.7
27	22.4	1.0-			46.9	28	102.2	77.0		142.2	107.1	-28		137.2	78	222.0	167.3
29	23.2	17,5			47.5	29	103.0	77,6	79	142.9	107.7	APPLY SELECTION		137.8			167.9
30	24,0	18.1	80	63.5	48.1	30	103.8	78.2	80	143.7	108.3	30	-	The second learning	80	223.6	168.5
31	24.8	18.7	81	64.	48.7	131	104.6	78.8	181	144,5	108,9	231			4 1 2 4		169.1
32	25.6			100000000000000000000000000000000000000	149 3		105.4		82	145.3	A 2000 18	6 (A-105-C)		139.6			169.7
33	26.4	19,9			49.9	33	The second second	0 .	83		110.1	100000		A STATE OF THE STA	2007		170.3
34	27.2	100	The second second		150.6	A			84	A	10 mg 1	State of the second	STATE OF THE PARTY	140.8	and the same		170.9
35	28.0			-		35	107.8		-		111.		-	-	-	1000000	171,5
36.	28.7	21.7				136	108.6			148.5		236	188.	142.0	280	228.4	172.1
37	29.5	22,3	87	09.	5 52.4	37	109.4	82.4	99	149.3	112.	37	100	142	2 89	229.	172.
	30.3	22 9		71.	3 53.0	30	110.2	83.6		150.9	112	7 30	190.	143.	8 8	220	8 173.
39		23.			9 54.	1 40	111.8	84.2		151,7	114.	3 40	191.	7 144,	4 90	211.	6 174.
40	31.9	Section 1971					A PRINCIPAL PRIN			The second second	114	CO PERSONAL PROPERTY.	1 192.	The second second	13		4 175.
41	32.7	24.	9	172.	7 54.	141	113.	85.	0	153.	115.		2 193.	3 145.		2 2 2 2 .	2 175.
42	33.	25.	9	74.	5 55° 3 56.		114.	2 86	0	154.	1116.	1 4	3 194.	1 146.		3 234.	0 176.
43	35.		5 9		1 56.		115.		9	1 154.	116.	7 4	4 194	9 146.	8 9	4 234,	8 176.
44		and the Property		5 75.	9 57.			8 87.			7 117.	3 4	5 195	7 147.	4 9	5 235.	6 177.
45	36,		THE PERSONNEL PROPERTY.		7 57		6 116.		9 19	6 156.	5 117	9 24	6 196	5 148.	0 29	6 236	4 178.
		5 28.	3 0	7 77	5 58.	4 4	7 117.	4 88.	5 9	7 157.	3 1118	6 4	71197	3 148	DO	7 237	2 178.
47	38.	3 28.	9 9	8 78	3 59.	0 4	8 118.		1 9	8 1158.	1 1119	2 4	8 1198	1 149	2 9	8 238	0 179
49		1 29.		9 79	1 59.	6 4	9 119.	0 89.	7 9	9 158.	9 119	8 4	9 198	9 149	8 9	9 238	.8 17.9
50	139.	9 30.	1 10	0 79	.9 60	2 15	c 119.	8 90.	3 20	0 159.	7 120	4 25	0 199	7 150	4 30	0 239	6 180
1	De	PLa	ק ד	AD	ED La	t Di	A De	Lat	D	ft De	La	TD	ift De	p La	t D	if De	p La
וועו	L'De	rita	47.50		11-	and the same				7			•				

for 53 Deg.

420-

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0 11.94

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Diff	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep
I	00.8	00.6	51	40.2	31.4	101	79.6	62.	151	119.0	93.0	201	158.4	123.8	251	197.8	154,5
2	100	01.2	52	41.0		02	80.4	62.8	52	3.611	93.6	02	159,2	124.4	52	198.5	
3	02.4	2000	1000	41.8	TOTAL TOTAL	03	81.2	63.4		120.5	94.2	03		125.0	53	199.3	1558
4	10 TO 10 TO 10	02.5	54	42.5	Section of the second	04	81,9		54	121.3	94.8	04	160.7		54	200.1	State of the last
_5	03.9	To be seen to be	55	43,3		05	82.7	64.6	55	122.1	95.4	05	161.5	126.2	55	200,9	
6		03,7	56	44.1	34.5	106	83.5	65.3	156	122.9	96.0	206.			256	2017	
7 8	05.5	04.9	57	44.9		08	84.3	66.5	57 58	123.7	96.7	08	163,1		57	Arrest &	158.2
9	1000	05.5	59	46.5	10.7	09	85.9		59	124,5	97.3	. 09	164.7		58	203.3	150,5
10	and the same of	06.2	60	47.3	1 1	10	86.7	67.7	60	126.1	98.5	10	165.5	129.3	6c	204,9	
ii	08.7	96.8	61	48.1	37.6	111	87.5	68.3	161	126.0	99.1	211		129.9	261		160.7
12	CALL ST	07.4	62	48.9	38.2	12	88.2	69.0	100	127 6	99.7	12		130.5	62	206.4	
13.	10.2	08.0	63	49.6		13	89.0	69.6	63	128 4	100 4	13		131.1	63	07.2	161.9
14		08.6	64	50.4		14	89.8		64	129.2	101.0	14	1000	1318	64	208,0	
15		09.2	65	51.2	40.0	15	90.6	70 8	65	130.0	101.6	15	169.4	1324	65	208.8	163 2
16	1 2 2 2 1 1 1 1	09.9	66	52.0	1000	116	91.4			130.8	102.2	216		133.0			163 8
17	1	10.5	67	52.8		17	92.2	72.0	9	131.6		17		133.6		210.4	1.
18		11.1	68	53.6	1	100 1 100 100	930			132.4	103.4	18		154.2		211.2	165.0
19		11.7	69 70	1	The state of	20	93.8			133,2	104.1	20	172.5	134.8		211 9	166.2
-	-	12.9		-		-			-		-	-		136.1	-		
21	1 1 1	13.5	71 72	1 .	1	121	95.3		. 7 . 2	134.7	105.9	221		136.7	72	213.5	166.9
23		14.2	73	1	1	Manage.	96.9			136.3		23		137.3	- / -	215.1	1
24		148	74	-0	1		97.7	1 .		137.1		24	176 5				168.7
25	19.7	15.4	75		46,2	25	98 5			137,9	107.7	25	177-3	138.5		216.7	169,3
26	20.9	16.0	76	59 9	46.8	126	99.3	77,6	176	138.7	108.4	226	178.1	139.1	276	217.5	169.9
27	21,	16.6	77		47.4		100.1			139.5	109.0	27	178.9	139.8	77	218.2	170 5
28	A COLOR	17,2	78		148 0		100.9	1 - 1 - 1 - 1	10000	140.2	109.6	28	179.6		78		171.2
.29		17.9	79		48.6		101.6	10		141.0		29	180.4		1 13	219.8	
30	1	18.5	80	-	49 3	-	102.4	-	-		110.8	30	-		-	-	172,4
31	100 300	119.1	81				103.2				111.4	231	182.0	142.8		the many and a second	173.0
3 ² 33	1 .	20.3	83		13		104.8	1 0	83	143.4	112.1	33		143.5	A CONTRACTOR OF THE PARTY OF TH	222.2	173.6
34	1	8 20,9		66.2		1 33	105.6				113.3	34	184.4			223,8	
35	1	5 21.5	8				106.4			145.8		35	185.2		1	100	
36	28.	22.2	86	67.8	53.0	-	107.2	-	-	146.5		236	185,9		286	225.3	
37	1	2 22 8	8	68,	5 53.6	37	107,9	84.4	87	147.3	115 1	37	1.00	145.9			176.7
38		23.4	88	109.	3 54.2	38	108.7	85.0	88	148.1	115,8	38	187.5	146.	88	226.9	177.3
39	30.	7 24.0		70.			109.5				116.4		188.3	147.2	89	227.7	177.9
40		5 24.6	-	70.		_	110.				1170	-		47.8		The second second	178.6
41		3 25.2	9	71.	7 56.0	141	111.1	86.8	191		117,6	241	190.9	148.4			179.2
42		1 25.9	9:	72.	5 50.6	42	111.0		. 92	151.3	118.2	42	190.7	149.0	92	2 30.1	179.8
43	33,	26.5	9.	73.						152.1	118.8	43		149.6	93	230.0	180.4
		7 27·1 5 27·7			57.9		114.2			152.6	120.1	44	103.0	150.8	94	232.4	181.0
45	126	2 28.3		75.	and the same of	-								151.			
47	137	0 28.9	9	7 76.	4 50.	146	115.8	90.	97	155.2	120.7	246 47	194.6	152	290	234.0	182.2
48	137.	8 29.6	9	8 77.	2160.	48	116.	6. 91.	98	150.0	121.3	48	195.4	152.	08	234.8	183.5
49	138.	6 30.2	9	9 78.	0 61.0	49	117.	4 91.	99	150.2	1122 5	49		153.5	90	235.6	184,1
50	139.	4/30 8	10	0 78.	8 61,	150	118.2	2 92	4 200	157.6	123.1	250	197.0		300	236.4	184,7
Di	ft De	p Lat	Di	il De	Lat	Diff	Dep	Lat	Diff	Dep	Lat		Dep				
-			-	,,,,,,,	7-40	1		200	12011	. — <u> r</u>	,	1	1-01	1 2-1	1 Din	1 20	Lat

for 52 Deg.

					Jan				•			٠,	on patern	0.		37
Dit 1	LaiDe	Diff	Lat	Del	Dift	Lat	Dep	Din	Lat	Dep	Diff	Lat	Dep	Dift	Lat	1 De
1 00	0.8 00 €	51	39 6	32.1	101	78 5	63.6	151	117 3	95.0	201	156.2	126.5	251	-	158.0
	1.6 01.3	52	40.4		02	79.3	64.2	52	118.1	95.7	C2	157.0	127.1	100	195.8	158.6
13	2.3 01.9	53	41.2	- TI - S. C. C. C. C.	05	80.0	64.8	53	118.0	96.3		157,8		53	196,6	159.2
	3.1 02.5	54	42.6	34,c	05	80.8	65 4	54	119.7	96.9		158,5	the same factor of	100	197.4	159.8
	1.7 03.8	56	43.5	35.2	106	82.4	66.7	_		98.2	05	159.3	-	55		160.5
	5.4 04 4	57	44.3	35.9	07	83.1	67.3	156 57	121.2 122.C	98.8	206	160.9			198.9	161.1
1 1 -	6.2 05.0	58	45.1	36.5	08	83.9	68.0	58	122.8	99.4	90	161.6	130.9		200.5	161,7
	7.005.7	59		37.1	69	84.7	68.6	59	123.6	100.1	09	152.4		1125.0	201.3	163.0
1-1-	7.8 56.3	60	46.6	-	10	85.5	69.2	6c	124,3	100.7	10	163.2	1 32,2	6c	202.0	1.63.6
	8.5 06.9	61	47.4		111	86.3	60,9	161	125.1	101.3	211	164.0		261	202.8	164.2
	9.3 07,6	62		39.0	12	87 0 87.8	70.5	62	125.9	101.9	12	164.7			203.6	164.9
	8.80	64		40.3	14	88.€	71,7	64.	127.4	103.2	13	165.5			204.4	165.5
15 11		65	50.5		15	89.4	72.4	65	128.2	103,8	10	167.1	134.7		205.2	166.1
	2.4 10,1	66	51 3	41.5	116	90.1	73.0	166	129.0	104.5	216	-	135.9	-	206,7	167 4
17 13	3.2 10.7	67	52.1	42.2	17	90,9	73,6	67	1 2 4	105.1	17	168.6	136 6		207.5	68,0
	4,011.3	68	1	1		91.7	74.3	68	130.6	105.7		169,4	137,2		208.3	168.7
	4.8 12.0	69 70	53.t 54.4		20	92,5	74.9	69	131.3	1-06.4	D 1 9 17 1	170.2	1. 1. 1. 1. 1. 1.		209.0	169.3
1 _ 1-	6.3 13.2	-	-	-	-	93 3	75 5	70	132.1	107.0	20	171,C	-	70	209.8	169.9
	7.1 13.8	71 72	55.2 56.c	44.7	121	94.0	76.1 76.8	72		107,6	221	171.7		271	210.6	170.5
	7.9 14.5	73	56.7		23	95.6	77.4	73		108.9	22	172.5		1 X 1 1 1	211.4	171.2
	8 7 15.1	74	57.5	46.6	24	96.4	78,0	74	135.2	109.5	24	174.1	141.0	1	212.1	171.8
25 19	9 4 15.7	75	58.3	47,0	25	97.1	78.7	75		110.1	25	1748		75	213.7	173.1
26 20	0.2 16.4	76	59.1	47,8	126	97.9	79,3	176	136.8	110.8	226	175.t	142 2	-	214.5	173.7
1 /	1.6 17.6	77	59.	48.5	27	98.7	79.9	77	F37.5	111.4	27	176.4	142.9		215.3	174.3
	2.5 18.2	78 79	61.4	49.1	28	99.5	80.6	78	138.3	112.0	28	177.2	143.5		216.0	174.9
1	3.3 18.9	80	62.2	50.3	30	101.0	81,8	79 80	139.1	113.3	30	178.0	144.7		216.8	175.6
-	4.1 19.5	81	62.9	-	131	101.8	82.4	181		113.9	231	179.5		-	-	176.2
1	4.9 20.1	82	63.7	51.6	32	102.6	83.1	82	141.4	114.5	32	180.3	145.4	1 0	218.4	176.8
1 2	5.6 20.8	83	64.5		33	103.4	83.7	83	142.2	115.2	33	181.1	146.6		219.9	178.1
	7.2 22.0	84	65,3 66 1		34	104.1	84.3	84	143.0	115.8	34	181.8	147.3		220.7	178,7
		84		53.5	35	104.9	85.0	85	143.8	116.4	35	182.6	147 9	85	221.5	179.4
	8.c 22,7 8.8 23.3	86	66.8	54.1	136	105.7		186	144.5	117,1	236		148.5		222.3	1800
38 20	9.5.23.9	88	68.4	55.4	37 38	106.5	86.8	88	145.3	117.7	37 38	185.0	149.1		223.0	
39 30	0.3 24.5	89	69 2	56.0	39	108,0	87.5	89		118.9		185.7	150.4		223.8	181.2
	1.1 25.2	90	69.9	56.6	40	8.801	88.1	90	147.6	119.6	40	186 5	151.0		225.4	
41 31	1.9 25.8	91	70,7		141	109,6	88.7	191	148.4	120.0		187.3	151.7	291	226.1	
	2.6 26.4	92	71.5	57.9		110.3	89.4	92	149.2	120.8	42	188.1	152.3	92	226.9	183,8
	3.4 27.1		72.3			111 1	90.0		150,0	121.5	43	188.8	152.9	93	227.7	184.4
	5.0 28.3	94 95	73.8	59,2 59 8	44	111.9			150,8	122.1	44	189.6			228.5	185.0
	5.7 28.9	96.		60.4		113.5	91.9	-		123.3	45	190.4	-	-		185.6
47 36	5.5 29.6	97	75.4	61.0	47	114,2		97	153.1		246 47	191.2	154.0	296	230.0	186.3
48 37	7.3 30.2	98	76.2	61.7	48	115.0	93.1	98	153.9			192 7		97	231,6	187.5
49 38	30.8	99	76.9	62.3	49	115.8	93.8	99	154.6	125.2	49	193.5	156.7	99	232.4	188.2
50 38	3.9 31.5	100	-	62.9	150	116 6 Dep	94.4	-			250	194.3	157.3	300	233.1	188.8
Diff	ep Lar	Dift	Dep	Lai	DA	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat		Dep	Lat
	7				400						(w) in					-

31 B 5.13 12-17-13 18-43 69.56 33.13

333

40 Difference of Latitude and Departure for 40 Deg.

	100	The state of				1000				Mark 188	De Charles	2.00	a de de la constante de la con				
Ditt	Lat	Dep	Ditt	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Ditt	Lat	Dep	Dift	Lat	Dep
1	00.8	00.6	51	39.1	32.8	101	77,4	64.9	151	115.7	97.3	201	144.0	129.2	251	192,3	161.4
1 4 5	01,5	01.3		39.8	33.4	02	78.1	65.6	4 5 6 5	116.4	97.7	02	154.7	129,9		193.0	162.0
2	20000 0000	01.9	State of the last	1.2 - 1	34.1	4530	78,9	66.2	53	117,2	98.4	03	155.5	130.5	100 mm 12 mm	193.8	162 6
3	Charles St. Tal.		3.5			03		66.8	10 - 20 C 10 C	118,0	99.0	04	156.3	131.1		194,6	163.3
4		02.0	54	41.4	34,7	04	79,7	General March	54	118.7	Se United States of Control of Control	100000	157,0	131,8	54	195.3	163.9
5	03.0	03.2	55	42,1	35.3	05	80,4	67.5	55	-	99.6	05		-3.,0	55		
6	04.6	03 9	56		36.0	106	81.2	68,1	156	119.5	100 3	206	157.8	132.4		196.1	164.6
7	05,4	04,5	57	43,7	36.6	07	82,0	68.8	57	120.3	100.9	97	158,6	133 1	3/	196,9	165.2
8	06,1	05.1		44.4	37.3	08	82.7	69,4	58	121.0	101.6	68	159.3	133.7			165.9
9	06.9	05,8	59	45.2	37,9	09	83,5	70,1	59	121,8	102.2	09	160.1	134 4		1984	166.5
10	07,7	06,4	60	46,0	38.6	10	84,3	70.7	60	122,6	102,8	10	160.9	135,0	60	199.2	167,1
111	-	07,1	61	46.7	39.2	111	85.0	71.3	161	123.3	103.5	211	161.6	135.6	261	199.9	167.8
97.30		07.7	.62		39,9	12	85,8	F. Pegali, Sec.		124.1	104.1	12	A 2 M	136.3	and the second	200.7	168.4
12		08.4		48.3		100	86,6	72 0	F 825.6.1	124.9	En a single table	1 100	AND THE RESERVE	136.9	1000 300		169.1
		A Section Section		The Control of the Control		13		72.6		125,6	E 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		163.9		0.000	202.2	169.7
14	1	09.0		49.0		14	87,3	73.3		The State of the State of			164,7			203.0	170 4
15		-	-	-	_	15	88.1	73.9	65		100.1	-			-		
16	12.3	10,3			42.4	116	88.9	74.6	A CONTRACTOR	127,2			165.4	138,8	1 750 to 10	203.7	171.0
17	13.0	10,9			43.1	17	89.6	75.2		127,9			166.2	139,5	the second second	204.5	173.6
18	13.8	11,6	68	52.1	43.7	18	90,4	75,9		128,7		18	167.0	0	1000	205.3	172.3
119	14,6	12,2	69	52.9	44.4	19	91.2	76,5	69	129.4	108,6	19	167.7	140,8	69	206 0	172.9
20	15,3	12 9	70	53.6	45.0	20	91.9	77,1	70	130,2	109 3	20	168.5	141.4	70	206.8	173.6
21			-			121	92,7	77.8	171	121.0	109.9	221	169.3	142.1	271	207.6	174.2
	The state of the s	14.1				100	The state of the state of		1 2 3	131.7		22	170.0	Real Control of Control	72	208.3	174,8
22		14.8	79 Table 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		46.3	22	93,4		S. Bress			1000	170.8	the court of the court of the	73	209.1	175.5
23				1 . 6		23	94,2	B 100 1 2 1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2	73	1000		23	171.6	to the second	1997	209.9	176.1
24		15 4	9	100000	0	24	95.0		74	Date of the	1	24		144.6	916 101	210.6	176,8
25	19.2	16,1	13		-	25	95.7	80.4	75		-	25	172.3		-		-
26	19.	16.7	76	58.2	48.9	126	96.5	81.0	176			226	173.1	145,3	276	211.4	177,4
27	20.	17,4			49.5	27	97.3		77	135,6	113,8	27	173.9	145,9	10 10 10	212.2	178.1
28	21.4	18.0	78	59,7	50.1	28	98,0	82.3	78	136,3	114.4	28	174.6	146,6	78	212.9	
29	22.2	18.6		10	50,8	1 29	98.8	82.9	1 79	137.1	115.1	29	175.4	147,2	79	213.7	179 3
30	23,0	19 3	80	61,3	51.4	30	99.6	83.6	80	137.9	115.7	30	176.2	147-9	80	214.5	180.0
-		-	81	-	-	_	100.3	_	181		116.4	-	176.9	148.5	281	215.2	180.6
3		STREET, STREET				131	101.1			139.4			177.7		1000		181 3
32		20,6			7.					140,2			0				181.9
33	- 6	21,2					101.5	0 4				33	179.2	150.4	-	217.5	182.6
34	1.0					1000000				140.9	1		0.	Carrier Sec.		218.3	183,2
35		-	-		54.6	-	103.4	-	85	-	-	-		-	-		
36	27.	6 23,	86		55.3	136	104.2		186	142.5	119.6	236	180.8		286	219,1	
37	28.	3 23.8	8 87	66.6	55.9	37		88.1	87	143,2	120.2	37	181.5	152.4	87	219.8	184,5
38	29.	1 24.4	1 88	67.4	56.6	38	105,7	88.7	88	144,0	120,9	38	182.3	153.0	88	220,6	185,1
39		25.1	1 89		57,2			89.4	89	144.8	121.5	39	183.1	153,6	89	221.4	185,8
40		6 25.			57.9						122.1		183.8	154.3	90	222.1	186.4
	-	4 26.4			58.5	-	1		40 6 7		122.8	-			-	222.9	187.1
41	200	2 27.0									123.4	1 42	185.4	155,6	02	223.7	
42	32,	27.0	92	77.	59,1	42				The second second	124 1			156	1 00	224,4	188
4:		27.6	93	74,	59.8	43				0 4	124.7			156.0	1 93	225.2	180.0
44	33,	7. 28.	94		60,4					10 March 1977				157		2260	189.6
4	34,	28,			61.1			-			125.4				-	-	-
46	35,	2 29.6	96	73,	61,7	146		93.9	1196	150.1	126.0	246	188.4	158,1	296	226.7	
4:	7 36.	0 30.2	97	174,	3 62.4	47	112,6	94.	97	150.	126.6	47	189.2	1 58.8	97	227.5	190.9
48		8 30.8	98	75.	163.0	48	113,4	95,1	98	151,	127.3	48				228.3	
49		5 31,			63.6			95.8	99	152.	1127.9	49	190,7	160,1	99	229:0	192.2
1 50	128.	2 22.1	1100	76.6	6 64.1	150	1114.0	96.4	200	153.	1128.6	250	191.	160,7	300	229.8	192,9
				1=	=	É	=				===	1	1	7		Dep	Tag
Di	De	p Lat	Dif	De	olLat	Dit	I Dep	1 Lat	וועוו	il Deb	Lat	Dil	t) Dep	Lat	Diff	Dep	Lat
-	-	-	_	-					100	THE RESERVE	and and the second	ale of	The second second		73		

for 50 Deg.

Difference of Latitude and Departure for 41 Deg. 41

2:01	TabDa	-ID	: a T	at 11	Dent	Dial	Lat	Dep 1	Dial	Lat	Den I	Diff	Lat	Den	Dift	Lat	De	-
Diff				-	-	CONTRACT OF	-		-		-	-		_				-
I		362 1820	70000				12 of 50			5 (2) (4)	100000000000000000000000000000000000000	2. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.						
2	Control of the Co.					100				Delivery of the Control of the Contr		1 7 7 1 1		6.5 70 W. C.	建一大大		The same of	No. of the last of
3	00.8 00.7 51 38.5 33.5 101 76.2 66.3 151 114.0 99.0 201 151.7 131.8 251 189.4 164.6 01.5 01.5 01.3 52 39.2 34.1 02 77.0 6.9 52 114.7 99.7 02 152.5 132.5 52 190.2 165.3 02.3 02.6 54 40.8 35.4 04 78.5 68.2 54 116.2 101.0 04 154.0 133.8 54 191.7 166.6 03.8 03.3 55 41.5 36.1 05 79.1 8.9 55 117.0 101.7 05 154.7 134.5 55 192.5 167.3 04.5 05.2 58 43.8 38.0 08 81.5 70.8 58 119.2 103.6 08 157.0 156.2 135.8 57 194.0 168.6 06.0 05.2 58 43.8 38.0 08 81.5 70.8 58 119.2 103.6 08 157.0 156.2 135.8 57 194.0 168.6 06.0 05.2 58 43.8 38.7 09 82.3 71.5 59 120.0 104.3 09 157.7 137.1 59 195.5 169.9 07.5 06.6 60 45.3 39.4 10 83.0 72.2 60 120.8 105.0 10 158.5 137.7 60 196.2 170.5 08.3 07.2 61 46.6 40.0 111 83.8 72.8 161 121.5 105.6 211 159.2 138.4 261 197.0 171.2 09.107.9 62 46.8 40.7 12 84.5 73.5 62 122.3 106.3 12 160.0 139.1 62 197.7 171.9 09.8 08.5 63 47.5 41.3 13 85.3 74.1 63 123.0 106.9 13 160.8 139.7 63 198.5 172.5 10.6 09 2 64 48 3 42.0 14 86.0 74.8 64 123.8 107.6 1160.8 139.7 63 198.5 172.5 113.0 09.8 65 49.1 42.6 15 86.8 75.4 65 124.5 108.2 15 162.3 141.0 65 200.0 173.8 14.3 12.5 69 52.1 45.3 19 89.8 75.1 166.8 110.2 18 164.5 143.0 68 202.3 175.8 113.0 10.5 66 49.8 43.3 116 87.5 76.1 166 125.3 108.9 176.2 18 164.5 143.0 68 202.3 175.8 115.1 13.1 70 52.8 45.9 20 90.6 78.7 70 128.3 111.5 2 166.8 144.3 70 52.8 45.9 20 90.6 78.7 70 128.3 111.5 2 166.8 144.3 70 52.8 45.9 20 90.6 78.7 70 128.3 111.5 2 166.6 144.3 70 203.8 177.1 115.8 13.8 17.5 74 55.8 48.5 24 93.6 81.3 74 131.3 114.1 2.2 166.8 145.9 74 205.8 177.8 116.1 15.7 74 55.8 48.5 24 93.6 81.3 74 131.3 114.1 24.1 169.1 146.9 74 206.8 179.9 18.1 15.7 74 55.8 48.5 24 93.6 81.3 74 131.3 114.1 24.1 169.1 146.9 74 206.8 179.7																	
5	00.8 00.7 51 38.5 33.5 101 76.2 66.3 151 114.0 99.0 201 151.7 131.8 251 189.4 164.6 01.5 01.3 52 39.2 34.1 0.2 77.0 6.9 52 114.7 99.7 02 152.5 132.5 52 190.2 165.3 02.3 02.0 53 40.0 34.8 03 77 7 67.6 53 115.5 100.4 03 153.2 133.2 53 190.9 166.0 03.8 03.0 02.6 54 40.8 35.4 04 78.5 68.2 54 116.2 101.0 04 154.0 133.8 54 191.7 166.6 02.8 03.5 55 41.5 36.1 05 79.1 8.9 55 117.0 101.7 05 154.7 134.5 55 192.5 167.3 04.6 57 43.0 37.4 07 80.8 70.2 57 118.5 103.0 07 154.0 133.8 57 194.0 168.6 06.0 05.2 58 43.8 38.6 08 81.5 70.8 58 119.2 103.6 08 157.0 136.4 58 194.7 169.2 07.5 06.6 05.2 58 43.8 38.4 09 82.3 71.5 59 120.0 104.3 09 157.7 137.1 59 195.5 169.9 07.5 06.6 04.5 33.4 10 83.0 72.2 60 120.8 105.0 10 158.5 137.7 60 196.2 170.5 08.3 07.2 61 46.6 40.0 111 83.8 72.8 161 121.5 105.6 122.8 105.0 10 158.5 137.7 60 196.2 170.5 09.1 07.9 62 46.8 40.0 12 83.5 70.8 62 122.3 106.3 12 160.0 139.1 62 197.7 171.2 09.1 07.9 62 46.8 40.0 12 83.5 74.1 63 123.0 106.9 13 160.8 139.7 63 198.5 172.5 10.6 09.2 64 48 342.0 14 86.0 74.8 64 123.8 107.6 14 161.5 140.4 64 199.2 173.2 11.3 09.8 65 49.1 42.6 15 86.8 75.4 65 124.5 108.2 15 162.3 141.0 65 200.0 173.8 12.1 10.5 66 49.8 43.3 116 87.5 76.1 166 125.3 108.9 166.5 163.0 141.7 266 200.8 174.5 11.3 12.5 69 52.1 145.3 19 89.8 78.1 69 127.5 110.9 19 165.3 143.0 68 20.3 175.8 14.3 12.5 69 52.1 145.3 19 89.8 78.1 69 127.5 110.9 19 165.3 143.0 68 20.3 175.8 14.3 12.5 69 52.1 145.3 19 90.6 78.7 70 128.3 111.5 20 166.6 144.3 70 203.8 177.1 11.3 11.5 70 55.8 48.5 24 93.6 81.3 74 131.3 114.1 2.2 166.8 145.6 75.5 84.5 24 93.6 81.3 74 131.3 114.1 2.2 166.8 145.6 75.5 84.5 24 93.6 81.3 74 131.3 114.1 2.2 166.8 145.6 75.5 84.5 24 93.6 81.3 74 131.3 114.1 2.2 166.8 145.6 75.5 84.5 24 93.6 81.3 77 133.6 113.5 20 166.0 144.3 70 203.8 177.1 11.5 177.5 15.8 48.5 24 93.6 81.3 74 131.3 114.1 2.2 166.8 145.6 75.0 83.3 175.8 11.5 77.5 180.4 177.7 77 55.1 47.5 5.8 48.5 24 93.6 81.3 74 131.3 114.1 2.2 166.8 147.6 75 206.8 179.1 12.0 14.0 14.0 14.0 14.0 14.0 14.0 14.0 14																	
16		-	-	-		106	80.0	69.5	-	17.7	102.3	206		-	-	COLUMN TWO IS NOT		
7						07			and the same of th			A CONTRACT OF STREET						The state of the s
8	The second second	.2	58 4	13,8	38,0	08	81.5			Charles III	The second	08	157.0	136.4		194.7	169	.2
9			59 4	44.5	38.7	09				Service Control		09						
10			60	45.3	39.4	10	83.0	-	60	120,8	105.0	10		-	60	196.2	170	,5
11	08.3 07	.2				111		72.8	161	121.5	105,6	211	159,2	138.4	261	197.0	171	.2
12	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			7				73.5				1 2 1 3						
13	09.8 08	-	_			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1						100000		2000000				
14		1.										13						
15	11.3 09			-	-	-	-					-		-	_			
16						100	89.5		6-			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			The Control			
17		_																
18	1				1	1 1 1 1 1		77.4	and the same of			Mark Control				Contract of the		4. 4. 4
19							1											200
-	-	-		_	-	121			_		AND DESCRIPTIONS	221		-	_		-	- 1
21							ALC: UNITED BY					The state of the s			1 1 1			
23		100					-											
24			1. 2.	55.8	48.5	1000	-			No. of Lot of Street,	Mary Control of the Control	CALL SECTION	169.	146.	74			
25						25	94-3		75	132.1	114.8	25	169.	147.	6 75	The state of the state of		
26		-	_	57.4	49.9	126	95.1	82.6	176	132.8	115.4	226	170,	148.	2 276	208.	3 18	1,0
27	1	- 0.8	19 1 11			27	95.8	83.3					171	3 148.		209.	31 1	1.7
28				58.9	51.2	100	96.6		78	134.3	116.8		A Charles of the	and the second	E-3 E-38 - 1. S			
29	21,91	9.0								135.	117.4	29	The state of the state of		and the second		6 18	3.0
30	22.6 1	9.7	80	60.4	52.5	30	98.1	85.3	80		118.1	- Branches	and in column 2 is not	6 150.		-		3.7
31	23.4 2	0.3	81		53.1		98.9	85.9	181	970	6 118.7		A CONTRACTOR OF THE PARTY OF TH	3 151.			1 18	4.3
32	24,22	All the same of the	82		53.8		99.6				4 119.4			1 152.		2 212		
33		1,6			54.4		100.4			138.	1 120.0	ALL THE SECOND		8 152. 6 153.			6 18	
1.34	1	2.3			55.1		101.1	87.9	85	139.		and the same	The second of the second	4 154			1 18	6.3
3.5		3.0	-	-	55.8	_		-	-			_		1 154	_	-		
36			86	64.9	56.4	130	102.6	89.2	87	A	4 122. 1 122.		7 178			7 216	6 15	7.0
37		4.3	88	66	57.7	38	104.2	89.9			9 123.			6 156		8 217		
38		4.9	89	67.2	58.4	39	104.9	THE PARTY AND ADDRESS.		142.	6 124,		9 180		.8 8	9 218		
39		6 2	90		59.0		105.7				4 124.		0 181	.1 157	,4 9	0 218		
49			91			-	106.4		_		2 125.	and bearing	_	.9 158		1 219		-
4:		2.6	92		4 60.		107.				.9 125		2 182			2 220		
4		8.2	93		61.	43	A CONTRACTOR		93		7 126.	6 4	3 183	,4 159	.4 9	3 221	1 10	92.2
4	4 33,2 2	8.9	94	70.	961.	7 44	108.	94.			.4 127			.2 160		4 221	.9 1	92.8
	5 34.0 2		95		7 62.	3 45	109.				.2 127		_	.9 160		95 222	.6 1	93.5
4	6 34.7 3		96	72,	5 63.	0 146	110.		196		.9 128	.6 24		.7 161		6 223	1.4	94.2
4	7 35.5	0.8	97	73.	2 63.	6 47	110.	9 96.	4 97	148	.7 129	,2 4		.4 162		97 22	4.2 1	94.8
14	8 36.23	1.5	98	74,	0 64.	3 48					,4 129			7,2 162				95.5
4	9 37.0	32.1	99		7 64.				7 99	150	0.2 130			7.9 16		99 22	5.7 1	96.1
	0 37.7				5 65.	_	113.		4 200	-	2.9 131			3,7 16.				90.0
D	ift Dep	Lat	Dif	De	pLa	t Dif	t Dep	Lat	Dif	t De	ep La	it L	ift D	ep La	at D	Diff De	p	Lat
-	эсрі									4							A	

for 49 Deg.

40 Difference of Latitude and Departure for 40 Deg.

		715					71		The same of	7. 3. T. S			PROPERTY.	1			
Ditt	Lat	Dep	Ditt	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep
1	00.8	00.6	51	39.1	32.8	101	77,4	64.9	151	115.7	97.1	201	154.0	-	-	192,3	161.4
2	31,5	1 10 10 1			33.4	02	78.1	65.6	52	116.4		02	154.7	100000000000000000000000000000000000000	100 000 000 000	193.0	162.0
3	02,3	01.9		Charles of the same	34.1	03	78,9		53	117,2	98.4	2 (41.5)	155.5	The second second	10 to	193.8	162 6
4		02.6	54	20 20 1 1 1 1	34,7	04	79,7	66.8	54	118,0			156.3		54	194,6	163.3
_ 5	03.8	03.2	55	42,1	35.3	05	80,4	67.5	55	118.7	99.6	05	157,0	0	55	195.3	163.9
6	04.6	03 9	56	42.9	36.0	106	81.2	68,1		119.5	100 3	206	157.8	132.4		196.1	164.6
7		04,5	57			07	82,0	68.8		The second second	100.9		158,6		57	196,9	165.2
	06,1		58		37.3	08	82.7	69,4	58	121.0	101.6	08	159.3			197.6	165.9
9	06.9		59			09	83,5	70,1	59	Control of the second	102.2	09	160.1	134 4	59	19814	166.5
10	07,7	-	60		38.6	10	84,3	70.7	60	122,6	102,8	10	160.9	135,0	60	199.2	167,1
11	08,4	07,1	61	46.7	39.2	111	85.0	71.3	161	123.3	103.5	211	161.6	135.6	261	199.9	167.8
12			-62			12	85,8	72 0	4 . 3415. 1	124.1	104.1	12	162.4		62	200.7	168.4
100	the state of the state of	08.4		48.3	200	13	86,6	72.6	100		104,8	100000000000000000000000000000000000000	163.2			201.4	169.1
14	1 9 7 2	09.0	64			14	87,3	73.3	64			The State of the S	163.9		200000000000000000000000000000000000000	202.2	169.7
15	11.5	09.6	65		41.8	15	88.1	73.9	65		106.1		104,7	138,2		203.0	1704
	12.3					116	88.9	74.6	S 500		106.7		165.4	138,8	200.00	203.7	171.0
		10,9		51,3		17	89.6	A STATE OF A STATE OF THE STATE			107.3		the second second	139,5	1000	204.5	171.6
100.		11,6		52.1	\$ 1.00 Dec 10.000	18	90,4	75,9			108.0	1000	167.0		100	205.3	172.3
19	20010 31	12,2	69		1000	19	91.2		1	State of the state	108,6	19	168.5	140,8		206 0	172.9
-	15,3	12 9	70	_	45.0	20	91.9	_	70	130,2		20		141.4	-	206.8	173.6
21	16.1	13.5	71	The comment of the control of	10 20 10	121	92,7	77.8	171		109.9	221	169.3	142.1	1500 900	207.6	174.2
22	141	14.1	72		46.3	22	93,4	78.4	1. 1	131.7		22	170.0			208.3	174,8
23		15 4	73	1.00	46 9	23	94,2	79,1	73	132,5		23	170.8	143.3		209.1	175.5
25		16,1	7.4 7.5	57,4	48,2	24	95.0	79,7	74 75	133,3	Section 8	24	171.6	144.6	18 8 W.	209.9	176,8
26	19.9	1	76	_	48.9	126	96.5	81.0	176			25			75		Maria de Cara
27	A	17,4	77		A 10	27	99.5	81.6	1 4 500	134,0	113,1	27	173.1	145,3		211.4	177,4
28	A	18.0	78			28	98,0		77 78				174.6	A Committee of the Comm		212.0	178.7
29	22.2		79	10		29	98.8		79		1	29	175.4	147,2		213.7	179 3
30	23,0	1000	80		51.4	30	99.6	83.6	80	Carried Co.	Pr. 10 51 37	30	176.2	147-9		214.5	180.0
31	23.7	19,9	81	62,0	52,1	131	100.3	84.2	181	_	116.4	231	176.9	148.5		215.2	180.6
32		20,6	82			32	101.1			139.4			177.7	149.1	C	216.0	181 3
33	25,3	Maria Contract	83			33	7.101	85.5	83	140,2	117,6	33	178.5		100 x		181.9
34	26.0	21.9	84	64,3	54.0	34	102.6	86.1	84	140.9		34	179.2	150.4	~	217.5	182.6
35	26.8	22,5	85	65,1	54.6	35	103.4	86.8	85		10	35	180.0	151,1		218.3	183,2
36	27.6		86		55.3	136	104.2	87,4	186	142.5	119.6	236	180.8	151.7	286	219,1	183.9
37	28.3	23.8	87	66.6	55.9	37	104.9	88.1	87		120.2	37	181.5	152.4	87	219.8	184,5
38	29.1	24.4	88	67.4	56.6	38	105,7	88.7	88	144,0	120,9	38	182.3	153.0	88	220,6	185,1
	29.9	25.1	89	68,2	57,2	39	106.5	89.4			121.5	39	183.1	153,6	80	221.4	185,8
40	-	25.7	90		57.9	40		_	90		122.1	40	183.8	154.3	90		186.4
41		26.4	91		58.5	141	108,0		191	146,3	122.8	241	184.6	154.9	291	222.9	187.1
42	32,2	27.0	92	70.5	59,1	42	108,8	91,3	92	147.1	123.4	42	185.4	155,6	92	223.7	187.7
43		27.6	93	71,2			109,5				124 1	43	186.1	1564	93	224,4	188.4
	33,7	28.3		72,0		Section 1	110,3	A STATE OF THE PARTY OF	94		124.7		180.9	156.9		225.2	
45	The Part of the Part of	28,9	95	_	61.1	45	111,1		95		125.4		187.7	and the second	00	2260	-
46		29.6	96		61,7	146	3.111		196	150.1	126.0	246	188.4	158,1	296	226.7	
47	36.0	30.2	97	74,3	02.4	47	112,6	94.5	97		126.6	47	189.2	158.8	97	227.5	190.9
		30.8		75.1			113,4				127.3			159.4	98	228.3	191.6
49	37,5	31,5	99	75.8	64.0	49	114,1	95.8	99		127.9				99	229.0	192.2
=	30.3		=			-	114.9				128.6			-	-	-	192,9
Diff	Dep	Lat	Dift	Dep	Lat	Ditt	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat
						and converse		era grant egy							100		

n: c					11
Difference of	Latitude and	Departure	tor at	Den	
		2 spartare	101 41	Deg.	41

	A Springer of the State of the		1000			1. 1. 1. 1. 1	11 11 11 11 11										
Diff	LatDep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep	-
-	00.8 00.7	51	38.5	33.5	101	76.2	66.3	-	114.0	99.0	-	151.7		market and a			
2	01.5 01.3	000 market 100		34.1	02	77.0	6.9	52	114.7	99.7		152.5			109.4	164.6	
3	02.3 02.0	12717		34.8	03	77 7	67.6		Commence of the second second	100.4		153.2				165.3	
4	03.0 02.6			35.4	04	78.5	68,2	54	116.2	101.0	04		133.8		CONTRACT OF THE	166.6	
5	03.8 03.3	55	41.5	36,1	05	79.1	8.9	55	117.0	101.7	05		134.5	55	192.5		
6	04.5 03.9	56	42.3	36.7	106	80.0	69.5	156	-			155.5			PRINCIPAL PRINCI		
7	05.3 04.6			37.4	07	80.8	70.2	57	118.5		07	156.2		TO 100 100 100 100 100 100 100 100 100 10	193.2		
8	06.0 05.2	58	43,8		08	81.5	70.8	58	119.2		08	157.0		57		168.6	
9	06.8 05.9	59	44.5	38.7	09	82.3	71.5	59	120.0	A COLOR	09	157.7		59		169.9	1
10	07.5 06.6	60	45.3	39.4	10	83.0	72.2	60	120,8	105.0	10	158.5	137.7	60		170,5	
11	08.3 07.2	61	46.0	40.0	111	83.8	72,.8	161	121.5	105,6	211		138.4	261	Chick Statement	171.2	
12	09.107.9	62	46.8	40.7	12	84.5	73.5	62	122.3		12	160.0		Carrier I		171.9	1
13	09.8 08.5	63	47.5	100	13	85.3	74.1	63	123.0		13	160.8	139.7		198.5	172.5	
14	10.609 2	64	48 3		14	86.0	74.8	64	123.8	107.6	14	161.5		64	199.2		
15	11.309.8	65	-	42 6	15	86.8	75.4	65	124.5	108.2	15	162.3	141.0	65	the second second	173,8	
16	12.1 10.5	66		43.3	116	87.5	76.1	166	125-3	108.9	216	163.0	141.7		0	174,5	
17	12.8 11.2	P 2 - 2 V	50.6	44.0	17	88.3	76.7	67	126.0		17	163.8	142.3	F 7 C. F 7	201.5		100
18	13.6 11,8	The second second		44.6	18	89.1	77.4	68	126.8		18	164.5	143.0	124 6 60		175.8	1
19	14.3 12.5	69		45.3	19	89.8	78.1	69	127.5	110.9	19	165 3	143.6			176.4	
20	15.1 13.1	70		45,9	20	90.6	78.7	70	128.3	111.5	20	166.0	144.3			177.1	Ŀ
21	15.8 13.8	71	53.6	46.6	121	91.3	79.4	171	129,1		22 I	166,8	145.0	No. of Concession, Name of Street, or other Designation, Name of Street, or other Designation, Name of Street, Original Property and Name of Stree	12	177.8	F
22	16.6 14.4	72	F . F	47.2	22	92.1	80.0	72	129,8	112.8	22	167.5	145.6	March 2007		178,4	i
23	17.4 15.1	73		47.9	23	92.8	80,7	73	130.6	113.5	23	168.3		73	206.0	179,1	1
24	18.1 15.7	A CHARLES		48.5	24	93.6	81.3	74	131.3		24	169.1	146.9	74	206.8		Ŀ
25	18.9 16.4	75	-	49.2	25	94.3	82.0	75	132.1		25	169.8	147.6	75		180.4	1
26	19.6 17.1	76		49.9	126	95.1	82.6	176	132.8		226	170,6	148.2	276	208.3	181,0	
27	20.4 17.7	- 12		50.5	27	95.8	83.3	77	133.6	Contract of the contract of	27	171 3		77	209.1	181.7	ı
28	21.1 18.4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		51.2	28	96.6	84.0	78	134.3	1 - 1 - 1 H	28	172.1				182.4	
29	21,9 19.0	79 80	12	51.8	29	97.4 98.1	84,6	79 80	135.8	117.4	29		150.2	79	210.6	183.0	1
30	-	_	-	-	30		85.3	-			30		150.9			183.7	ı
31	23.4 20.3	81		53.1		98.9	85.9	181	136.6		231		151.5	281	212.1	184.3	ı
32	24,2 21.0			53.8	32	99.6	86.6 87.2	82		119.4	32		152.2	82	212.8	185.0	ŀ
33	24.9 21,6	84		54.4 55.1	33	101.1	87.9	84	138.1		33		152.8		213.6	185.6	I
35	26.4 23.0			55.8	35	101.9	88.6	85	139.6	A CONTRACTOR	34		153.5	8,	214.3	186.3	ı
		0.0	-	56.4	-	102.6	89.2	-		-	-					186.9	I
36	27.2 23.6		65.7	57.1	27	103.4			140.4	122.7	236	178.1	154.8	286	215.8	187.6	1
	27,9 24.3			57.7	38	104.2	90.5	88		123.3	37 38	178.9	155.5	97	210.0	188.3	ł
	29.4 25.6		67.2	58.4	39	104.9	91.2			124,0			156.8	145	217.4	188.9	I
40	30.2 26.2			59.0		105.7	91.8			124.6	40	181.1	157,4	00		189.6	1
41	30,9 26.9			59.7	141	106.4	92.5	191		125.3	241		158.1				ı
42	31.7 27.6	92	69.4	60.4		107.2	93.1	92		125.9	42		158.7	100		190.9	I
43		93	70.2	61.0	43	107,9				126.6		187.4	159.4		220.4	191.5	1
44	33,2 28.9		70.9	61.7	44	108.7	94.5	ALC: NO.		127.3		184.2	160.0		221.0	192.8	1
45	34.0 29.5			62.3		109.4	95.1	95		127.9		184.9	160.7	95	222.6	193.5	ı
46	34.7 30.2		72.5	63.0		110.2	95.8			128.6	_		161.4	-			I
47	35.5 30.8			63.6		110.9				129,2		186.4	162.0		224	194.2	l
48	36.2 31.5		74,0	64.3		111.7				129.9		187.2	162.7		224	195.5	-
49	37.0 32.1			64.9		112.5	97.7	99		130.5		187.0	163.3		226	196.1	L
50	37.7 32.8					113.2		200		131.2		188,7	164.0	300	226.	4 196.8	1
D:0								Dift		Lat		-		-	1		-
וועו	Dep Lat	ווען	Deb	ידיאני	DIR.	Dep	Lat	1	ьер	Lat	1211	Dep	Lat	וותו	lDep	Lat	1
	The state of the s												1	11/10/10	A PARTY	A STATE OF THE STA	-

for 49 Deg.

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42 Difference of Latitude and Departure for 42 Deg.

				100			and the same			2							
Ditt	Lat	Dep	Dift	Lat	Dep	Dift	Lat 1	Dep!	Ditt	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep
	00.7	00.7	51	37.9	34.1	101	75.0	67.6	101	112.2	101.0	201	149.3	120 5	261	186.5	-
2	21.5	01.3	52	38.6	The state of the s	0.	75.8	68.2	52		101.7	G2	150.1		251	187.2	167.9
3	02.2	11 11 11 11 11	53		35.5	0	75 5	68.9	5	A. S. T.	102.4	03		135.8	52	187.9	169.3
4	1	32.7	54	10.1		04	77.3	69 6	54		103.0	04	151.5		53	188 7	169 9
	03.7	03.3	55	40 9		0.	780	70.2	55	115.1	103.7	05		137.1	54	189.4	170.6
5	04.5	04.0	56	41.6	-	101	78.7					-		-	-		
	05 2		57	42.3		0-	79.5	70.9	57	115.9	105.0	200	153.0		256	190.2	171.3
7 8	059	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	58		38.8	0.	80.2	72.3	58		105 7	08	154.5		57	190.9	171.9
9	36.7		59		39.5	00	81.0	72.9	59	0.00	106.4	09	155.3		59		172.6
10	07.4		60	44 6	40.1	10	81.7	73.6	60	108.9		10	156.0	140.5		193,1	173.9
11		07.4	61	45.3	40.8	111	82.5		161	119.6	-	211	156.7	-	_	-	
12	8.	080	62		41.5	1:	83.2	74.3	62	120.3		12	157.5		261	193.9	174.6
13		08.7	63	+6.8		14	83.9	75,6	63		109,0	1 1 1 1 1 1	158.2			194.6	175.3
14		09.4	64		42.8	14	84.7	76.3	64	0	109.7	14	1590	A CONTRACTOR	64		175.9
15		10.0	65	48.3		1	85 4	76.9	65	122.6	110.4	15	159.7		65		177.3
16	110	10.7	66	-	44.2	116	86.2	77.6	166		111.0	-	-	-	-	-	
17		11.4	67	49.8		17	86.9	78.3	67	123.3	111.7	216		144.5		197.6	177.9
18		12.0	68		45.5	18	87.7	78.9	68		112.4	18		145.8		199.1	
19	1	12,7	69		46.2	16	38.4	79.6	69	125.5	113,1	19		146.5		199.8	180.0
20	14.9	13.4	70		46.8	20	89.1	80.3	70	126.3		20		147.2	70		180.6
21	156	-	71	52.7	47.5	121	89.9	80.9	171	127.0		1-	164,2	-	_		-
22		14.7	72	53.5	1 13	22	90,6	81.6	72	127.8		221		147.8	271	201.3	181.3
23	17.1	15.4	73	54.2	48.8	2:	91.4	82.3	73		115.7	23		149,2	73	1 0	132,6
24	178		74		49.5	24	92.1	83.0	74		116.4	-		149 9	74	203.5	183.3
25	1	16.7	75	55.7	50.2	24	92.9	83 6	75	130,0	10 10 10	25	167.1		75	204.3	184.0
26	193	17.4	76	56.5	-	121	93.6	84.3	176	-	117.7	226	-	151.2	-		184.6
27	20.1	18.1	77		51.5	27	94.3	85.0	77		118.4	2 4 7		151.9	77		185.3
28		18.7	78		52.2	28	93.1	85.6	78		119,1	100		152.5		206.5	
29	21.5	194	79		52.9	25	95,8	86.3	79	2.83	119.7		1 18 1	153.2	1	207.3	186.6
30	22.3	20.1	80	59.4		30	96.6	87.0	80		120.4	The state of the s		153.9		208.0	187.3
31	23.0	20.7	81	60.2	54.2	131	97.3	87 6	181	134.5	2000	-		154.5	281	208.7	188.0
32		21.4	82		54.9	32	98,1	88.3	82		121.8			155.2		209.5	
33	1 1 2 1 1 1	22,1	83	61 7		33	98.8	89.0	83	A CARLO CONTRACTOR	122,4			155.9		210.2	189.3
34	25.3	22.7	84	62.4	56,2	34	99.5	89.6	84	136.7				156.5	84	the state of the state of	190.0
35	26.0	23.4	85	63.	56,9	35	100.3	90.3	85	137,4	123.8	35		157.2	85	211.7	190.7
36	26.7	24.1	86	63.9	57.5	136	101,0	91.0	186	138.2	124.4		_	157.9	286	212.5	191.3
37		24.8	87		58.2		101.8			138.9	125.1	37		158.5	87	213,2	192.0
38		35.4	88	65.4	58.9		102.5		88	139.7	125.8	38	176.8	159.2	88	213.9	192.7
39		26,1	89		59,5	39	103.3		89		126.4		177.5	159,9	1 89	214.9	193.3
40	29.7	26.8	90	66,9	60.2.	40	104.0	93,7	90	141.1	127.1	40	178.3	160.6	90	215,4	194.0
41	30 5	27.4	91	67.6	60.9	141	104.7	94.3	191	141.9	1.27.8	241	179,0	161.2		216.2	194.7
42	31,2	28,1	92		61.5		105.5	95.0	92		128.4			161.9		216.9	195.3
43	31.9	28.8	93		52.2		106,2		93	143.4	129.1		180.5	162.6	93	217.7	196,0
44		29.4	.94		62.9	44	107.0	96.3	94	144.1	129.8	44	181.3	163.2	94	218.4	196.7
45	33.4	30.1	95	70.6	63.6	45	107.7	97.0	95	144,9	130.5	45	182,0	163.9	95	219.1	197.4
46	34.2	30.8	96	71.3	64.2	146	108.5	97.7	196	145.6	131.1		182.7	164,6	296	219.9	198.0
47	34.9	31.4	97	72.1	64.9	47	109,2	98.3	97	146.3	131,8	47	183.5	165.2	97	220.6	
48	35.7	32.1	98	72.8	65.6		109.9			147.1	132.5	48	184.2	165.9		221.4	
49	of and	32.8	99	73.5	66.2	49				147.8	133.1	49	185.0	166.6		222.1	
50	37.1	33.5	100	74.3	66.9	150	1114	100.4	200	148,6	133.8	250	185.7	167.2	300	222.9	
Dift	Dep	Lat	Dift	Dep	Lat	Diff	Dep	Lat	Diff	Dep	Lat	Dift	Dep	Lat	Die	Dep	Lat
							P			Р			- СР	Ditt	1011	- Deb	Lat
														6 4 3			

43

Difference of Latitude and Departure for 43 Deg.

2:11	f	Dani	1.3:00	Lat	Dan	Defa	Inti	Oan !	Diei	Lat	Den	13:41	1	1 Vars		1	1000
		Dep	Dift	-			Lat		-	Lat		Ditt		-	Ditt	Lat	Dep
1	00.7	007	51	37,3	34.8	101	73.9	68,9	151	110.4	103.0	201	147.0	137.1			171.3
2	21,5	014	52	38,0	35.5	02	74,6	69,5	52	111,2	103.6	02		137.7	52	184.3	171.8
3	02.2	02.0	53	38.8	36.2	03	75.3	70,2	53	111.9	104.3	03	148.5	138.4	53	1350	172 5
4	02,9	02.7	54	39.5	36.8	04	76.1	70,9	54	112.6	105,0	04	149.2	139.1	5+	185.8	173.25
5	03,7	03 4	55	40,2	37.5	05	76,8	71,6	55	113.4	105.7	05	1499	139.8	55	186,5	173 9
6	04.4	04,1	56	41.0	38.2	106	77,5	72,3	156	114.1	106,4	206	150.7	140,<	3.56	£87,2	174.5
	05,1	04,8	57	41.7	38.9	07	78,3	73.0	57	114,8		27	151.4	141.2		188.0	175.2
3		35,5		42,4	39.5	08	79.0	73.6		115,6		08	152.1	141.8		188.7	175.9
		06,2	59	43.1	40.2	09	79.7	74 3	59	116.3	100000	09		142,5		189.4	176.6
	07,3	06,8	A	43,9	40 9	10	80,4	750	60	117.0		10	153.6	143.2		190.1	177.3
	08,0		61	-	-	-	-		161			-	-		-	-	-
		07.5	W. W.	44,6	41,6	111	81,2	75,7	A 100 100 100 100 100 100 100 100 100 10	117.7		211	154.3	143.9		190,9	178,0
	08,8	38,9	10.2.1	45.3	42.3	12	81.9	76.4		118.5		12	155.0	144.5		191.6	178.6
1	09,5			46.1	43.0	13	82,0	77,1	63		111.2	13		145,2		192.3	179,3
14	1 355	09,5		46,8	43 6	14	83,4	77.7	64	119,9	13 6 4 5 1 1	14	156.5	145.9		193.1	180,0
15	11.0	10,2	65	+7,5	44 3	15	84,1	78,4	65	120.7	112.5	15	157.2	146 6	65	1938	180.7
16	11.7	10,9	66	18,3	45.0	116	84,8	79,1	166	121,4	113.2	216	158,0	147.3		194.5	181.4
17	12.4	11,6		19,0	45,7	17	85,6	79.8	67	122.1	3.	17	158,7	148 c		195.3	182.1
18	13.2	12,3	68	49.7	46.4	18	86.3	80,5	68	122.9	114.5	18	159.4	148.6	68	196.0	182.7
19		13,0	69		47.1	19	87,c	81.2	69	123.6		19	160,2	149.3		196.7	183.4
20	14,6	13,6	70	51,2	47.7	20	87.8	81.8	70	124.3	115.9	20	160.9	150,0	70	197.5	184.1
21	15,4	14.3	71	51.9	48,4	121	88.5	82.5	171	125.1	116,6	221	161.6	150.7	271	1982	184.8
22	1	15.0	72	152 7	49,1	22	89,2	83 2	72	The same of the sa	117.3	22	162 4	151,4		198,9	185.5
1 23	16,8	15.7	73	53,4	49,8	23	90.0	839	73		118.0	23		152.1		199.7	186.2
24	1 0		74	1 - 10 A A	50.5	24	90,7	84.5	74	127,3		24		152.7		200,4	186.8
25	1 . 0	17,1	75	54,9	51,2	25	91.4	85,2	75	128.0	119.3	25	164.6	153.4		201.1	187.5
25	19,0	17,7	76	-	-	126	92.1	85.9	176	128.7	120,0	226	165 3	154.1	-	201.9	188.2
27	1	18.4	77			27	92,9	86.6	77	10000	120.7	27		154.8			188.9
28	1	19,1	78			28	93.6	Apr. 10 172 - 100 Apr.		130.2		28		155.5		203,3	
20	1	19,8	79			29	94,3	88,0		130.5		29	167.5			204.0	
30	1	20,5	80		54.5	30	95,1	88.6	80	131.t		30	168.2			0	190.9
1-		-	1-	-					181			-		-	-		
31	1	21,2			55.2	131	95,2	893	82	132.4		231		157.5		205.5	191.6
32				60,7		32	90,5	90.0	83	133.1		32		158.2			192.3
33	1	22,5			The second	33	97,3	90.7	84	133.	124.8	33	170.4			207.0	193.0
34	1 1	23,2				34	98.7	91,4	85	134.6	125.5	34	171.1	159,5	04	207.7	A CONTRACTOR OF THE PARTY OF TH
35		-	-	-	-	-	-	92.1		135.3	120.2	35	171.9		-	208.4	194,3
36						136	99.5	92.7	186	130.0	126.8	236	172.6		286	209,2	195.0
37				63,6		37	100.2	93.4	87	130.8	127,5	37	173 3	161.6	87	209.9	195.7
38	1 . 12	25.9	88	04,4	60,0		100.9	94.1	88		128,2		174.1	162.3	88	210,6	196,4
39	100000	26,6		05.1	60,7	39	101.7	94.8			128.9			163,0	89	2114	197.1
40	29.3	-	-		61,4		102.4		90	139.0	129.5	40	-	163,6	90	212.1	197.7
41	30.0	28,0		EXPLORED TO THE	62.1		103,1	96.2	191	139.7	130.2	41	176.3	164,3	291	212.8	198.4
42	30,7	28,6			62,7		103.0			140.4	130.9	42		165.0	92	213.6	199.1
1 43	31,4	29.3	93		63,4		104 6				131.6	43	177.7			214.3	199.8
1 44	32,2	30,0	94		64,1		105,3		94	141.9	132,3	44		1.66.4			200.5
45	32,9	30.7	95	69,5	64,8	45	106.0	98,9	95	142.6	133 0	45		167,1		215.7	
46	33.6	314	96	70.2	65 5	-	106.8	99 5	-	B B B C B B C	133,6	-		-		216.5	201 8
47		32.1		70.0	66,2	47		100.2			134.3	47	180.6	168.4	07	217.2	202.5
1 48		32.7			66.8	48	108,2	100.9	98		135.0	48	181.4	160.	08	217.0	203.2
		33,4			67,5	49	100.0	101,6			135.7		182.1	169,8			203.2
50	36,6	34,1	100	10000		150	100.7	102.3	200	146.	136.4		182.8	170.0	200	210 4	204 6
1=	-	-			=												===
Dil	tDep	Lat	Dil	t Dep	Lat	IDiff	Dep	Lat	Dill	Дер	Lat	Diff	Dep	Lat	Dift	el Dep	Lat
				Acres manage					nem's								

for 47 Deg.

44 Difference of Latitude and Departure for 44 Deg.

1 00.7 00.7 51 36.7 35.4 101 72.6 70.2 151 108.6 104.9 201 144.6 139.6 251 180,5 174, 2 01.4 01.4 52 37.4 36 1 02 73.4 70.8 52 109.3 106.3 02 145.3 140.3 52 181.3 175, 3 02.2 02.1 53 38.1 36.8 03 74.1 71.5 53 110.1 106.3 03 146.6 141.0 53 182.6 175 4 02.9 02.8 54 38.8 37.5 04 74.8 72.2 54 110.8 107.0 04 146.7 141.7 54 182.7 176.5 03.6 03.5 55 39.6 38.2 05 75.5 72.9 55 111.5 107.7 05 147.5 142.4 55 183.4 177. 7 05.0 04.9 57 41.0 39.6 07 77.0 74.3 57 112.9 109.1 07 148.9 143.8 57 184.9 178. 8 05.8 05.6 58 41.7 40.3 08 77.7 75.0 58 113.6 109.7 08 149.6 144.5 58 186.6 179.9 06.5 06.3 59 42.4 41.0 09 78.4 75.7 59 114.4 110.4 10.9 150.3 145.2 59 186.3 179.1 10.0 77.2 06.9 60 43.2 44.7 10 79.1 76.4 60 115.1 111.1 10 151.1 145.9 66 187.7 181. 12 08.6 08.3 62 44.6 43.1 12 80.6 77.8 62 116.5 112.5 12 152.5 147.3 62 183.5 182.1 13 09.4 09.0 03 45.3 43.8 13 81 3 78.5 63 117.2 113.2 13 153.2 147.9 63 189.2 182.1 151.0 10.9 7. 64 46.0 44.5 14 82.0 79.2 64 118.0 113.9 14 153.9 148.6 64 189.9 183.1 15.10,8 10.4 65 46.8 45.1 15 82.7 79.9 65 118.7 114.6 15 154.6 149.3 65 190 6 184. 17 12.2 11.8 67 48.2 46.5 17 84.9 82.0 68 10.4 115.4 117.4 19 157.5 152.1 69 193.5 186.3 179.1 12.2 11.8 67 48.2 46.5 17 84.9 82.0 68 120.4 117.4 19 157.5 152.1 69 193.5 186.3 193.1 15.1 14.6 71 51.1 14.6 71 51.1 14.9 12.5 184.0 193.5 186.3 193.1 15.1 14.6 71 51.1 14.6 71 51.1 14.9 12.5 180.0 11.5 18.1 14.6 15 154.6 14.9 3 65 190 6 184.1 17.4 19.1 17.5 154.6 14.9 3 65 190 6 184.1 17.4 19.1 17.5 154.6 14.9 3 65 190 6 184.1 17.4 19.1 17.5 154.6 14.9 3 65 190 6 184.1 17.4 19.1 17.5 154.6 14.9 3 65 190.5 186.3 186.1 17.5 11.1 14.6 71 51.1 14.6 71 51.1 14.9 157.5 152.1 16.9 193.5 186.2 153.5 186.3 179.1 18.5 18.5 18.5 18.5 18.5 18.5 18.5 18		in many			200					aste pr	14.4					St. 30%	Address in the	49 114
1 0-7, 00-7, 01-7, 01-3, 13-6, 73-4, 101, 72-6, 70-8, 73-1, 10-8, 10-4, 10-4, 10-4, 13-4, 10-8, 13-4, 10-8,	\mathbf{D}	Lat	Dep	Ditt	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Ditt	Lat	Dep	Dit	Lat	Dep
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41 29,5 28.5 91 65.5 63.2 141 101.4 97.9 191 137.4 132.7 241 173.4 167.4 291 209.3 202. 43 30.9 29.9 93 66.9 64.6 43 102.9 99.3 93 138.8 134.1 43 174.8 168.8 93 210.8 203. 44 31.6 30.6 94 67.6 65.3 44 103.6 100.0 94 139.5 134.8 44 175.5 169.5 94 211.5 204. 45 32.4 31.3 95 68.3 66.0 45 104 3 100.7 95 140.3 135.4 45 176.2 170.2 95 212.2 204. 46 33.1 32.0 96 69.1 66.7 146 105.0 101.4 196 141.6 136.1 246 176.9 170.9 296 212.9 205, 47 33.8 32.6 97 69.8 67.4 47 105.7 102.1 97 141.7 136.8 47 177.7 171.6 97 213.6 206. 48 34 5 33.3 98 70.5 68.1 48 106.5 102.8 98 142.4 137.5 48 178 4 172.3 98 214.4 207. 49 35.2 34.0 99 71.2 68.8 49 107.2 103.5 99 143.1 138.2 49 179 1 173.0 99 215.1 207. 50 36.0 34.7 100 71.9 69.5 150 107.9 104.2 200 143 9 138.9 50 179.8 173.6 300 215.8 208.	40			90	64.7	62.5	40					132.0				00	208.6	200.7
42 30.2 29.2 92 66.2 63.9 42 102.1 98.6 92 138.1 133.4 42 174.1 168.1 92 210.0 202. 43 30.9 29.9 93 66.9 64.6 43 102.9 99.3 93 138.8 134.1 43 174.8 168.8 93 210.0 203. 44 31.6 30.6 94 67.6 65.3 44 103.6 100.0 94 139.5 134.8 44 175.5 169.5 94 211.5 204. 45 32.4 31.3 95 68.3 66.0 45 104.3 100.7 95 140.3 135.4 45 176.2 170.2 95 212.2 204. 46 33.1 32.0 96 69.1 66.7 146 105.0 101.4 196 141.0 136.1 246 176.2 170.9 296 212.9 205, 47 33.8 33.3 98 70.5 68.1 48 106.5 <td>-</td> <td>120</td> <td>-</td> <td>107 600</td> <td></td> <td>_</td> <td></td> <td></td> <td></td> <td>Three markets</td> <td></td> <td></td> <td></td> <td>-</td> <td></td> <td>-</td> <td>-</td> <td>-</td>	-	120	-	107 600		_				Three markets				-		-	-	-
43 30.9 29.9 93 66.9 64.6 43 102.9 99.3 93 138.8 134.1 43 174.8 168.8 93 210.8 203. 44 31.6 30.6 94 67.6 65.3 44 103.6 100.0 94 139.5 134.8 44 175.5 169.5 94 211.5 204. 45 32.4 31.3 95 68.3 66.0 45 104.3 100.7 95 140.3 135.4 45 176.2 170.2 95 212.2 204. 46 33.1 32.0 96 69.1 66.7 146 105.0 101.4 196 141.0 136.1 246 176.2 170.9 296 212.9 205, 47 33.8 32.6 97 69.8 67.4 47 105.7 102.1 97 141.7 136.8 47 177.7 171.6 97 213.6 206. 48 34.5 33.3 98 70.5 68.1 48 106.5 <td>41</td> <td>120,</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>191</td> <td>137.4</td> <td>132.7</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>202.1</td>	41	120,								191	137.4	132.7						202.1
44 31.6 30.6 94 67.6 65,3 44 103.6 100.0 94 139.5 134.8 44 175.5 169.5 94 211.5 204. 45 32.4 31.3 95 68,3 66.0 45 104.3 100.7 95 140.3 135.4 45 176.2 170.2 95 212.2 204. 46 33.1 32.0 96 69,1 66.7 146 105.0 101.4 196 141.0 136.8 47 177.7 171.6 97 213.6 206. 48 34.5 33.3 98 70.5 68.1 48 106.5 102.8 98 142.4 137.5 48 172.3 98 214.4 207. 49 35.2 34.0 99 71.2 68.8 49 107.2 103.5 99 143.1 138.9 49 179.1 173.6 300 215.8 208. 50 36.0 34.7 100 71.9 69.5 150 107.9 104.2<										92	130.1	33.4						
45 32.4 31.3 95 68,3 66.0 45 104 3 100.7 95 140.3 135.4 45 176.2 170 2 95 212.2 204. 46 33.1 32.0 96 69,1 66.7 146 105.0 101.4 196 141.0 136,1 246 176.9 170.9 296 212.9 205, 47 33.8 32.6 97 69.8 67.4 47 105.7 102.1 97 141.7 136.8 47 177.7 171.6 97 213.6 206. 48 34 5 33.3 98 70.5 68.1 48 106.5 102.8 98 142.4 137.5 48 178 4 172.3 98 214.4 207. 49 35.2 34,0 99 71.2 68.8 49 107.2 103.5 99 143.1 138,2 49 179 1 173,0 99 215.1 207. 50 36.0 34.7 100 71.9 69.5 150 107.9 104.2 200 143 9 138.9 50 179.8 173.6 300 215.8 208.																		
46 33.1 32.0 96 69,1 66.7 146 105.0 101.4 196 141.0 136,1 246 176.9 170.9 296 212.9 205, 47 33.8 32,6 97 69.8 67.4 47 105.7 102.1 97 141.7 136.8 47 177.7 171.6 97 213.6 206. 48 34 5 33.3 98 70.5 68.1 48 106.5 102.8 98 142.4 137.5 48 178 4 172.3 98 214.4 207. 49 35.2 34,0 99 71.2 68.8 49 107.2 103.5 99 143.1 138,2 49 179 1 173,0 99 215.1 207. 50 36.0 34.7 100 71.9 69.5 150 107.9 104,2 200 143 9 138.9 50 179.8 173.6 300 215.8 208.				05	68 3	66.0								175.5	109.5			204.2
47 33.8 32.6 97 69.8 67.4 47 105.7 102.1 97 141.7 136.8 47 177.7 171.6 97 213.6 206. 48 34 5 33.3 98 70.5 68.1 48 106.5 102.8 98 142.4 137.5 48 178 4 172.3 98 214.4 207. 49 35.2 34.0 99 71.2 68.8 49 107.2 103.5 99 143.1 138.2 49 179 1 173.0 99 215.1 207. 50 36.0 34.7 100 71.9 69.5 150 107.9 104.2 200 143 9 138.9 50 179.8 173.6 300 215.8 208.	45	32.0					-											-
48 34 5 33.3 98 70.5 68.1 48 106.5 102.8 98 142.4 137.5 48 178 4 172.3 98 214.4 207. 49 35.2 34,0 99 71.2 68.8 49 107.2 103.5 99 143.1 138,2 49 179 1 173,0 99 215.1 207. 50 36.0 34.7 100 71.9 69.5 150 107.9 104,2 200 143 9 138.9 50 179.8 173.6 300 215.8 208.				96	09,1	66.7	146				141.0	136,1	246	176.9	170.9	1296		
49 35.2 34.0 99 71.2 68.8 49 107.2 103.5 99 143.1 138.2 49 179 1 173.0 99 215.1 207. 50 36.0 34.7 100 71.9 69.5 150 107.9 104.2 200 143.9 138.9 50 179.8 173.6 300 215.8 208.	47	33.	32,6	97	09.8	07.4	47	105.7						177.7	171.6	97	213.6	206.
49 35.2 34.0 50 36.0 34.7 100 71.9 69.5 150 107.9 104.2 200 143.9 138.9 50 179.8 173.6 300 215.8 208. Dift Dep Lat Dift De				98	70.5	60.1					142.4	137.5	48	178 4	172.3		214.4	207.
100 100		35.							103.5	99	143.1	138,2	49	179 1	173,0	99	215.1	207.
Dift Dep Lat				-	-		-	107.9	104,2	-			50	179.8	173.6	300	215.8	208.
1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	Di	Der	Lat	Dif	Den	Lat	Dif	Der	Lat	Diff	Dep	Lat	Diff	Den	Lat	Dia	Den	Lat
					1 1		V 100							1-04	1 Dat		Бер	Lat

for 46 Deg.

			1 1 1 1 1 1		-		
Difference	nt	atitude	and	Denarture	tor	A P.	Dem
Dilletelle	OI	Latitude	anu	Departure	IOI	45	Dig.

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10 mm								m.H.									,
Dift	Lat	Dep	Dift	Lat	Dep	Diff	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep
1	00.7	00.7	51	36.1	36.1	101	71.4	71.4	151	106.8	106.8	201	142.1	142.1	251	177,5	177.5
2		01.4		36,8	36.8	02	72,1	72.1	52	107.5	107.5	02	142.8	142,8		178.2	178.2
3		02.I	53	37.5	37,5	03	72.8	72.8	53	108.2	108.2	03	143.5	143.5	53	178.9	178.9
4	.2.8	02.8	54	38.2	38,2	04	73.5	73.5	54	108.9			144.2	144,2	54	179.6	179.6
5	03,5	03 5	55	38.9	38,9	.05	7.4.2	74.2	55	1096	109.6	05	144.9	144,9	55	180,3	180.3
6	04.2	04,2	56	39.6	39,6	106	74.5	74,9	156	110.3	110.3			145-7	256		181.0
7	04,9	04.9	57		40.3	07	757	75,7	57	111.0			1 N N N T	146.4	57	181,7	181.7
8		05.7	-		41,0	08	76.4	76,4	58	111.7		11/2 50 11	147,1	147.1	58		182,4
9		06.4	59	41.7	41.7	09	77.1	77.1	59	112.4	112.4	09	147.8	147.8	59	183,1	183.1
10	27.1	07.1	-	42.4	42,4	1.0	77,8	77.8	60	113.1	_	10			-		-
11	07.8		61	43.1	43.1	III	78.5	78.5	161	113.8			10-20-00-00-00-00-00-00-00-00-00-00-00-00	149,2	261 62	184.5	184.5
12	00,5	08.5	62	43.8	43.8	12	79.2 79.9	79,2	62	114.5	114,5	13		149.9	63	186.0	186,0
13	1 -	09.9	64	45.3	45,3	14	80.6	80,6	64	1153			151.7	151.3	64	186.7	186.7
15	1 ' :	10,6	65		46.0	15	81.3	81.3	65	116.7		15		152.0	65	187.4	187.4
16	11.3	11.3	66	46,7	46.7	116	82.6	82.0	166	117.4	117.4	216	152,7	152.7	266	188,1	188.1
17	1 -	12.0	67	47.4	47.4	17	82.7	82.7	67	-	118.1	17	153,4	153,4	67	188,8	188,8
18.	1	12.7	68	48,1	48.1	18	83,4	83.4	68	118.8	118.8	1 .	154.1	154.1	68	189,5	189.5
19	13.4	13.4	69	48.8	48.8	19	84.1	84.1	69	119.5	119,5	19		154.8	69	190.2	190.4.
20	14.1	14.1	70	19.5	49 5	20	84.8	84,8	70	120.2	120.2	20	155.6	155.6	70	190.9	190.9
21	14,8	14,8	71	50,2	50.2	121	85.6	85.6	171	120,9	120.9	221	156,3	156,3	271	191,6	191,6
22	15.6	15.6	72	50.9	50.9	22	86.3	86.3	72	121.6	121.6	22	157.0	157.c	72	192.3	192.3
23	16,3		73	51.6	51.6	23	87.0	87.0	73	122.3		23		157.7	73	193,0	
24	17,0	A. Care S	74	1 -	52.3	24	87.7 88.4	87.7	74		123.0	24	158,4	158.4	74	193.7	193.7
25	17.7	-	75	_	53.0	25		88,4	75	-	123.7	25	159,1	159.1	75	194.4	194.4
26	1	18.4	.76	53.7	53,7	126	89.1	89.1	176	1244		226	159.8	159,8	276	195,2	195.2
27	1	19.1	77		54.4	27	89.8	89,8	77 78	200	125,2	27	160,5	160.5	77 78	195 9	195.9
20	1. 22 - 2	20.5	79	55.2	55.2	29	91.2	90,5	79	126.6	125.9	29	161.9	161.0	79	190,0	197.3
30	21.2	1 -	80	56.6		30	91.9	91,9	80	127.3		30	162.6	62.6	80	198,0	1
31	21.0	-	81	_	57.3	131	92.6	92.6	181		128.0	231	163.3	163.3	281	198.7	198.7
32		22,6			58.0	32	93.3	93,3	82		128,7	32	164.0	164.0	82	199 4	
33	23.5		83	58.7		33	94,0	94.0	83	129 4	1	33	164,7	164.7	83	200.1	1
34	24,0	24.0	84	159.4	59.4	34	94,7	94.7	84	130.1	130.1	34	165,5	165.5	84	200.8	200.8
35	24.7	24.7	85	60.1	60.1	35	95,5	95.5	85	130.8	130,8	35	166,2	166.2	85	201.5	201.5
36	25	25.5	86			136	96.2	96.2		131.5	131.5	236	166 9	166.9		202.2	202.2
37		26.2	87	61,5	61.5	37	96.9	96,9	87	132 2	132.2	37	167,6	167.6	87		202,9
38		26,9			62,2		97.6				132.9		168,3			-	
39		27,6		62.9	62,9	39	98.3				133,6		169.0	169.0	.89		
40	-	28.3	_		63.6		99.0	_			134.3	40		-		205.1	
41		29.0		64.3	64.3	141	99.7			135.1	135.1		170,4				205.8
42 43		7 29.7		65.8	65.8	42	A CONTRACTOR OF THE PARTY OF TH	100.4			135,8		1 0	171.1		206.5	
44		31.1		66.5	66,5	44		101.8			137.2			E CO. C. C.			
45		31.8			67.2	45	102.5				137.9		173.2				208.6
46		5 32,5			67.9	-	-	103,2	_		138.6		-	173,9		-	
47		2 33.2			68.6	47		103.9	97	139.	139.3	47	174.6	174,6	97		
48		9.933		69.3	69.3	43	104,6	104,	98	140.0	140.0	48	175.4	175.4	98	210.7	210,7
49	34,	6 34.6	The state of the state of	70.0	70.0	49	105.4	105.4	99	140,7	140.7	1 49	176,1	176.1	99	:11.4	
50		4 35.4			70.7				200	141.4	141.4	250	76,8	176 8	300	2 12.1	212.1
Dit	De	Lat	Dif	Dep	Lat	Dif	Dep	Lat	Dif	Dep	Lat		Dep	Lat	Dit	Dep	Lat
1				·					-								

Numbers for the readier finding the Course in the foregoing Tables of Difference of Latitude and Departure.

)ift	and D	iff. o	Lat.		Dift.	aud	Depai	rture	Ī	Diff	of La	t. and	Dep
No	Deg.	Nº	Deg		No	Deg.	Nº	Deg.		No	Deg.	Nº	Deg
000	1	17	89		17	1	1000	89		2	1	5882	89
999	2	35	88		3	2	999	88		3	2	2855	88
998	3	52	87		5	3	9,8	87		5	3	1908	87
997	4	70	86		70	4	997	86		7	4	1432	86
996	5	87	85		87	5	996	85		9	5	1145	85
995	The same of	105	84		105	200	995	84		10		950	84
993	7	122			122	7	993	83		12	7	816	83
990	8	139	82		139	8	990	82		14	8	711	82
988		156	-		156	-	988	-		.6	9	632	81
985	10	173			173	10	985	80		18	10	568	80
982	11	191	79		191	11	982	79		19	11	515	79
978	12	208	1		208	1	978			21	12	470	341.00
974	13	225			225		974	77		23	13	433	77
970 966	14	242			242	14	970	76		25	14	401	76
961	15	259 276	75		259 276		961	75		29	15	373	75
956	17	292			292		956			30	17	349	74
951	18	309			309					32	18	308	
		_			-		951	1		-	-	-	-
945	19	326			326		945	71		34 36	19	290	71
940	20	342	70		342	20	9.10			38	21	275 26c	70 69
934	22	358	1		358 375	22	934	68		40	22	248	68
921	23	375	67		391	23	921	67		42	23	236	67
914	24	407	1		407	24	914	66		45	24	225	66
906		423			423		906			47	25	214	
899	26	438	64		438		899			49	26	205	6.
891	27	454	63		454		891		10000	51	27	196	
883	28	470			470		883	1		1 53	28	188	62
875		485			485		875	61		55	29	180	61
866	30	500	2 3		500		866			58	30	173	Treatment of
857	31	515			515		857			60	31	166	Mary to the
848	32	530	59		530	32	848	58	1917	62	32	160	1 21
839	32 33	530 545	57		545	33	839	57		65 67	33	154	57
829	34	559	56		559	34	829	56		67	34	148	56
839 829 819	35	574	55		574 588	35	819	55		70	35	143	55
809	36	588	54		588	36	829 819 809	54		73	36	138	54
799		602	53		602	37	799	53		75	37	133	53
799 788	38	616	52		616	38	799	53 52 51		75 78	38	128	52
777	39	629	51		629	49	777	51		181	39	123	51
766	40	643	51		643 656 669	40	766	50		84	40	1119	50
755	41	656	49		656	41	755	49		87	41	115	49
743	42	669	48	{	669	4.2	743	48		90	42	111	48
777 766 755 743 731	43	629 643 656 669 682	47		.082	43	731	47		93 96	43	107	47
719 707	44	695	40		695		719	46		96	44	103	46
707	45	707	1 45		707	45	1 707	45	***	100	1 45	100	1. 45

The Use of the Table of Difference of Latitude and Departure in working any of the Cases of Plain Sailing.

N these Tables, the Course is less than 4 Points, or 45 Degrees, will be found at the Top of the Tables; but, if it is more than 4 Points, or 45 Degrees, it will be found at the Bottom of the Tables; and on every Side there are six Columns for the Distances, marked Dist. which contains 50 Miles in each Column, the first beginning at 1, and at 50; the second beginning at 51, and ending at 100; and so on to 300 Miles Distance; and to each of the Columns of Distance there helongs two other Columns, shewing the Difference of I atitude and Departure to any of the Distances marked Lat. and Dep. in which you are to observe, that if your Course be found at the Top of the Tables, then you are to take the Difference of Latitude and Departure as they are marked at Top; but if your Course be found at Bottom, then you must take them as they are marked at Bottom.

Note, If any Case where the Course is given in Points, half Points, or Quarters, you must make use of the following Tables of Difference of Latitude and Departure, which are calculated for Points, &c. but where the Course is given in Degrees, or where it is not given at all, you must make use of the foregoing Tables of Difference of Latitude and Departure.

PLAIN SAILING.

CASE the First.

Course and Distance being given, to find the Disserence of Latitude and Departure.

RULE.

Find your Course as before directed, and look in some of the Distance Columns belonging to that Course, for your Distance, the Dissernce of Latitude and Departure answering to that Distance, will be the Dissernce of Latitude and Departure required.

EXAMPLE

EXAMPLE I.

A Ship sails N.N.E. 136 Miles, I demand her Difference of Latitude and Departure.

Having found my Course, which is 2 Points in the Table for Points, I find my Distance 136 in the 3d Column for the Distances, and right against that, I find 125.7 Tenths for my Difference of Latitude, and 52.0 Tenths for my Departure.

Note, In all Cases whatsoever, if the given Side or Sides be in Miles, then the Sides found by the Table, will also be in Miles; but if the given Side or Sides be Leagues, then the Sides found will also be Leagues.

P

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T it n

Plain Sailing, Case the Second.

Course and Difference of Latitude being given, to find the Distance and Departure

RULE.

Find your Course as before, then look in some of the Difference of Latitude Columns belonging to that Course, for your Difference of Latitude, the Distance and Departure answering to that Difference of Latitude, will be the Distance and Departure required.

EXAMPLE II.

A Ship sails S. 48 Degrees 00 Minutes E. till her Difference of Latitude be 164 Leagues, I demand her Distance and Departure.

Having found my Course 48 Deg. at the Bottom of the Table in Page 42, I look in some of the Columns mark'd Lat. at Bottom, for the nearest I can find to my Difference of Latitude, which is 163.9, and answering to that, I find for my Distance 245 Leagues, and for my Departure 182.0 Leagues.

Plain Sailing, Case the Third.

Course and Departure being given, to find the Distance and Difference of Latitude.

R U L E.

Find your Course as before, then look in some of the Departure Columns belonging to that Course, for your Departure, the Distance and

and Difference of Latitude answering to that Departure, will be the Distance and Difference of Latitude required.

EXAMPLE.

A Ship sails South West by South until her Departure be 165 Miles. I demand her Distance and Difference of Latitude.

Having found the Course, which is 3 Points at the Top of the Table for Points, in Page 69, I look in some of the Columns marked Dep. at Top, for the nearest I can find to my Departure, which 165.0, and answering to that, I find for my Distance 297 Miles, and for my Distance of Latitude 246.9 Miles.

Note, In any Case where the given Side is too large to be found in the Tables, then divide it by 2, 3, 4, or any other Number that will reduce it enough to be found, and then the required Sides, when sound, must be multiplied by the same Number; but the Course must never be multiplied nor divided.

Plane Sailing. Case the Fourth.

Distance and Difference of Latitude being given, to find the Course and Departure.

R U L E.

Put two Cyphers to the Difference of Latitude, and divide it by the Diftance (without taking any Notice of the Comma that stands between the Miles and Tenths) and note the Quotient: Then look into the Table of Numbers, at the End of the Tables of Difference of Latitude and Departure, in the Columns belonging to Distance and Difference of Latitude, for the nearest Number to that Quotient, the Degrees answering to that Number will be the Course. Then to find the Departure, proceed as in Case I. But here you are to observe, that in all Cases where the Course is to be found by the Table of Numbers, the Difference of Latitude and Departure are supposed always to be in Miles and Tenths; as for Example, 112.4 Tenths, 207.9 Tenths, &c. so that if at any Time either of them should be given in Miles without Tenths; as 117,124, &c. you are then to put a Cypher to them, to supply the Place of Tenths, and call them 117.0 Tenths, 124.0 Tenths, &c. and then put two Cyphers more according to your other Rules to find the Number for the Course.

EXAMPLE.

A Ship sails between the North and West, until her Distance is 276 Miles, and her Difference of Latitude 211.4 Miles, I demand her Course and Departure.

Having put two Cyphers to the Difference of Latitude, which makes it 211400; I divide by the Distance 276, and find the Quotient to be 766 nearly; then I look into the Table of Numbers, under Dist. and Dist. of Lat. in Page 46) for the nearest to it, which is 766, against which I find 40 Degrees for my Course, and with that Course, and my given Distance, I find my Departure to be 177.4 Miles, by Case the first.

Plane Sailing. Case the Fifth.

Distance and Departure being given, to find the Course and Difference of Latitude.

RULE.

Put two Cyphers to the Departure, then divide it by the Distance, and look in the Table of Numbers, in the Columns belonging to Distance and Departure, for the nearest Number to the Quotient; the Degrees answering to that Number will be the Course, and then the Difference of Latitude may be found by Case the first.

E X A M P L E.

A Ship sails between the South and East, until her Distance is 546 Miles, and her Departure 412 Miles, I demand her Course and Difference of Latitude.

Having put a Cypher to my Departure to supplythe Place of Tenths, which makes it 412.0 and then two more Cyphers, according to the Rule for this Case, which makes it 412000, I divide it by the Distance 546, and find the Quotient to be 754, against the nearest to which, viz. 755 in the Table of Numbers, under Dist. and Dep. in Page 46, I find 49 Degrees for my Course; and with that Course, and my Distance (divided by 2, because it is too large to be found in the Tables) I find a Difference of Latitude 179,1 (Page 41, by Case the first) which multiplied by 2, because the Distance was divided by 2, gives 358.2 for the whole Difference of Latitude.

Plane Sailing. Case the Sixth.

Difference of Latitude and Departure being given, to find the Course and Distance.

RULE.

Put two Cyphers to the Departure, and divide it by the Difference of Latitude, then look in the Table of Numbers, in the Columns belonging to Difference of Latitude and Departure, for the nearest Number to the Quotient, the Degrees answering to that Number will be the Course; then to find the Distance, proceed as in Case the Second or Third.

EXAMPLE.

A Ship sails between the North and West, till her Difference of Latitude is 184 Miles, and her Departure 115 Miles, I demand her Course and Distance.

Having supplied the Place of Tenths in both these Sides, which makes them 184.0 and 115.0, I then put two Cyphers to the Departure, which makes it 115000, and divide it by the Difference of Latitude 1840, and find the Quotient to be 62; against which, in the Table of Numbers, under Difference of Latitude and Departure, I find 32 Degrees for my Course, and with that Course, and my Difference of Latitude, (by Case the Second) or with that Course, and my Departure (by Case the Third) I find my Distance to be 217 Miles.

Note, By these foregoing Rules for Plane Sailing, you may work any Case in Traverse, Mercator, Parallel, or Middle Latitude, only by supposing the Names of the Sides and Angles in Mercator, Parallel, and Middle Latitude, to be changed into the Sides and Angles they represent in Plane Sailing.

TRAVERSE SAILING.

The several Courses and Distances a Ship sails being given, to find what direst Course and Distance she has made good, and her Disterence of Latitude and Departure.

RULE.

Make a Table as on the following Side, and set down in it your several Courses and Distances; then, by the Rule for Case the first of Plane Sailing, find the Difference of Latitude and Departure to each

of the Courses and Distances, and set them down in the Table opposite to the Courses they belong to, taking Notice that the Difference of Latitude must always be set in the North Column, if the Course be Northerly, and in the South Column, if the Course be Southerly; and the Departure must always be put in the East Column, if the Course be Easterly,

and in the West Column, if it be Westerly.

Then add up all your Columns of North, South, East, and West, separately, and set down their respective Sums at the Bottom of each Column; and if you have but one Column of Northing or Southing, and but one of Easting or Westing, then their Sums will shew the Difference of Latitude and Departure of the same Name with the Column they stand under: That is, the Difference of Latitude will be Northerly, if it stands under the North Column; and the Departure Easterly, if it stands under the East Column, &c.

But if you have Numbers in all the Columns of North, South, East, and West, then take the Sums of the North and South Columns, and subtract the Less from the Greater, the Remainder will be the Difference of Latitude, of the same Name with the greater of them: Also do the same with the Sums of the East and West Columns for the Departure; then, with that Difference of Latitude and Departure, find the Course and Distance, as in

Case the Sixth of Plane Sailing,

E X A M P L E.

A Ship sails the following Courses, viz. SSW. 54 Miles, W. by S. 39, NW. by N. 40, NE. by E. 69, and NNW. 60 Miles, I demand her direct Course, Distance, Difference of Latitude, and Departure.

	Dift.	Diff. o	f Lat.	Dep	arture
Courses		North	South	East	West.
SSW	54		49.5		20.7
W by S	39		7.6		38.2
NW by N	40	33.3			22.2
NE by E	69	38.3		57.4	
NNW	60	55.4			23.0
		127.0 57.5		57.4	104.1 57·4
Diff. Lat	N.ly	69.5	DepV	V.erly	46.7

Note, 'Tis by this Method that the Difference of Latitude and Departure are found in working any Day's Work at Sea; and from the Difference of Latitude and Departure so found, we find the Course, Distance and Latitude by Dead-Reckoning, Meridian Distance and Longitude made; all which will be further explained in the Rules for keeping a Journal. Course N.34.00 W.

To work any Right-angled Triangle by the foregoing Rules for PLANE SAILING.

In all Right-angled Triangles which are to be worked by the Tables, you are to suppose four Things, viz. Course, Distance, Difference of Latitude, and Departure; two of which must always be given to find the other two: Then, as these Rules are designed for working of Plane Sailing, if you would work any other failing by them, as Mercator, Parallel, Middle Latitude, or any other Right-angled Triangle, you must suppose the Sides and Angles of that Triangle are called by the same Name as the Sides and Angles they represent in Plane Sailing are called by, and then work with them as if it was a Case of Plane Sailing.

The North and South Line in any Right-angled As for Example. Triangle (by whatever Name it is called in the Sailing it belongs to) must be worked as if it was Difference of Latitude in Plane Sailing: The East and West Line as Departure; the longest Side as Distance, and the Angle opposite to the East and West Line as Course. For Example, see the following

Figures.

Figure for Mercator's Sailing.

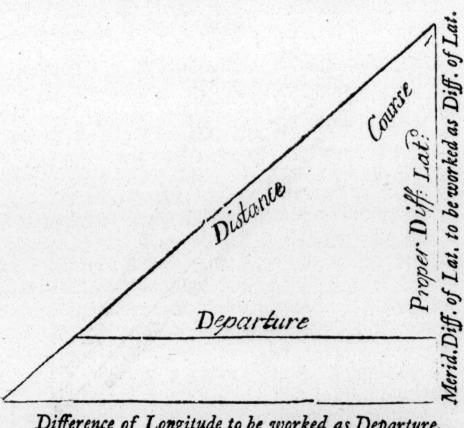
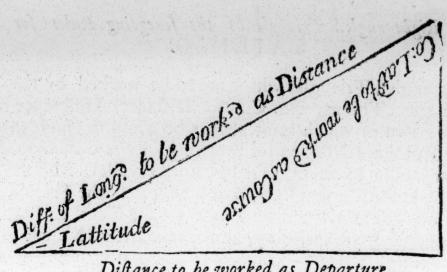
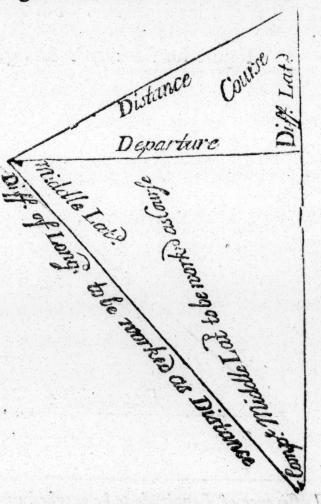


Figure for Parallel Sailing.



Distance to be worked as Departure.

Figure for Middle Latitude Sailing.



Mercator's Sailing. Case the First.

he Latitudes and Longitudes of any two Places being given, to find what Course and Distance a Ship must sail from one Place to another.

RULE.

Having the two Latitudes and two Longitudes given, find the proper difference of Latitude, the Meridional Difference of Latitude, and the Difference of Longitude, as by the Rules for that Purpose; then, with he Meridional Difference of Latitude, and the Difference of Longitude, taken as Difference of Latitude and Departure) find the Course by the sixth Case of Plane Sailing, and with that Course, and the proper Difference of Latitude, find the Distance by Case the Second of Plane Sailing.

X A M P L E.

What Course and Distance must a Ship sail from a Place in Latitude 50.00 North, and Longitude 03.10 West, to a Place in Latitude of 17.10 North, and Longitude 59.11 West.

Having put two Cyphers to the Difference of Longitude, and divided it by the Meridional Difference of Latitude, I find the Quotient to be 138, against which, in the Table of Numbers (under Difference of Latitude and Departure) I find 54 Degrees for my Course, and with that Course, and my proper Difference of Latitude, I find my Distance to be 3348 Miles.

The Course being thus found in Degrees, I want, in the next Place, to know which quarter of the Compass it is in, that is, whether it be so many Degrees from the North towards the East, or from the North towards the

West, &c. To do which, take the following Rule.

If you are to fail from a greater North Latitude to a less, or from North Latitude into South; or from a lesser South Latitude to a greater, then you must sail to the Southward.

But if you are to fail from a greater South Latitude to a less, or from South Latitude into North; or from a less North Latitude to a greater, you must sail Northward.

If you are to sail from a greater East Longitude to a less, or from a less West Longitude to a greater, or from East Longitude into West, you must sail to the Westward, except the Difference of Longitude be more than

180 Degrees, and then you must fail to the Eastward.

But if you are to go from a greater West Longitude to a less, or from a less East Longitude to a greater, or from West Longitude into East, you must sail to the Eastward, except your Disserence of Longitude be more than 180 Degrees, and then you must sail to the Westward.

EXAMPLE.

In the foregoing Case of Mercator's Sailing, I find by the two Latitudes that I am bound from a greater North Latitude to a less, viz. from 50.00 N. to 17.10 North, then by the Rule I must sail to the Southward; and I find by the two Longitudes that I am bound from a less West Longitude to a greater, viz. from 3.10 West to 59.11 West; then by that Rule I am to go to the Westward, therefore my Course will be South 54.00 West, or SW. three Quarters West nearest.

This first Case of Mercator, being the Case that is always made Use of to find the Course and Distance from Place to Place, or to find the Bearing and Distance of any Place from the Ship at any Time, I have set down the Work of it at large, and shall leave the other Cases for the Reader to exercise him-

felf with, by working them by the Rules already given him.

A Table of the Angies which every Point and Quarter Point of the Commakes with the Meridian.

	D	M	1	D	M	1	D	M	1' 1	1D	M
<u>1</u>	2	49	21/4	25	19	44	47	49	6½ 6½ 6¾	70	19
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34	8	20	$2\frac{3}{4}$	30	56	$4\frac{1}{2}$ $4\frac{3}{4}$	53		$6\frac{3}{4}$	75	
1	11	15	3	33	45	5	56	15	7	73	45
1 1	14	04	3 ½ 3 ½	36	34	5 1	59	04	71/4	81	34
$1\frac{1}{4}$ $1\frac{1}{2}$ $1\frac{3}{4}$	16	52	3 1/2	39	22	5 1/4 5 1/2 5 3/4	59	53	7 ¹ / ₄ 1 7 ¹ / ₂ 3 7 ³ / ₄	84	23
$1\frac{3}{4}$	19	41	3 3 3 4	42	11		64	41	73	87	11
2	22	30	4	145	02	6.	67	3c	8	130	09

The Use of this Table is to turn Points into Degrees, or Degrees into Points, as sollows: Suppose I would know how many Degrees 5 Points are, then I look for 5 Points, and against it I find 56 Deg. 15 Min. Or, if I would know how many Points 42 Deg. 17 Min. are, I look for the nearest to it, which is 42 Deg. 11 Min. and against that stands 3\frac{3}{4} Points.

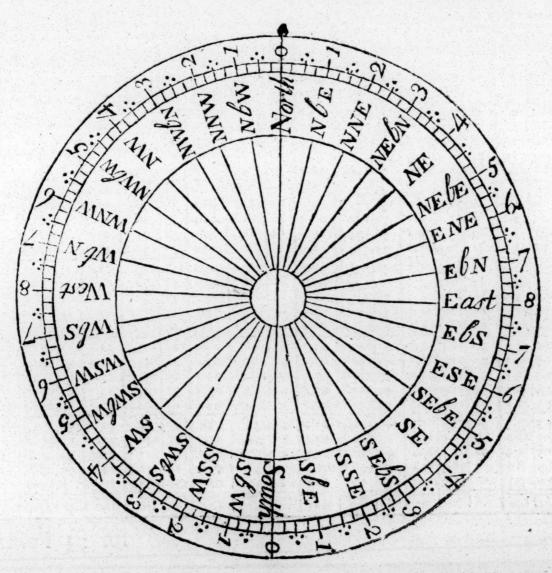
The Course and Distance being set down in a Traverse-Table, as in Page (52) it will be found necessary for the ready looking them out in the Table of Difference of Latitude and Departure, to know what Angles they make with the Meridian, (or as we commonly say) to know how many Points there are, for which Reason I have here given the Figure of the Mariner's Compass, which is to be used as follows.

Example ist. Suppose I would know how many Points I must look out for in the Tables of Difference of Latitude and Departure, for a

SW. by W. Courfe.

Look in the Figure below, and against the Point mark'd with SW. by W. you will see the Figure 5, which shews that you must look out for 5 Points.

Example 2d. How many Points is E. by N. \(\frac{3}{4}\) E. against E. by N. I find 7, and my Course being \(\frac{3}{4}\) Points more, it makes $7\frac{3}{4}$.



58 Difference of Latitude and Departure for & Point.

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4	04.0	30.4	54	53 7	05.3	04	103.5	10,2	54	153.3	15.1	C4	203.0	20.0	54	252.8	24.9
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12	11,9	01.2	62	61.7	06,1	12	111.5	11.0	62	161.2	15,8	12	211.0	20.7	62	260.7	25.7
13	12.9	01.3	63	62.7	06,2	13	112.5	11.1	63	162.2	15.9	13	242.0	20.8	63	261.7	25.8
14	13,9	015	64	63.7	06.3		113.5	11.2	65	163.2	16.1	14	213.0	20.9	65	263.7	25.9
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18	17.9	21.9	69	68,7	06,7	19	118.4	11.6	69	168.2	16,5	19	217.9	21.4	60	267.7	26,4
19	10.9	02,0	70	69 7	06.8		119 4	11.7	70	169.2	16.6	20	218.9	21.5	70	268 7	26.5
-	-	02.1	71	70.7	07.9	121	120 4		171	170.2	16.7	221	219.0	21.6	-	269.7	26.6
21	21.9	32,2	72	71.7	27,0	100000000000000000000000000000000000000	121,4	A COLUMN TO THE REAL PROPERTY OF THE PARTY O	73	171.2	168	E 14 X2 3	210.9	21.7	271	270.7	26.7
22	1 .	02.2	73	72.6	37.1	23	122 4	12.0	73	172.2	16.9	100	221.6	21.8	72	271.7	26,8
23	1	02.3	74	73.6	07.2		123.4	12.1	74	173.2	17,0	24	222,9	219	74	272.7	26.9
25	100	02.4	75	74.6	07.3		124 4	12.2	75	174.2	17.1	25	223.9	220	75	273,7	27,0
26	-	02.5	76	75.6	07,4	126	125.4	12.3	176	175 2	17.2	226	224.	22.1	276	274.7	27,1
27	26,9	02,6	77	76 6	07 5	27	116.4		77	176.2	17.3	27	1259	22.2	77	275.7	27.2
28	27.9	02.7	78	77.6	27.6		127.4	12.5	78	177.1	17.4	28	226.9	22,3	78	276.7	27 3
29	10	02 8	79	78.6	27 7	29	128.4	12.6	79	178 1	17.5	29	227.9	22,4	79	277.7	27.4
30		02,9	80	79.6	07.8	30	129.4	12.7	80	179 1	17.6	30	228.9	22.5	80	278.7	27.5
31	30.9	03.0	81	80.6	08.9	131	130.4	12.8	181	180,1	17.7	231	129.9	22.6	281	279.6	27.6
32	31.8	23.1	82	81 6	08.0	32	131.4	12.9	82	181.1	17.8	32	230.9	22.7	82	280,6	27.7
33	32.8	03.2	83			33	1324	13.0	83	182.1	17.9	33	231.9	22.8	83	281,6	27.8
34	33.8		84	83.6	08.2		133.4	13.1	84	183,1	18.0	34	232.9	22.9	84	282.6	27.9
35	34 8	23,4		-	1-3		134.4	13.2	85	184.1		-	233.9	23.0	85	283.6	28.0
36	35.8	03.5	86	85.6	08.4	Sec. 45 (80) Sec.	135.3		186	185.1	18,2		234.9	23.1		284.6	28.1
1 37	136 8	03.6	87	86.6	08.5	37	136.3	13.4	87	186,1	18.3		235.9	23.2	87	285.6	28.2
38		03.7	88	87,6	08.6	38	137.3	13.5	88	187 1	18.4	38	236.9	23.3		286,6	28.3
39	38.8	33.6	09	30.6	08.7	39	138.3			188.1	18.6	39	237.9	23.4	89	287.6	28.4
	39 8	33.1.		39.6	-	100000	139.3		90			40	238.8		90	288,6	28.5
41		34.0	91	90.6	08.9	141	140.3		191	190.1	18.7	241	239.8	23 6	291	289.6	28.6
42		04,1					141.3			191.1	18.9	42	240.8		92	290.6	28.7
43	42 8			93.5			143.3		93	192.1	19.0	43	241.8	23.8	93	291.6	28,8
44		04.4	94		09,3		144.3		95	194.1	19.1	45	243.8	24.0	94 95	292.6	28.9
45	74.0										10.2	73	-	THE RESIDENCE OF THE PERSON NAMED IN			29.0
46	45.8	04.5			09.5		145.3	14.3	196	195.1	19.2	246	244.8	24.1	296	294.6	29.1
47 48	10.8	04.6	97 98	27.5	09.6	47	147.9	14.4	97 98	197 0		48	245.8 246.8	24 2 24 3		295.6	29.2
49	48.8	04.7	99	98.5	09.7		147-3	14.6	99	198.0	19.5	49	247.8	24.4	98	296,6	29.2
50		04.9	100	99.5	09.8	150	149,3	14,7	200	199.0	19.6	50	248.8	24 5	300	297,6 298.6	29.3
-	-	_	_				and the second		=	Dep			-		-		29,4
Dift	'Dep	Lat	Diff	Dep	ıLat	Dift	Dep	Lat	Dil	Dep	Lat	Diff	Dep	Lat	Litt	Dep	Lat
				30000						10 m							

for 7½ Points.

60 Difference of Latitude and Departure for 3 Point

Diff	LatiDe	olDi	ıt L	at II	Depl	Ditti	Lat	Dep	Dift	Lat	Dep 1	Ditt	Lat	Dep	Dift	Lat	Den
-	01.000.			-	-		-	14.8	-				198.8	-			
	02.000.			1.4		101	99.9			149.4	22.1	7 12 17	199.8	29.5		248.3	1. 4.
	03.00.	-		2.4		02	101.9	15.0		150.3	22.4	02	200.8	29.6		249.3	37.0
3	04.0 00.	-		3.4	11 11 11 11 11 11		102.9	15.3		152.3	22.6	04	2018	29.9	1. T. T. T. T. T.	251.2	37.1
7 1	04.9 00.				08.1	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	103.9	15.4	55	153.3	22.7	05	202.8	30.1	100	252.2	37.4
5	05.900.	-	-	-	03.2	-	104 8	15.5	156	154 3	22.9	206	203.8	30.2			-
X . Comment	06.901.			6 4	.8.4	07	105.8	15.7	.57	155.3	23.0	07	204,7	30.4	7 . T	253.2	37-5
	07.901.				08.5		106.8	15.8	58	156.3	23.2	08	205.7	30.5		255.2	37.8
	08.9 21.		59		03.6		107,8	16.0	59	157.3	23.3	09	206.7	30.6		256.2	38.0
10	09 9 01				08.8	10	108 8	16.1	60	158.3	23.5	10	207.7	30.8	60	257.2	38.1
11	10.901	6	61	60.3	08.9	111	109.8	16.3	161	159.2	23.6	211	208,7	30.9	261	258.2	38.3
12	11.9 01.	-			09.1	12	110.8	16.4	62	163.2	23.8	12	209 7	31.1	62	1. 1.	38.4
13	12.9 01	9 1	63 6	62.3	09 2	13	111.8	16.6	63	161 2	23.9	13	210.7	31.2	63		38.6
14	13.802	A	64		09.4	14	112.8	16.7	64	162.2	24,0	14	211.7	31.4	64	261.1	38.7
13	14.8 02	,2	65	64.3	09.5	15	113.7	16,9	65	163,2	24.2	15	212.7	31.5	65	262.1	38,9
16	15.8 02	.3	66		09.7	116	114.7	17.0	166	164.z	24.3	216	213.7	31.7	266	263.1	39.0
17	16.8 02				09.8	17	115.7	17.2	67	165.2	24 5	17	214.6			264.1	39.2
13	17.8 02			67.3	10.0	11.00	116.7	17.3		166.2	24.6	18	215.6	and the same of		265.1	39.3
19	18.802	2 4 1 7	-		10.1		117.7	17.5	69	167.2	24.8	19	216.6			266.1	39.5
20	19.8 02	,9	-	69.2	10.3	20	118.7	17.6	70	168.1	24.9	20	217.6		70	267,1	39.6
2 1	20.8 03			70.2	10.4		119.7	17.7	171	169,1	25.1	221	218.6		271	268.1	39,7
22	21,803	1	' 1		10.6		120.7			170.1	252	22	219.6			269.0	
23	22.703		. 31		10.7			1 441 4 1-		171.1	25,4	23	220.6			270.0	
24	23.703				10.8	Burn in	1			172.1	25.5	24				271.0	1. 57
25	24,7 03	-	75	74.2	-	-				173 1	25.7	25		-		272.0	
26	25.703			75.2		The same of				174.1	25.8					273,0	
27	26.7 04			76.2	1					175.1	26.0	- /	224.5			274.0	
28	28.7 04		78	77.1		100000	1			176 1	26.3	28	225.5	1			
30		1.4	79	79.1	1 3 93					177.1	26.4	30					
			81	80.1	-	-			-		26.5	-	-		_		
31		1.7		81.1			1		A	180.0		1000		1 200	The same of the		
32	- /	1.8		82,1		3				181.0	26.8		1		20 20 20		10.5
34	1 4	5.0	84	83.1		1 33		1		182 0	27 0	33	A Part of the last				1
35	1 . 11	5.1	85	84.1						183.0				100000000			
36		5.3	86	85.1	12.	_			_	184.0					_	282,0	
37	36.60	5.4	87	86.1	12,	8 37	TOF			185.0	27 4	37			8 87	283	42.1
		5.6	88	87,0	12.	9 38	136.	20.		185.0	27.6	3	235.		9 88	284.	42,2
39	35.60	5.7	89	88.0	13.	39	137.	20.		186,9	27.7	39	2 36.	4 35.	89	285.	12.4
40	39:60		90	-	13.	2 40	138.	5 20	5 90	187.9	27.9	40	237.	4 35.		286.	42,5
39 40 41	40.60	6.0	91	90.0	13.	3 141	139.		7 191	188.0		241	238.	4 35,	3 291	287.	8 42 7
42	41.50	6.2	92	91.0	0 13.	5 42	140.	5 20.	8 92	189.	28.	4	2 239.	4 35.	5 9:	2 288.	8 42.8
43		6.3	93		0 13	^			93	190.9				4 35.	6 9	3 289,	8 43.0
44		6.5			0 13.					191.0		-			8 9	4 290.	
45	44.50		95		13.			-	_	192.0		-		3 35,		5 291.	8 43.3
46	45.50		96	95.	0 14.	1 14	6 144.			193.	28	7 24	6 243.				8 43,4
47	140.50		97	95.	9 14.	2 4	7 145.	4 21.	6 97	194.	28,	9 4	7 244.	3 36.		7 293.	8 43.0
48	47.50	7.0			9 14.			4 21.		195.	8 29.			3 36	4 9	8 294.	
49		7.2	100	97.	9 14.			4 21.			8 29				5 9	295.	
50						_	_							_	_		_
Di	itt Dep'I	Lat	\mathbf{D}_{i}	l De	p La	t Di	It Day	l La	t Diff	Dep	Lat	Di	it De	p Lat	Di	ft Dep	Lat
		1		N 11.14	1			1			100				40, 40, 10		

Difference of Latitude and	Departure for 1 Point.
Lat Dep Ditt Lat Dep Ditt Lat Dep Dit	H Lat Den Dift Lat Den Dift

	D	iffer	en	ce d	of I	at	itud	e an	d l	Dep	artu	re	for	Po	int.	ADMINIO	61
Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep
1	35.75	60.2	51.	100	10.0		99.1	19.7	The state of the s	148.1	29.5	201	197,1	39.2	251	246.1	49.0
2	11000	00,4	52	51.0	The second	02	100.0	19.9	52	149.1	29.7	02	198.1	39.4	52	247.1	49,2
3		00.8	53	53.0	100	03	102,0	20.3	53	150.0	29.9	04	199,1	39.8	53	248.1	49.4
5		01.0	55	53.9	Section 1	05	103.0	20.5	55	152.0	30.2	05	201.0	40.0	54· 55	249.1	49.8
6	05,9	01.2	-	54,9	10.9	106	104.0	20.7	156	153.0	30.4		202.0	40.2	256	251.1	50,0
. 7	1000-100	01,4	57	55.9	11.1	07	104,9	20.9	57	154.0	30,6	07	203.0	40.4	. 57	252.0	50,1
8		01.6		56,9	1, 100		105.9	21,1	58	154.9	30.8	08	204.0	40,6	58	253.0	50.3
9	0.00	02.0		57.9 58.8		09	105.9	21.3	59	155,9	31,0	09	205.0	40.8	59	254.0	50.5
10	10.8	-	61	59.8	-	10	-	21.5	-	156.9	31.2	_	205.9	41.0	60	255.0	50.7
11	4 C C C C C	02.3	1 2 100	60.8		111	108.9	21.7	161	157.9	31.4	F. 1 . 1	206,9	41.2	62	256.0	50.9
13	The second second	02.5		61.8		13	110.8	22.0	10.00	159 8	31.8		208,9	41.4	63	256.9	51.1
14	13.7	02.7	64	62 8	12.5	14	111.8	22,2	64	160 8	32.0	1 1	209.9	41.8	64	258.9	51.5
15	-	02,9	65	63.7	12.7	15	112.8	22.4	65	161,8	32.2	15	210.8	42.0	65	259.9	51.7
16		93,1	66.	64.7		116	113.8	22.6		162.8	32.4	ALCOHOL: NO	211.8	42.1	266	260.9	51.9
17		03.3	67	65.7			114,7	22.8		163.8	32'6		212,8	42.3	67	261.8	52,1
18		03.5	68	66.7			115.7	23.0	68	164.7	32,8	A Parent	213,8	42.5	68	262.8	52.3
20		03.9	70	68.6		19	117.7	23,2	70	165.7	33.0	20	214.8	42.7	70	263.8 264.8	52.5
21		04.1	71		-	121	118.7	23.6	-	167,7	-		216,7	-	-	265.8	The second section is
22		04.3	72	10 m	14.0	22	119.6	23.8	171 72	168.7	33.4	100 Per 100	217.7	43.1	72	266.7	52,9
23		04,5	73	71.6	14.2	23	120.6	24.0	75	169.7	33,8		218.7	43.5	73	267.7	53.3
24		04.7	74	72.6		24	121.6	24.2	74	170.6	34.0	24	219.7	43.7	74.	268.7	53.5
25	-	04.9	7.5	_	14.6	25.	122,6	24.4	75	171.6	34.1	125	220.6	43,9	75	269 7	53.7
2.6	25.5	05,1	76	the state of the	14,8	126	123.6	24.6	176		34.3	226	221,6	44,1	276	270.7	53.9
27		05.3 05.5	77 78	75.5 76.5	15,0	27	124.5	24.8	77	173.6	34.5	27	222.6	44,3	77	271.6	54.0
29		25.7	79		15.4		126.5	25,0	179	174.6	34.7	1000	224.6	44.5	78.	273.6	54.2
30		05.9	80		15,6		127.5	25.4	180	176.5	35.1	30	225,6	44.9	80	274.6	54.4.
31		06.0	81	JAMES STREET	15,8	_	128.5	25.6	181	177.5	35-3	231	226.5	45.1	281	275.6	54.8
32	31.4	06.2	82	80.4	16,0	32	129.5	25,8	82	178.5	35.5	32	227,5	45.3	82	276.5	55.0
	32-4		83	81.4	16.2	-	130.4	26.0	83	179,5	35.7	33	228.5	45.5	83	277.5	55.2
5	33 3	06.6	84	82.4	16,4		131.4	26.1	84	180,4	35.9	3.3	229,5	45.7	84	278.5	55.4
35	1000	06.8				-	132,4	26.3	85	181.4	36,1	35	230.5	45.9	85	279-5	55.6
36		07.0	87	84.3 85.3	17.0	130	133.4	26,5	186	182.4	36.3 36.5		231.4	46.0	286	280.5	55.8
38		07.4	88	86.3	17.2		135.3	26.9	88	184.4	36.7		233.4	46,4	88	281.5	56.0 56.2
39	38.2	07.6	. 89	37.3	17,4	39	136.3	27,1	89	185,3	36.9	39	234.4	46,6	89	283.4	56.4
40	39.2		90	88.3	17,6	40	137.3	27,3	90	186,3	37.1	40	235.4	46,8	90	284.4	56.6
41	40.2	08.0	91	89.2	17.8	141	138.3	27.5	191	187.3	37,3	241	236.3	47,0	291	285,4	56.8
42	41.2	08.2	92	90,2	18.0	42	139.3	27.7	92	188,3	37.5	142	237.3	47,2	92	286.4	57.0
43	42.2	08.4	93		18.1		140.2		- E 18-11	189.3	37.7	43		47.4	93	287,3	57.2
44	44.1	08.8	94	93.2		44	141.2			190,2	37.9	44	239.3	47.6	94		57.4
46	-	09.0						11000000		THE RESIDENCE AND ADDRESS OF THE PARTY NAMED IN		246	M Inches	48.0	95 296		57.6
47		09,2	97	95.1	18.0	47			97		38.4	47	242,2	48.2	97		57.8
4.8		09.4	98	96.1	19,1	48	145.1	28.0		194.2	38.6	48	243.2	48,4		292.2	58.1
49	48.1	09.6	99	97,1	19.3	49	146.1	29.1	99	195.2	38.8	49	244.2	48.6	99	293.2	58.3
50	49:0	09.8	100	98.1	19.5	150	147,	29.3	200	196,1	39.0	250	245,2	48.8	300	294.2	158.5
Dift	Dep	Lat	Dift	Dep	Lat	Di	t Dep	Lat	Dif	Dep	Lat	Dif	Dep	Lat	Dif	Dep	Lat

for 63 Points.

for 7 Points.

62 Difference of Latitude and Departure for 14 Points.

Ditt	Lat	Den	Dial	1 00	Davil	m:a	Lat	Dep.	Dift	Lat	Dep	Diffe	Lat	Dep	Dift	Lat	De
		Dep	-		Dep	-		-	-	146.5	-	-		48.8	-		
		00,2	51		12.	101	98.0	24 5	151 52	147.4	36.9	A STATE OF A STATE OF	195.0		B	243.5	61. 61.
1		00.5		50.4		02	99 5	25.0	53	148.4	37.2	03	195.9	49.1		244.4	
		0.10	Market and the	51.4		04	100 6	25.3	54	149,4	37.4	C4	197 9	49.6	54	A TO A LOUIS OF	61
	1	01.2	55	53 4	13,4	05	101.9	25 5	55	150.4	37.7	05	198.9	49.8	55	ALCOHOLD DESCRIPTION OF THE PERSON OF THE PE	62
		01.5	56	54.3		106	102.8	25.8	156	151.3	37,9	206	199.8	50.1	-	248.3	62
	7 0	01.7		55,3	100	07	103.8	26.0	57	152.3	38.2	07	200.8	50.3	57	The state of the s	
	-	21.9		56.3		08	104.8	26.2	58	153.3	38.4	08	201 8	50.5	58	250.3	62
	38.7	72.2	59	57.2	14.3	09	105.7	26.5	59	154.2	38.6	09	202.7	50.8		251.2	62
10	29.7	32.4	60	58.2	14.6	10	106	26.7	60	155,2	38.9	10	203.7	51.0	60	252.2	63
11	10.7	32.7	61	59.2	14:8	111	107.7	27.0	161	156.2	39.1	211	204 7	51.3	261	1 23	63
12	11,6	02.9	62	60,1	15.1	12	108.t	27,2	62	157,1	39,4	1. 1. 1. 1	205.6	51.5		254.1	63
13		03.2		61.1	15.3	13	109.6	27-5	63	158.1	39.6		206 6	51.8		255.1	63
14		33.4				14	110.6	27.7	64	159.1	39.9		207.6	52.0		256.1	64
15	-	23.6	-	63.1	15.8	15	111.6	27.9	65	160.1	40.1	-	-	52,2		257.1	64
16		03.9	66	64,0	16.0	116	112.5	28.2	166	161.0	40.3		209.5	52.5		258.0	
17		04,1		65.0		17	113.5	28.4	68	162.0	40.8	Sec. 252	210,5	52.7		259.0	
18	17.5	04.6			16.5	18	114.5	28.9	69	163.9	41.1		212.4	53.0		260.9	THE RESERVE
20	A Later of	04.9		67,0		20	116,4	29.2	70	164 9	41.3	20	213.4	53.5	70	1	
21		05.1	71	68,9		121	117.4		171	165 9	41.6	-	214.4	53.7	-	262.9	-
22		05.3	72		17.5	22	118.3	29 4	72	166.8	41.8		215.3	53 9		263.8	66
23		05.6		70.8		23	119,3	29.9	73	167.8	42.0		216.3	54.2		264.8	
24		05.8	74	71.8		24	120 3	30.1	74	168.8	42.3	- T	217.3	54 4		265.8	66
25	44.3	06.1	75	72.8	18.2	25	121,3	30.4	75	169.8	42,5	25	218.3	54.7	75	266.8	66
26	25.2	06.3	76	73.7	18.5	126	122.2	30.6	176	170.7	42.8	226	219.2	54.9	276	267.7	67
27	26,2		77	74.7		27	123.2	30.9	77	171.7	43,0		220.2	55.2	77		67
28		o6.8	78	75.7	The State of the S	28	124.2	31.1	78	172.7	43.3	A	221,2	55.4		269.7	67
29	8 11	07.0	79	Will be	19.2	29	125.1	31.3	79	173.6	43.5		222,1	55.6		270.6	67
30	-	07.3	80	-	-	30	120.1	31.6	80	174.6	43.7	30	223.1	55.9	80	-	68
33		07.5	81	78.6	1 1	131	127.1	31.8	181	175.6	44.0		224.1	56.1	281		68
32		97.8	82 83			32	128.0	32.1	82	176.5	44 2		225.0	56.4	8.	273.5	68
33	32.0 33.0		84		20.2	33	129.0	32.3	84	177.5	44.5	A SECOND	227.0	56.9	84	274.5	68
34	34 0		85		20.7	35	131.0	32.8	85	179 5	45.0		228.0	57,1	85	276.5	69
	-	08.7	86		20.9	136	131.9	-	186	180,4		236	228.9		286	277.4	-
36	13.			84.4	21.1	37	132.9	33.0		181.4	45.2	100	229.9	57·3 57.6	87	278.4	69 69
	35.9 36.9		88	85.4	\$1.4	38	133.9			182.4	45.7		230.9	57.8	88	279.4	70
39	37.8	09.5	89	86.3	21.6	39	134.8	33.8	89	183,3	45.9	39	131.8	58.1	89	280.3	70
40	38.8	09.7	90	87.3	21.9	40	135.8	34.0	90	184.3	46.2		232.8	58.3	90	281.3	70
41		10.0	91	88.3	22.1	141	136.8	34.3	191	185,3	46.4	241	233.8	58.6	291	282.3	70.
42	40.7	10.2	92	89.2	22.4	42	137.7	34.5	92	186,2	46.7	42	234,7	58.8	92	283.2	71.
	41.7			190,2	22.6	43	138.7	34.7		187.2	46.9		235.7	59.0		284.2	The second of
	42.7				22.8			35.0	94	188.2	47.1		236.7	59.3		285.2	71
45		10.9	95		23.1	45	140.7	35.2	95	189.2	47,4		237.7	59.5		286,2	71
46	44.6	11,2	96	93.1	23.3	146	141.6			190.1	47.6	246	238.6	59.8	296	28.71	73
47	45.6	11.4	97	194.1	23.6	47	142.6	35.7	97	191.1	47.9		239 6	60.0	97	288.1	72
48		11.7			23.8	49	143.6		99	192.1	48.1		241.5	60.3		289.1 290.0	72
49	18.5	12.2	100		24 3					194.0		50	242.5			291.0	
-	-	_	=			-		3					Dep	Lat			=
Diff	1	17	D	1117		112.0	1 7	Lat	D	Dep	Lat	D. V	D		T		La

Difference of Latitude and Departure for 1½ Points	6.
OLO 20.2 51 48 814 8 102 16 Dep Ditt Lat Dep	63

	Dit	Lat	Dep	Di	it L	at L)ep[[Ditt	Lat	De	7.0	Sitt T		1		-,-					03
	1	01,0	20.3	5	1 4	8.8	4.8	OI	96			itt I	-	Dep		it La	at IED	ep	ift	La	t Der
	2	01,9	00,6	5	2 4	9.8 1	5.1	02	97.6	29.			4.5	43.	49 "	1	.4 5	8.3	251	240.	_
ł	3	22.9		5			24	03	98,6	29.			5.5	44	1 1000 1	1 23	13 5	8,6	52	241.	2 73.1
	4	-	01.2	54		1.7 1		04	99.5	30,			7,4	44 4		1	- 1 -	8,9	53	242,	
1	5 6	24.8	01.5	5		1.6	6.c	05 1	100.5	30,			8.3	44,7				9.2	54	243.	
1			01.7	56				06 1	101.4	30.				45,0	-	-		9,5	55	244.	
1	, ,	06,7	4	57					02,4	31,0			9 3	45.2		1 31	1 5	7 7	256	245.	0 74.2
1		08,6		58		.5 16			03.4	31.5		8 15		45.5	08	10.00	14 15 10 10 10	0,0	57	245,	9 74.5
		29.6		59		,5 17			04,3	31.6	A	9 15	200	46.1	09	199,	Carl III	0.3	58	246.	- 1
	-1	-	-	-					05.3	31 9	6	0 15	3.1	46.4	10	201.		,9	59	247.	
		10 5		61	13		.7 11		06.2	32,2	16	1 154	1 1	46.7	211	201.			_	248.	
		2,4		63		.3 18			07.2	32.5	1	2 15		47,0	12	202	9 61	.2 2	62	249.	
	-	3.4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	64	61	2 18	-	-	08.1	32.8	1		0.0	47.3	13	203				250.	
			14,4	65	62	2 18	100		10.1	33,1	6	-	. 7	47.6	14	204.		100	-	251,7	
1.0		5,3	4.6	66		2 19	_		11.0	33.4	6	-	-	47,9	15	205.	8 62			253.6	
			49		64	1 19	4 1	· · · · · · · · · · · · · · · · · · ·	12.0	33.6	16	1 3		48.1	216	206,				254,6	
1			5.2	68	65.	1 19	7 1		12.9	33.9	68	00		48,4	17	207	7 62			255.5	
13	- 1		5.5	69	66.	0 20.	CI		13.9	34.5	60	1000	1. 2 6 1	18.7	18	208,6	63	,2	68	256,5	77.7
12	0 1	9,10		70	67,	-	3 2		14,8	34.8	70			19,0	19	209.6	1 3			257,4	
2	1 2	1 9	6.1	71	67.	9 20.		1 11	158	35.1	171		-	19.3	20	210.		_	70	258,4	78.3
1.			64	72	68.	9 20,	9 2:	11 2	6.8	35,4	72	164		9.6		211.5		1 2	71 3	259 3	78.6
12	- 1	200				9 21,		3 11	7.7	55.7	73			9.9		212,5			72 2	60.3	78.9
2 2		3.90	7.3		70.					36.0	74	166,		0 5		213,4				61,3	79.2
2		-			-	-	-	-	9.6	36.3	75	167	5 5	08		215,3	65.		4 2	62.2	79.5
2		,90	0		100	22.0			0.6	36.5	176	100	-		-	216.3		_		63.2	79.8
12	1	.8 38	100			22.				36.8	77	169.	. 1 2	1,3		217,2	65,			64,1	80,0
1 28		8c 8.				22.		100	-	37.1	78	170.	3 5	1.6		218.2	66.		7 2 8 2	65 I 66.0	80.3
30	28	.708	7			23.				37.4	79	171.		1,9		219.2	66.			67.0	80.6 80.g
31	29	.7 09	,0		77.5	-	-	-		37.7	80	172.	-	2.2	30	220.1	66.	8		68,0	81.2
32				Control of		23.8			5.4		181	173.		2 5 2	31 2	21,1	67.0	_	_ _	68.9	81.5
33		,6 og	.6	83 7		24.1		12		8.6	82	174.	1 -			22,0	67,		2 2	69.9	81.8
34				84 8	30 4		1 33	128		8.9	83	175.	1 -			23,0	67.6	8		708	82.1
35	33	5 10		85 8		-		120		9.2	85	177.0	1 -			23.9	67.9	8.	4 2	71.8	82,4
36	34	-		86 8	2.3	24.9	136	130	10.10			178.0	1-			24.9	68.2	4.50	5 2	72.7	82.7
37		4 10	,7 8	37 8	3.3	25.2	27	131	1.1 3	9.7	87	179.0	1 23			25,9	68.4		5 27	73.7	82,9
38		3 11	.0	8 8	4,2	25.5	38	132	2.1 4	0.0	88	179.0	EA	.5	37 2	26.8	68.7	8	7 27	73.7	83.2
40	37.	3 11	6 6	9 8	6.1	25.5 25.8 26.1	39	133		0.3	89	180,9	54		38 2 39 2	27,8 28.7	69.0	88	27	6.6	83.5
39 40 41	30			0 8	-	-6	_	134		0.6	90	181.8	55		10 2	29,7	69.3	89	27	6.6	83.2 83.5 83.8 84.1
42	40	2 II.	9 9	1 8 2 8	7.1	26.4		134	,9 4	0.9 [01	182 8		.4 7	40 2	20.6	69.9	0.00		7.5	84.1
43	41.	2 12.	5 0	3 8	0.0	27.0	42	135	9 4	1.2	92	183,7	55	.71	12 2	31.6	70.2	291	27	8.5	84.4
44	42.	1 12.		4 9	0.0	27.3	43 44	130	\$ 4	1.5	93	184.7	56	.0	13 2	32,5	70.5	92	27	9.4	84.7
45	43,	1 13,	1 9	5 9	0 9	27,0 27.3 27.6	45	136 137 138	8 4		94	183,7 184.7 185,7	56	.3 4	14 2	33 5	70,5	94	28	1.4	85.0
45	44.	13.	3 9	6 9	1.0	27.8	146		- -	2,1	95	180,0	56	.6	6 2	30 6 31,6 32,5 33 5 34.5	71,1	95	28	1,4 2,3 3.3	85.0 85,3 85.6
47 48	45.	0 17.	6 9	7 9:	2.8	28.1	47	139	4	2.3 1	96	87.6	56	.8 24	6 2	35.4	-	296	28	2 -	2.0
48	45,	9 13.	9 9	8 9:	3,8	27.8	48	141	.6 4	2.9	97 1	80,5		.1 4	17	36.4	71.3	97	120	4.2	85,8
49	46.1	DIA.	2 0	0.104	1 . 71	2 X 7	14.0	142	,6 4		99 1	189.5	57	4 4	18 2	37.31	71,0	98	28	5,2	86.4
50	47.	14.	5 10	0 9	5.7	29,0	150	143	5 4		00 1	91.4	97 58	7 4	9 2	38.3	72.2	99	28	5,2	86.7
Dift	De	Lat	5 100 Di	ft D	ep	Lat	Dift	De					=			9.2	72.5	300	128	7,1	87.0
4 2				No.		4			PIL	at h	IIII	Dep	La	t ID	ialc)ep	Lat	Uill			Lat
		5 -			1										196				S. 115	-	

for 61 Points.

64 Difference of Latitude and Departure for 13 Points

Ditt	. 1 21	1:)	113.6	II at	1000	1. 1.11	Lat	Lilen	11).	LLat	1	1 1	11.	(Dan	1 :0	11	
1-	-		-	Lat	-	-			Drit	1	rep	On	-	Dep	_ift		Dep
1 1		30,3	51		17.2		95.1	34.0	151	142,2	50 9	201	189.2	67.7	251	236.3	84.5
2	32.8	30.7	52			02	97.0	34.4	52	143	51.2	02	190.2	63.0	52	237.3	84.9
3 4		01.3	53			04	97.0	35.0	53	144.c	51,5	03	191.1	68.7	* 53 54	238.2	85.2
5	04.7	1	55				98,0	35,4	55	145 9	52.2	05	193,0	690	55	240.1	85.5 85.9
6	-	32.0	56	-	-	-	99.8	55.7	156	146 0	52 5	206	194.0	69.4	256		86.2
7	156,6	81,1	57		19 2	07	100.7	36.0	57	147,8	52.9	07	194.9	69.7	57	241.0	86.6
8	07.5	02,7	58	54 6		08	101.7	36.4	58	148.8	53.2	08	195,8	70.1	58	142,9	86.9
9	08,5	03.0	59	155.5	19.9	09	102,6	36.7	59	149 7	53.6	09	196,8	70,4	59	2438	87.2
10	99.4	934	6	56,5	20.2	10	103.6	37.0	60	150 6	53.9	10	197,7	70.7	60	244.8	87,6
11	10 4	03,7	61	57-4	10.5	III	104.5	37.4	161	151 6	54.2	211	198.7	71,1	261	245,7	87,9
12	1	04.0	62	58,4	20.9	12	105.4	37.7	62	152.5	54.6	12	199,6	71.4	62	246.7	88,2
13		04,4	63	59.3	1 11 1 21	13	106.4	38.1	63	153.5	54.9	13	200,5	71.7	63	247 6	88,6
14	13.2		64		21.6	14	107.3	38.4 38.7	64	154 4	55.2	14	201.5	72.1	64	243.6	88,)
15	4.	-	65	-	21.0	15		-	65	155,3	55.6	15	202 4	72.4	65	249.5	89,2
16	15.1	05.4	66	1 2 2 2 2 2	22.2	116	109.2	39.1	166	156.3	55.9		203.4	72,7	266	250 4	89.6
17		35.7 36.1	68	1 0	22,6	17	110.2	39.4	68	157.2	56 2 56.6		204.3	73.1	67 68	2514	89.9
19		06.4	69		23.2	19	112.0	40.1	69	159 1	56.9		205.2	73.4	69	252,3	90.3
20		06.7	70		23.6		113.0	40 4	70	160 1	57.3		207 1	73.8	70	253.3	90.6
1	-	07.1	71	66.8	2 7.0	121	113.4	40.8	171	161.c	57.6	-	208,1				90.9
21		07.4	72	67,8	24.2	22	114,0	41.1	72	161.0	57.9		209.0	74.4	72	255.1	91.3
23		07.7	73	68.7			115 8	41.4	73	162,9	58.3		210.0	75,1	73	257,0	91.6
24		28.1	74	69.7	24 9	24	116.	41.8	74	163.8	58.6		210.9	75.4	74	258,0	92.3
25	23.5	08,4	75	70.6	25.3	25	117	42,1	75	164.8	58,9		211.8	75,8	75	258.9	92.6
26	24,5	08.8	76	71.F	25.6	126	1186	42.4	176	165.7	59.3	326	212,8	76.1	276	259 9	93.0
27	1	09,1	77	1	25.9	27	119.6	42.8	77	166,6	59,6	27	213,7	76.5	77	260.8	93.3
28	26.4	09 4	78	73.4	26.3	28	120.5	43.1	78	167.6	60,0	PA 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	214,7	76.8	78	261,7	93.6
29	1:7.3	29.8	79.		26.t	29	121,5	43.4	79	168.5	60.3		215,6	77,1	79	262.7	94.0
30	28.2	10.1	- 8c	753	-	30	122.4	43.8	So	169.5	60.6	3	216.5	77.5	80	263.6	94.3
31	29.2		81	76,3		131	123.3	44 1	181	170.4	61.0		217,5	77.8	281	264,6	94.6
32	30,1	10,8	82	77.2	27.6	32	124.3	44,5	82	1714	61.3	3	218.4	78.1	82	265 5	95.0
33	31.1	11.1	83		28.0	33	125.2	44,8	83 84	172.3	61,6	22	219.4	78.5	83	266.4	95.3
34	32 C	11.5	85	79 J	28.3	34 35	127 1	45.1	85	173 2 174.2	62,3	3 '	221,3	78.8	0	267.4	95.6
$\frac{35}{6}$	330		86	81.0			128.0		186		62.6	35		79.1			96.0
36	33.9	12.1		81.0	29,0	136	129 C	45,8 46.1	87	175.1		. 2 .	222,2	79 5	286	269.3	96,3
37	34.8	12.5	88	82 9	20.6	37	129,0	46.5	88	177.0	63,0	131	223,1	79.8	88	270.2 271.2	96,7
30		13,1	89		30,0	39	130.9	46.8	89	177.9	63.7		225,0	80.5	89	272.1	97.0
40		13.5	90	84,7	30,3	40	131.8	47,2	90	178.9	64.0	40	226.0	808	90	273.0	97.7
41	-		91		T. 100		132.8			179,8	64.3		226.9	81.2	291	274.0	98.0
42		14.1	92	86,6	31,0	42	133.7	47.5	92	180,8	64.7		227,8	81.5	92	274,9	98.3
43	40.5	14,5	93	87.6	31.3	43	134,6	48.2	93	181.7	65.0		228,8	81.8	93	275.9	98.7
44	41.4	14.8	94	88.5	31.7	44	125 6	48,5	94	182.6	65.3	44	229,7	82.2	94	276.8	99,0
45	42 4	15.2	95	90.4	32 C	45	136.5	48.8	95	183,6	65,7	45	230 7	82,5	95	277.7	99.4
45	43,3	15.5	96	90.4	32.3	146	137.5	49,2	196	184.5	66.0	246	231,6	82.9	296	278.7	99.7
47	44.3	15.8	97	91.3	32.7	47	138 4	49.5	97	185,5 186,4	66.3	47	232,5	83.2	97	279.6	100.0
48	45 2	16.2	98	92.3 93,2	33,0	48	139.3	49.8	98	180,4	66.7	48	233.5	83.5	98	280,6	100.4
49	46.1	16.5	99	93,2	33.3	49	140.3	50.2	99	187 4	67.0		234.4	83,9 84.2	99	281,5	100,7
50	-		100	94.2	33,7	150	===	50.5	=		67,4	-	235.4	04.2	300	282,5	101.0
Dift	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat	Dist	Dep	Lat	Dift	Dep	Lat
	A LONG						THE LAST		N. Carlot						W 2.4		

for 64 Points.\$

Difference	ot	Latitude and	Departure for 2	Points	6
		=unitude und	Departure for 2	1 OHITS	O

15:41	Lat, De	Dift	Lat	Deni	Ditt	Lat	Dep	Dift	Lati	Dan I	Dia	Last	13.	15:01	7	- IN
Dill		_	-	-				Dift	Lat	Dep	Din	Lat	Dep	Dilt	Lat	Dep
1	00.9 00.		47.1	19.5	101	93.3	38.7	151	139.5	57.8	201	185.7	76 9		231.9	96.1
2	01.8 00.		48.0		02	94.2	39.0	52	140.4	58.2	02	186.6	77.3	52	232.8	96.4
3	02.801.	23			03	95.2	39.4	53	141.4	58.6	03	1\$7.6	77.7	53	233.8	96.8
4	03.701.	37		20.7	04	96.1	39,8	54	142.3	58.9	04	188.5	78.1	54	234.7	97.2
5 6	04.6 01.	37	-	21,0	05	97.0	40.2	55	143.2	59 3	05	189.4	78.5	_55	235.6	97.6
6	05.5 02.		51.7		106	97.9	40.6	156	144.1	59.7	206	190.3	78.8	256	236.5	98.0
7	06.5 02.	/	52.7		. 07	98.9	41.0	57	145.1	60.1	07	191.3	79.2	57	237.5	98.4
8	07.4 03.		1 1 1 1 1 1 1 1	22,2	08	99.8	41.3	58	146.0	60.5	08	192.2	79.6	58	238.4	98.7
9	08.3 03.		54.5		.09	100.7	41.7	59	146.9	60.9	09	193.1	80.0		239.3	99.1
10	09.2 03.		-	-	10	101.6	42.1	60	147.8	61,2	10	194.0	80.4	60	240.2	99,5
11	10.2 04.		56 4	19. 37 1	111	102.6	42.5	161	148.8	61.6	211	194,9	80.8	261	241.1	99.9
12	11.1 04.		57 3		12	103.5	42.9	62	149.7	62.0	12	195.9	81.1		242.1	100.3
13	12.005				13	104.4	43 2	63	150.6	62.4	13	196.8	81.5		243.0	100.7
14	12.9 05.			24.9	14	105.3	43.6	64	151.5	62.8	14	197.7	81.9		243.9	101.0
15	13.905.	-	-		15	106.3	44.0	65	152.5	03.1	15	198.6	82.3	65	244.8	101,4
16	14.8 06.	-	61.0		116	107,2	44.4	166	153.4	63.5	216	199.6	82.7	266	245.8	101.8
17	15.7 06.		100	1	17	108.1	44.8	67	154.3	63.9	17	200.5	83.0	67	246.7	102.2
18	16.6 06,		10. 15	26.4	18	109.0	45.2	68	155 2	64.3	18	201.4	83.4		247.6	
19	18.5 07.			26,8	2.5	109.9	45.5	69	156.1	64.7	19	202.3	83.8	69	248.5	
20	-		10 .	-	20	110.9	45.9	70	157.1	65.1	20	203.3	84.2	70	249.5	103.3
2.1	19.4 08.		65.6		121	111.8	46.3	171	158.0	65.4	221	204,2	84.6	271	250.4	103.7
1 2 2	21,308.	01	10	27.6	22	112.7	46,7	72	138.9	65.8	22	205.1	85.0	72	251.3	104,1
23	2 3.2 09.		160 .	28.3		113.6	47.1	73	159.8	66.2	23	206.c	85,3	73	2.52.2	104,5
24	23.1 09.	, , ,	6-		24	115.5	47.5	74	165.8	66.6	. 24	207.0	85.7		253.2	
25		- / /			_		47.8	75			25			75	254.1	105.2
26	24,0 10	2		29.1	126	116.4	48.2	176	162.6	67,4	226	208,8	86.5	276	255.0	
27	25.9 10.		1	1	27	117.3	48.6	77	163.5	67.7 68.1	27	209 7	86.9		255.9	106.4
29	26.8 11.		1 2 2 2	30.2	29	119.2	49,0	78 79	165.4	68.5	28	211.6	1 0 .		256.9	
30	27.7 11.	1 1 2				120.1	49.8	80	166.3	68.9	30	212.5	88.0		258.7	1
	28 6 II.		S 0 P		-	121.0	_	181	167.2			213.4	88.4		-	
31 32	29.6 12,	710		31.4		122.0	50.1	82	168.2	69.3	231	214.4			259 6	1
33	30.5 12.	100			33	122.9	50.9	83	169,1	70.0	3 ² 33	215.3	89 2			
34	31.4 13.	- 1	77.6	32.1	34	123.8	51.3	84	170,0	70.4	34	216.2	89.6		262.4	1 0
35	32.3 15.			32.5	35	124.7	51.7	85	170.9	70.8	35	217.1	89.9		263.3	
36	33,3 13.				-	125.7	52.0		171.9	71,2	236	218.0		-	-	109.5
37		2 87		33.3	37	126.6	52.4	87	172.8		37	219.0	1 , 3	1 1 1 1 1 1 1		109.8
38	35.1 14.		81.3	33.7	38	127.5	52.8		173.7		38	219.9	91.1			110,2
39	36.c 14.		81,2	34.1	39	128 4	53.2		174.6		39	220.8	91.5		267,0	110.6
40	37.0 15.	3 90	83.2	34.4	40	129 4	53,6		175.6		40	221.7			267.9	111.0
41	37.9 15.	7 91	84.1	34.8	141	130.3	54.0	191	176 5		241	2.22.7	92.2			111.4
42	38,8 16.	1 92	85.0	35.2	42	131.2	54.3	92	177.4	73.5	42	223,6		92		8.1118
43	39.7 16.	5 93	85,9	35.6	43	132.1	54.7		178,3	73.9	43	224.5	93.0	93	270.7	112.1
44			86.9	136.0	44	133.0		94	179.2	74 2	44	225.4	93.4		271.6	112.5
45			87,8	36.4	45	134.0	55.5	95	180.2		45	226.	93.8	99	272 6	112,9
46	42 5 17.		88.7	36.7	146	134.9	55.9	196	181.1		246	227.	94.1		273.5	113.3
47	43,4 18.	0 97	89.6	37.I 37.5	47	135.8	56,3	97	182.0	75.4	47	228,		97	274.4	1113.7
48			90.6	37.5	48	136.7	. 56.6	98	182,9	75.8		229.				114.0
49			91.5	37.9	49	137.7	57.0	99	183.9	76.2	49	230,	95.	9	276.	3 114.4
50		_	-	-	1;0	138.6	57.4		184.8	76.5	-			300	277.	1148
Di	DepLa	t Di	d Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat	Dif	Dep	Lat	Di	A Dep	Lat
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15-10

43.10

for 6 Points

66 Difference of Latitude and Departure for 21 Points

Diff Lat Dep Diff Dep Diff Dep Lat Diff Dep Lat						******					~ .	7:0:	7	D .	D:01			
2 0 1	Ditt	LatDep	Dut	Lat	Dep	Dift	Lat	Dep,	Dift	Lat	Dep	-			Dift	Lat	Dep	
2 01.50.09 5 2 47 6 2.23 02 93.2 43.6 52 137.6 65.0 02 183.6 86.4 53 227.8 107.8 1 93.7 03.8 1 93.8 1 9	I	00.9 00.4	51	46.1	21.8	101	91.3	43.2	151	136.5	64.6	201	81.7	85.9	251	226.9	107.3	1
3 01, 701, 31 53 47, 922, 71 03 93, 11 440, 51 138, 365, 4 03 183, 3 86, 53 1283, 7103, 6 04 184, 6 13, 144, 6 157, 2 04, 184, 6 187, 2 05, 149, 17 184, 184, 184, 184, 184, 184, 184, 184,	2	01.8 00.9				02	92.2				65.0			86.4	52	227.8	107.8	
4 03 601.77 54 48.8 33.1 04 94.0 44.5 54 139.0 65.8 04 184.4 87.2 54 229.0 105.6 6 03.4 20.6 55 50.2 3.9 106 95.8 45.3 156 140.1 66.7 206 185.3 87.7 55 230.5 109.6 60.3 23.0 57 51.5 14.8 40 70 96.7 45.8 15.7 141.5 67.1 07 147.1 88.5 57 143.1 149.9 5 07.2 03.1 03.8 15.2 14.8 15.8 97.6 45.2 58 142.8 67.6 68 188.4 88.9 55 63.3 12.1 190.9 190.0 14.1 60 54.2 57.7 10 99.4 47.0 60 144.1 68.4 10 189.8 89.8 60 23.5 111.2 11 09.9 24.7 6 1.5 51.26.1 111 11 10.3 47.7 16.8 15.5 12.6 111 11 10.3 47.7 16.8 16.5 16.5 16.5 16.5 16.5 16.5 16.5 16.5	3	02.7 01.3	53	47.9	22.7	03	93.1				65.4	. 03	83.5	86.8	53	228,7	108.2	1
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6 05.4 02.6 55 50.6 23.9 106 95.8 45.3 156 141.0 66.7 206 186.2 88.1 256 23.1-4 109.5 7 205.3 25.0 57 11.5 24.4 07 96.7 45.8 57 141.5 67.1 01.7 18.5 57 23.3 10.9 9 20.1 10.9 15.8 15.8 15.8 142.8 67.6 08.8 12.9 18.8 1.8 1.8 1.8 1.9 10.9 10.9 10.9 11.0 10.9 11.0 10.9 11.0 10.9 11.0 11.0	1	04.5 02.1		1	1	05					66.3	05	185.3	87.7	55	230,5	109.0	1
7 26 3 3 3 0 5 7 8 1.5 24 4 8 07 96.7 45.8 5 7 141.5 67.1 07 127.1 88.5 5 7 23.2 10.9 9 8 0 7.2 203.4 5 5 8 2.4 24 8 0 8 97.6 46.2 58 4 42.8 67.6 68.0 188.6 88.9 59 9 3.1 203.2 204.1 6.0 34.2 25.7 10 99.4 47.0 60 143.4 68.4 10 169.8 89.8 60 23.5 111.0 10 209 204.1 6.0 35.1 26.1 11 100.3 47.0 60 144.6 68.4 10 169.8 89.8 60 23.5 111.2 11 209.9 24.7 61 55.1 26.1 11 100.3 47.5 60 146.4 69.3 11 191.6 90.6 62 13.5 111.6 13 11.8 25.5 63 57 26.9 13 102.1 48.3 63 147.3 97.1 191.6 90.6 62 13.5 111.6 14 12.7 20.0 64 57 9 1.74 14 103.0 48.7 64 148.2 70.1 14 193.4 91.5 62 13.5 111.6 15 13.6 20.4 20.5 20.9 21.6 103.0 48.7 64 148.2 70.1 14 193.4 91.5 63.8 23.5 113.3 16 14.5 50.8 66 59.7 28.2 116 104.8 49.6 165 150.0 71.0 116 155.2 92.4 266 240.4 13.7 18 16.3 207.7 67 20.6 28.6 17 195.8 50.6 67 151.0 71.4 17 196.1 92.8 69 24.4 11.3 197.0 93.2 68 24.2 114.6 197.0 18.1 199.0 90.0 71 64.2 30.4 121 109.4 57.5 67 10.6 24.0 10.5 10.5 20.0 10.0 10.5 20.0 10.0 10.5 20.0 10.0 10.5 20.0 10.0 10.5 20.0 10.0 10.5 20.0 10.0 20.0	-		-		-	106			-	141.0	66.7	206	186.2	88.1	-	231.4	100.5	1
8 07.2 03.4 58 52.4 24 8 08 97.6 46.2 58 142.8 67.6 08 188.6 88.0 58 83.3 1103 9 0 30 103.8 53 33.3 25.4 0 98.5 46.6 59 143.7 68.0 05 188.0 89.4 99 23.7 1107 10 20 0 20 0 4.1 60 54.2 25.7 10 99.4 47.0 60 144.4 68.4 10 189.8 89.8 69.4 99 23.7 1107 1107 110 20 14.5 110 20					1					37400 300							1	1
9 3\$,103.8 59 53.3 25.9 09 98.5 46.6 59 143.7 68.0 09 188.9 89.4 59 23.4 11.10.7 10.0 09 00.4 16.5 54.2 25.7 10.0 99.4 47.0 65.0 143.6 65.4 10.1 189.8 89.8 00.2 3.5 11.2 19.0 19.0 19.0 19.1 12.5 12.5 12.5 12.5 12.5 12.5 12.5 12		F		1	1	-		46.2				at the same						1
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Difference of Latitude and Departure for 21 Points

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2	01,	80.9	52	2 45,	9 24.	02	90.0		52				1 0		A 100 PM	221,4	
3	32.	01.4	53	46.	7 25.0	03	90 8	48,5			C. C		10 TO 1	1		222,3	
4	03,	3000	2		6 25.4	04	91.7	49,0	54			1 3	1 2 20 50			223,1	119.2
5	-	02.4	55	48.	5 25.9	05	92.6	49.5	55				180,8	96.1	3.	224.0	
6	05,	3 02.8	56	49.	4 26.4	106	93,5	49.9	156			1-	-	-	-	224 9	
7		03.3	57		3 26,0		94.4	50.4	57		73.5	100	182.6	1		225,8	
8		03,8	58		2 27,3		95.3	50 9	58				183,5	97.5	-	226.7	
9		04.2	59		27.0		96.1	51.4		12/2 /		100	184.3	98,0	-	227,6	
10	08,8	94,7	60	52.	28.3	10	97.0	51,8	60	A		10	185,2	98.9	1 00	228.4	122.0
11	09.7		61	53.8	3 28.7	111	97,9	52.3	161	142,0	-	_	186,1	-	60	229,3	122,5
12		05.7	62	54	29,2		98,8	52 8	62		1 . 2 . 2		180,1	99.4	1 1 1 1 1 1 1 1 1 1	230.2	123.0
13		06.1	63		29.7	13	99.7	53.2	63			12	187,0	99,9	62	231,1	123.4
14	1000	06.6	64		130,2	14	100.5	53.7	64			13	188,7	100.4	63	232,0	1239
15	13.2	-	65		30,6	15	101.4	54.2	65			15	189.6	100,8	64	232,8	124.4
16	4.1		66	58,2	31,1	116	102,3	54.7	166	146.4	Comments and American	-		-	65	233 7	124.9
17		0.80	67	59.1	31.6		103.2	55.1	67	147,3		216	190.5	101.8	266	234.6	125.3
18		08,5	68		32,0	18	104,1	55.6	68	148.2	79.2	17	191.4	102.2	67	235.5	125,8
19		09,0	69		32.5	19	105.0	56 1	69	149,1	79.6	18	14	102,7	68	236.4	126.3
20	-	09.4	70	61.7	33,0	20	105.8	56.5	.70	149 9		19	193,2	103.2	69	237.3	6.7
21	18.5	09.9	71	62.6	33.5	121	106.7	57.0	171	150.8	80.6	-		103.7	70	238.1	127.2
22		10.4	72		33.9	22	107.6	57-5	72	151.7		221	194,9	104.1	271		127.7
23	20.3		73		34.4	23	108.5	58.0	73	152.6	81.5	22	195,8	104.6	72		128.2
24	Total Control	11.3	74	55.3	34.9	24	109.4	58,4	74	153.5	82,0	23	196,7	105,1	73	Contract of the last	128.6
25	22.1	11.8	75	66.2	35.3	25	110.3	58,9	75	154 3	82.5	24	198.4	105.5	74	241.7	129.1
26	22.9	12.3	76	67,0	35,8	126	111.1	59.4	176	155,2	82.9	25		_	75	242,5	129 6
27	23.8	12.7	77	67.9	36.3	27	112.0	59,8	77	156.1	83.4	226	199,3	106 5	276	2434	130.0
28	24,7	13,2	78	68.8	36.8	28	112.6	60,3	78	157.0	83.9	27	200,2	107.0	77	244.3	130.5
29		13.7	79	69.7	37.2	29	113.8	60.8	79	157.9	84.3	28	201.1	107.4	78	245,2	131.0
30	20.5	14.1	80	70.6	37.7	30	114.7	61.3	80	158.8	84.8	29	202 9	107.9	79 80	246.1	131.5
31	47.4		81	71.4	38.2	131	115.5	61.7	181	159.6	-	30		None and a second	_	247.0	131.9
32		15.1	82	72.3	38.6	32	116.4	62,2	82	160 5	85.3 85.8	231	203.7	108.8	281	247.8	132.4
33		15.5	83	73.2	39.1	33	117.3	62.7	83	161.4	86.2	3	204.6	109.3	82	248.7	132,9
34		16.0	84		39.6	34	118 2	63,1	84	162,3	86.7	22	205.5	109.8	83	249.6	133.3
35	-	16 5	85	750	10.1	35	119.1	63.6	85	163.2	87.2		207 3	110.3	84	250.5	133.8
36	31.8	17.0		75.9		136	120,0	64.1		164.1	87.6		208,2	-	85	251.4	134.3
37	32 6	17.4	87		41.0	37	120.8	64.5		164.9	88.1	3		111.2	286	252,3	134,8
38	33 5	17.9	88	77.6	41.5		121,7	65.0	88	165.8	88.6		209.9	111.7	87	253.1	135,2
39	34.4	18.4		78.5			122.6	65.5	89	166,7	89.1		210.8	112,1	88	254 0	135.7
40		18.9	90	79.4		40	123.5	66.0	90	167.6	89.5		211.7	113,1	89	254,9	136.2
41	36.2	19.3	91	80 3	42.9	141	124.4	66.4		168 5		_			90		136,6
42	37.0	19.8	92	81.1	43.4		125.2	66,9		169.3	90,5		212,6	113,5	291		137,1
43	37.9	20.3	93	82.0	43.8		126.1	67.4		170.2	90,9		213,4	114.0	92		137.6
44	,8.8		94	82.9 83.8	44 3	44	127.0	67.8		171.1	91,4		215,2	114.5	93	258,4	138.1
45	39.7		95	83.8	44 8	45	127.9	68.3	95	172.0	91.9		216.1	115.4		259.3	130.5
	40 6		96	84,7 85.6	45,2	146	128.8			172.9	-				-		1390
	41.5		97	85.6	45.7	47	129.7	69.3	97	173.8	92.8		217.0	115.9	296	261,1	139.5
	42.3		98	86,4	46.2	48	130.5	69,7		174.6	93.3	47	218.7	116.4	97	262.0	39,9
49	43,2	23.1	99	87.3	40.6	49	131.4	70.2		175.5	93,8		219.6	117,3	98	262.8	
	44.1	_	100	88.2	47,1	150	132.3	70,7	200	176.4			220.5	-	300		140.9
Dill	Dep	Lat	Dift	Dep	Lat		Den			Dep		250				-	141.4
					diam'r.		-P 1		2110	Depi	Lat	Dift	Dep	Lat	Diff	Dep	Lat
																St. Berlins	A 12 1 1 1 1 1 1

for 5½ Points.

	1000	A					1				a same						
Din	Lat	Dep	Dift	Lat	Dep	Ditt	Lat	Dep	Ditt	Lat	Dep	Dift	Lat	Dep	Dift	Lat	Dep
1	20.9		51	43,7	26.2	101	86.6	51.9	151	129.5	77.6	201		103.3	251	215.3	129.0
2	21.7		52		26.7	02	87.5	52.4	52	130.4	78.1	C2		103.8	1	216.1	129.5
3	02.6		53		27.2	0	88.3	52.9	53	131.2	78.6		174.1		-	217.0	130.0
4	04.3	02,1	54	17.2	27.8	04	89.2 90 I	53.4	54	132.1	79.1 79.7	04	. 0	104.8	3,1	217 9	130.5
5 6			55		28.8			54.0	55	-	80.2	-	176.7				131.0
	05.0		56		29.3	106	90.9	54.5	156	133.8	80.7	200	177.5		- 1	229.6	131.6
7 8	06.9		57 58		29.8	08	92,6	55 5	57 58	135.5	81.2	08	178.4		57 58	221.3	132.1
9		04.6	59		30.3	09	93.5	56.0	59	136.4	81,7	09	179.3	107.4	59	222.1	133.1
10	03.6		60	51.5	30.8	10	94,3	56.5	60	137.2	82,2	10		107.9	60	223,0	133.6
11	09 4	05.7	61	52 3	31.4	111	95.2	57.0	161	138.1	82.7	211		108.4	261	223.9	134.1
12	10.3	06.2	62	53.2	31.9	12	96.1	57.6	62	138.9	83.3	12	181.8	109.0	62	224.7	134.6
13	100	C. Single	63	1	32,4	13	96.9	58.1	63	139.8	838	13	182.7	109.5	63	225.6	135.2
14	12.0		64	54.9		14	97.8	58,6	64	140.7	84.3	14	183 5	110.0	64	226,4	135.7
15	12.9	-	65	55.8	-	15		59.1	65	141.5	84.8	15	184.4	110.5	65	227.3	136.2
16	13.7	08.2	66		33.9	116	99,5	59.6	166	142.4	85.3 85.8	216	185.3	0.111	266	228.1	136.7
17	14,6		67 68	57.5	34.4	17	100.4	60.1	67 68	143.2	86,3	17		111.6	67	229.0	137.2
18	16.3		69		35.5	10		61.2	69	145.0	86.9	19	. 0 . 0		69		137.7
19		10.3	70	60,0	36.0	20	102.9	61.7	70	145.8	87.4	20	188.1	113.1	70	231.6	138.8
21	-	10.8	71	60.9	-	121	103.8	62.2	171	146.7	87.9	221	189.6		271	232.4	139.3
22		11.3	72	61.8	1 2 1 1 1	22		62.7	72	147.5	88.4	22	190,4		72	233.3	139,8
23	197		73	62.6	37.6	2:	105.5	63.2	73	148.4	88.9	23	191.3			234.2	140.3
24	20.6	1 -	74	63.5	38.0	24	106,4	63.7	74	149.2	89.4		192.1		74	235.0	140.8
25	21.4	12.9	75	64.3		25	107.2	64.2	75	150,1	89.9	25	193.0	115.6	7.5	235.9	141.3
26	22.3	13.4	76	65.2		126		64 8	176	151.0	90.4	226	193,8		1-1-		141.8
27	23.2	13.9	77	66,0			108.9	65.3	77	151.8	91,0		194.7			237.6	142.4
2.8	A BOOK	14.4	78	67.8	40.1	28		65.8	78	152.7	91.5	Acres 1	195.6				142.9
29	24.9	15.4	79 80	68.6	1 1	2 g 3 c	111.5	66.8	79 80	153.5	92.5		197.3			239.3	143.4
30	26.6	-	81	69,5	-	-	112.4		1-			1-	198.1			-	143.0
31	27.4		82	70,3		131		67.8	82	155.2	93.0		199.0	1 111	14		144.4
33	28.3		83		1	33	114 1			157.0	94.0		199.8		1		145.4
34	29.2	17.5	84	72.0	W 1	34	114.9		84	157.8	94.6		200 7	1000			146.
35	300	18.0	85	72.5	43,7	35	115 8	69 4		158,7	95.1		201.6	120.8	8 8 5	244 4	146.
36	30.9	18.5	86	73,8	44.2	136	116.6	69.9	186	159.5	95,6	236	202.4	121.3	286	245.3	147.0
37	31.7	19.0	87	74.6	44 7	37	117.5	70.4	87	160.4	96.1	37	203.3	121.8	87	246.2	147.
38	32.6	19.5	88	75.5	45.2	38	118.4	70.9		161.2				122.3	88	247.0	148.
39	33.5	20,0	89	70.3	45,7	39	119.2	71.4		162.1	97.1				89	247.9	
40	-	20.6	90	17.2	46.3	-	120.1			163.0		-		123.3	-	248.7	-
41	35.2	21.6			46.8	141	120.9	1 / 3		163.8	98.2	241	206,7			249,6	
42 43	36.0	22.1	92	70.	+7.8	42				165.5			208.	124.4	92	250.4	150.
44	37.7	22.6	94		18.3	44				166.4	99.7			125.4	93	252.2	150,
45	38.6	23.1	95	In		45		74.6		167,3	100.2				99		151.
45 46	-	23.6	96	-	49.3	_	125.2			168.1		_		126,4	-		
47	40.3	24.2	97	83.2	49.9	47		75.6	97	169.0	101,2	47	211.0	126.9			152.
48	41.2	24.7	98	84.	1 50.4	48	126.9	76.1	98	169.8	101.8	48	212.7	127.4	98	3 255.6	153.
49		25.2	99	184.0	150.9	49	127.8	76.6	99	170.7	102.3	49	213.6	128.0	99	256.	153.
50	42.9	25.7	100	-	51.4	-	128.7	77.1	200	171,5	102.8	250	214.4	128.5	300		3 154
Dil	De	Lat	Diff	De	Lat	Diff	Dep	Lat	Diff	Dep	Lat	Diff	Dep	Lat	Di	it Dep	La
1-			V. 1. 1.	1					-					11 1 1 1 1 1 1 1	100		

Difference of Latitude and Departure for 3 Points 69

-		100	.Di	411 04	1000	.D:6			200				Der Grand	9			,
Di		u Dep		Lat		Dift	Lat	Dep	Dit	t Lat	1 Dep	Dill	Lat	1 Dep	1 iti	Lat	Dep
	00,	8 20.6	51	42 4	28.3	101	84.0	56 1	151	125			-	-	-		Dep
1 2							84,8	56.7	1 -			201	167.1		251	208,7	139.4
1 3)2.	5 01.7			-		85.6	57.2				02	167 9			209.5	140.0
1 4		-1 '	33		A	1 3	86,5		1 33	127.2	1 3			112.8	53	210.3	140.5
		1 .				1	87.3			128.0	1 3 3	04	169.6	1113,3		211.2	141.1
5			-			-	-	58.3	1 00	128.0	86.1	05	170 4	113,9		212,0	141.7
6		0033		46.6		106	88.1	58,9	156	129.7	86.7		171.3	-	-	-	-
1 7	05,					07	89.0	59,4		130.5			172.1		256	212,8	142.2
8	06,	7 04.4	58	48.2	32,2	08	89.8	60,0		131.4	87.8					213,7	142.8
9	07.	5 05.0	59	49.1	32.8	09	90.t	60.5	1 3	132.2	88.3	1	172,9		58		143,3
10	03,	3 05.6	6		33,3	10	91.4	61.1		133.0		1	173.8	116.1	59	215,3	143.9
11	-	1 06.1				-				-	-		174.6	116.7	60	216.1	144.4
12		06.7				III	92.3	61.7		133.8	89.4	211	175.4	117,2	261	217.0	145.0
1 13 3		8 07.2			100	12	93.1	62,2		134.7	90,0		176.2	117.8	62	217,8	145,5
13		6 07.8		52.4		13	93,9	62.8		135 5	90,5	13	177,1	118.3	63	218.6	146,1
14			64		35,6	14	94.8	63,3		136 3	91,1	14	177.9	118.0	64	219.5	146.7
15	12,	-	65	-	36.1	15	95.6	63.9	65	137.2	91.7		178.7	119.4	65	210.3	
16	13.				36.7	116	96.4	64.4	166	138.c	92.2	-	-		-	-	147.2
17	14.	109.4	67	55.7	37.2	17	97.3	65.0	67	138.8	92.8		179,6	120.0	266	221,1	147.8
18	15,0	10,0	68	56,5	37.8	18	98,1	65.5	68	139.7	A CONTRACTOR	17	180,4	120,5	67	222,0	148,3
19	15.8	10.6	69	57.4	138.3	10	98,9	66.1			93.3	1	181.2	121.1	68	222,8	148.9
20	16,6	11.1	70	58,2	38.9	20	99.	66,7	69	140.5	93,9	19	182.1	121.7	69	223.6	149.4
1=	-	-		-	-	-		-	70	141.3	944	20	182.9	122.2	70	224 5	150.0
21	18.3	11.7	71	59.0	39.4	121	100.6	67.2	171	142,2	95.0	221	183,7	122,8	271	225,3	
22			72	59.9	40.0	22	101.4	67.8	72	143 0	95.5	22	184.6	123.3	72	226.1	150,5
23	19,1		73	63.7	40.6	23	102,3	68.3	73	143.8	96.1	23	185,4	123.9	73	227,0	151.1
24	20.0	13.3	74	61.5	11.1	24	103.1	68.9	74	144.7	96.7	24	186,2	124.4		2178	151.7
25	20.8	13.9	75	62.4	+1.7	25	103.9	69,4	75	145 5	97,2	25	187,1	the second second	74		152.2
26	21.6	14,4	76	53.2	42,2	126	104,8	70.0	176	146.3	-			125.0	75	228.6	152.8
27	22.4	15.0	77	640	42.8		105.6				97.8	226	187.9	125,5	276	229,4	153.3
28		15.6	78	64,8	43.3		106.4	70,5	77	147,1	98,3	27	188,7	126.1	77	230 3	153.9
20		16.1	79	65.7	43.9	29	107.2	71,1	78	148.c	98.9	28	189.5	126.7	78	231,1	154.4
30		16.7	80	66.5	14 4	-	108.1	71,7	79	148.8	99.4	29	190:4	127.2	79	231,9	155.0
-	25.8	-	-	-		30	-	72,2	80	149,6	0.001	30	191.2	127.8	80	232,8	155.5
31			81	67.3	45,0		108,9	72.8	181	150.5	100.5	231	192.0	128.3	281		-
32		17.8	82	68.2	45.6	32	109.7	73.3	82	151.3	101,1	32	192.9	128.9	82	233.6	156.1
33		18.3	83		46.1	33	110.6	73.9	83	152.1	4. "	33	193,7	129.4	83	234.4	156.7
34.	28.3	1	84	69.8	46.7	34	111.4	74.4	84	1530	102.2		194,5	130.0	84	235.3	157.2
35	39 1	19.4	85	70.7	47,2	35	112.2	75,0	85	153.8	102.8	34	195,4	130.5		36.1	157.8
36	29,9	20.0	86	71.5	47.8	136	113.1	75.5	186	-	-	35			85	236.9	158.3
37	30.8	20.6	87	72.3	48.3	37		76,1	87	154 6	103,3	235	196,2	131.1	286		158.9
38	31.6	21,1		73.2		38	114.7	76.7		155,5	103.9	37	197,0	131.7		238.6	159,4
39		21.7	80	74.0	49,4		115.6		00	150.3	104.4	38	197.9	132.2	88	239.4	160.0
40		22,2	90		50.0		116.4	77,2	89	157.1	105,0	39	198.7	132,8		240.3	160.5
1-	-	-	1-7-		-	-	-	77,8	90	158.0				133.3	90	241.1	161.1
41		22.8	91	75.7	50.6	141	117.2	78.3	191	158.8	106.1	241		A		-	-
42	34,9	23.3	92	76,5	31.1		118.1	78.9	92	159.6	106 7			134.4	291	241.9	161.7
43	35,0	23.9	93	77.3	51.7		118.9	79.4	93	160 4	107.2		7 7 7	135,0			162.2
44		24.4		78.1	52,2	44	119.7	80.0	94	161.3	107.8				93		162.8
45		25:0	95	79.0	52.8	45	120,5	80.5	95	162,1	108.2	1200		135.5		244.4	163.3
45 46	38.2	25.6	96	79.8	53.3		121,4	81,1	196	162 6		-		136.1	95	245,2	1639
47	39.1	26.1	97	30.6	53.9		122.2	81.7	190	162.9	108.9	2,042,00	204.5	136,7	296	246.1	164,4
48		26.7		81.5	54.4		123.0	82,2	97	163.0	109.4	47		- 5/24	97		165.0
49		27,2	99	82.3	55.0		123.9	80 0	98	164.6	110.0	48	206,2	137.8	98	247.7	165.5
50	41.6	27.8	100	83.1	55.6	150		82.8	99	165,4		49	207.0	138.3	99		166.1
				-			124.7	83.3	200		111.1	250	207.0	138.3	300		166.7
Dilt	Dep	Lat	Dift	Dep	Lat	Ditt	Dep	Lat	Dift	Dep	Lat	Dift		-		==	==
5 3										vp	Lat 1	OIII.	Deb	Lat	Dial	Dep	Lat
				7 1										•	-		

for 5 Points.

70 Difference of Latitude and Departure for 34 Points

-	71	1.5	-						-		1 70	-					
Dil	II La	t Dep	Ditt	Lat	Deb	Dit	Lat	Dep	Dil	Lat	Dep	Dift	Lat	Dep :	Dift	Lat	1 Dep
1	00.	8 00 6	51	41.0	30.4	10	81.1	60.2	151	121.3	90.0	201	161.4	119.7	25	201.6	-
2			52	1 0	31.0	0:	10	60 8		122.1	90.6	02	162.2	120.3		202.4	1,2,2
	1.00	8.10			31.6	0	82 7	61.4		122.9		03	Paris Print	120 9		4 2 1	150.1
3		2 02,4	5.3	33	32,2		0.	62.0		123.7	91.7		1	1215		204.0	150,7
4		03.0	54	43125	1 0	0		62.6		124,5	92.3	05	164.6	122.1	54	204.0	151.3
5			55		-	-	-	-	-	-		-			55	_	151.9
6		03,6	56	450		10	85.1	63.1		125.3	92.9	200		122,7	256		152.5
7		04 2	57		34.0	07		63.7	57	126.1	93 5	07		123.3	57	206,4	153.1
8		104.8	58		34.6	05		64.3	58	126.9	1	08		123.9		207.2	153.7
9		2054	59	47 4		cg		64.9		127.7		09		124.5		208.c	154.3
10	08.0	05.0	60	48.2	35.7	10	88.3	65.5	6c	128.5	95.3	10	168 6	125.1	60	208 8	154.9
II	08,8	06.6	61	49.0	36.3	111	89.1	66.1	161	129.3	95.9	21)	169.4	125.7	1.61	209 t	155.5
12		6 07.1	62	19.8		1 12	0	66.7	62	130.1	96.5	12	170.2	126,3		210,4	156.1
13		07.7	63	50.6		13		67 3		130.9		13		126.9		211.2	156.7
14		08.3	64	51 4	38.1	14		67.9		131.7	A TANK THE REAL PROPERTY AND ADDRESS OF THE PARTY AND ADDRESS OF THE PA	14	V 201 2	127.5		212.0	1.57.3
15	10	08.9	65	52 2	38.7	1	1	68.5	65	132.5	98.3	15	172.7	128.1	65	212.8	
- Commonio	-	09.5	-	-	-	-	-	-	-		98.9	-		128.7	-	-	157,9
16			66		39.3	116	The second second	69 1		133.3	A CONTRACTOR OF THE PARTY OF TH	A Second Co.	173.5			213.6	1 58.5
17		10.1	67	53 8	39.9	17		69.7	67	134.1	99.5	17	174 3	129.3			159.1
18		10.7	68		40.5	18	94.8	70.3		134.9	the same to	18	75.1	129.9		215.2	159.7
19		3 11.3	69	55.4	41.1	19		70.9	69	135.7	00.7	19	175.9	130.5		216.0	160.3
20	-	11.9	70	50.2	417	20	96.4	71.5	70	136.5	101,3	20	176.7	131.1	70	216.8	160.9
21	16.0	12.5	71	57.0	42.3	121	97.2	72,1	171	137.3	101.9	221	177.5	131.7	271	2176	161.4
22	17.5	13.1	72	57.8	43.9	22	98.0	72.7	72	138.1	102.5	22	178.3	132.3	72	218 4	162.0
123	18	13.7	73	58.6	43,5	23	98.8	73.3	73	138.9	103 1	23	179 1	132.9	73	229.2	1626
24		14.3	74	59 4	44.1	24	99.6	73.9	74	139.7	103.7	24	179.9	133.4	74	220.0	163.2
25		14.9	75	60,2	44.7	25	100.4	74.5	75	140.5	104.3	25	180.7	134.0	75	220,8	163,8
26	20.0	15.5	76	61.0		126	101.2	75.1	176	141.3	104.9	226	181.5	-	276	221.6	Marian Maria
27		16,1	and the second	61,8		27		75.7	77	142.1	105.4	27		135.2		222.4	164.4
28		16,7	77 78	62.6			102.8	76.3	78		106.0	28		135.8	77		165.0
					2 2 2 2 2	2	103.6	76.9	79		106.6	-1,77		136.4	Maria State of	223.2	165.6
29	1	17.3	79	63.4	10 10 10 10	1000	104.4		80		107.2	29	184.7	THE RESERVE TO A STATE OF THE PARTY OF THE P		224.C	166.2
30	-	17.9	80	64.2		3c		77.4		-	-	-		137.0	-	224.8	166.8
31	24.9	18.5	18	65.0	48.3	131	105.2	78.0	181		107.8	231	185.5	137 6		225.7	167.4
32		19.1	82	65,8		32	106,0	78.6	82	State Control of the	108.4	32		138.2		226,5	168.0
33	26.5	19.7	83	66 7	49.4	33	106.8	79.3	83		109.0	33	and the second	138.8	83	227.3	168,6
34		20,3	84	67.5	50.0	34	107.6	79.8	84		109.6	34		139.4		228.1	169.2
35	28.1	20.9	85	68.3	50.6	35	108.4	80.4	85	148.6	110.2	35	188.7	140.0	,85	228.9	169.8
36	28.0	21.4	86	69,1	51.2	136	109,2	81.0	186	149.4	110.8	236	189.5	140.6	286	229.7	170.4
37		22.0		69,9	51.8	37	110.0	81,6		1 50,2	111.4	37	190.3	141.2	87	230.5	171.0
38	30 5	22.6	88	70,7	52.4	28	110.8	82,2	88	151.0	112.0	38	191.1	141.8	88	231.3	171.6
39	31.3		89	71.5	53.0	39	111.6	82.8	89	151.8	112.6	39	191,9		80	232.1	172,2
40		23.8	90	72.3	53.6		112.4	83.4	90	152.6	113.2		192 7			232.9	172.8
40												40					
41	32.9		91	73.1	54.2	141	113.2	84.0	191	153.4	113.0	241	193.5			233.7	173.4
42	33.7			73,9	54.8	42	1140	84.6	92	154.2		42	194.3			234.5	174.0
43	34.5	25.0	93	74.7	55.4	43	114.8	85.2	93	155.0	115.0	43	195,1		93	235.3	174.6
44	35.3	20.2	94	75.5	50.0		1156	85.8	94	155.8	115.0	44		145.4	94	236.1	175.1
45 46	36.1	-	95	76.3	50.0		116.4	86.4	95	156,6		45	196,7			236.9	175.7
46	36.9		96	77.1	57.2	146	117.2	87.0	196		116.8	246	197.5	146.6	296	237.7	176.3
47	37.7		97	77.9		47	118.0	87.6	97	158,2	117.4	47	198.4	147.1	97	238.5	176.9
48	38.5	28.6	98	78.7	58,4	48	118.8	88.2	98	159.0	118.0	48	199.2	147.7	98	239.3	177,5
49	39.4			79.5			119.7	88.8	99	159.8	118.6	49	200 0			240.1	178.1
50	40.2	29.8		80.3		150	120.5	89.4		160.6	119.1	250		148.9		240.9	178.7
					-	=	Dep				==	=			==		=
Diff	Depl	Lat	Dit	Dep	Lat	Diftl	Dep	Lat	Dift!	Dep	Lat	Ditt	Dep 1	Lat 1	Ditt	Dep	Lat
w 1 10			A TOWN	5 3.4		1		v 23 12	100				A. 13 1		2 - 1 - 2	100	

for 43 Points

240

								3 2			,	
Dit Lat Dep		Dep Dift		ep Dift	Lat	Dep	Ditt	Lat	Dep	Diff	Lat	Dep
1 00.8 00.6	51 39.4	32,3 101		40 151			201	155 3	127.5	251	194.0	159.2
2 01.5 01.3	52 40.2	33.0 02		4.7 52	117.5		02		128.1	52		159.8
3 02 3 01.9	53 41.0	33.6 03	79.6 6	5·3 53 6.0 54	118,2		03	156.9	The second	53		160.4
4 03,1 02.5	54 41.7	34.2 04		6,6 55	119 0		C4	157,6		54	1 1 Y / C	161.1
	56 43 3				-	-	05		130.0	55	197 1	161.7
7 35.4 94 4	57 44.1	35.5 106	0	7.2 156	120 6	98.9	206	159.2 160.c		256		162.3
8 06 2 05.1	58 44.8	36.8 08		8.5 58		100 2	A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	160.7		57 58	199.4	163.0
9 37,0 05.7	59 45.6	37.4 09	84 2 6	9.1 59	10 10 10 10 10	100.8	09	161.5	132.5	59	200.1	164.2
10 37.7 06.3	60 45.4	38.0 10	-	9.8 60	1236	101.5	10	162.3	133.2	60	200.9	
11 08.5 07.0	61 47.1	38.7 111		0.4 161	124 4	102.1	211	163.1	133.8	261	2017	165.
12 39.3 07.6	62 47.9	39;3 12		1.0 62			12	1638			202.9	166.1
13 10.1 08.2	63 48.7 64 49 5	40,0 13		1.7 63		103.4	13	100	135.1	63	203,2	
14 10.8 08.9	65 50.2	40.6 14		2.3 64	127.5	104.6	14	165.4 166 1	135.7		104 0	
	66 51.0	41.9 116			128.3		15	-	-		204.8	
16 12,4 10.1	67 51 8	42.5 17		3.6 166		105.3	216	167.7	137,0		205.6	
18 13,9 11.4	68 52.6	43,1 18		4.8 68	129 8	106,5	18	168.5			207.1	
19 14 7 12,0	69 53 3	43,8 19	92.0 7	5.5 69	130.6	107.2	19	169.2	138.9	69	207.9	
20 15.5 12.7	70 54.1	44.4 20	92.7 7	6.1 70	131.4	107.8	20	170.0	139.5	70	208.6	
21 16.2 13,3	71 54.9	45.0 121	93.5 7	6.7 171	132,1	108.4	221	170.8	140.1	271	209.4	171.0
22 17.0 14 0	72 55.6.	45,7 22		7.4 72	1329	109.1	22	171.6	N 74 8 3	72	210.2	
23 17.8 14,6	73 56.4 74 57,2	46 3 23		8.0 73 8.6 74	133.7	109.7	23	172.3	Control of the Control of the Control	73	211.C	
24 18.5 15.2	75 58.0	47.6 25		8.6 74 9·3 75	134.5	110,3	24	173.1	142.0	74	211.7	
26 20.1 16.5	76 58.7	48,2 125		9.9 176	136.c		-	173.9		75		174,4
27 20.9 17.1	77 59.5			0.5 77	136.8		1000	174.6	143 3	276 77	213.3	
28 21.6 17.8	78 60.3				137.6	The state of the s		176.2	1-0		214.8	
29 22.4 18,4	79 61.1	50 1 29		1.8 79	138.3	113.5	1 4 12	177.0	1 1		215,6	
30 23.2 19.0	80 61.8	50.7 30		3.4 80	139.1				145.9	80	216.4	177.6
31 24.0 19.7	81 62.6	51.4 131	101.2 8	3.1 181	139.9				146.5	281	217.1	178.2
32 24.7 20.3	82 63.4				140.6			179 3	147.1		217.9	
33 25.5 20.9 34 26,3 21.6	84 64,9	52.6 33 53·3 34		4.3 83 5.0 84	141.4			180,1			218.7	
35 27.1 12,2	85 65.7	53.9 35		5.6 85	12 N. J. C. S. C.	117,3		181.6	149,0		219.5	180.1
36 17.8 22.8	0.6	54 5 136	-		143.7	_	_		149.7	-	221,0	
37 28.6 23 5	87 67.2	55.2 37	105.9 8	6.9 87	144.5	118.6			150.3		221.8	
38 29,4 24.1	00,000,0	55 8 38	106.6 8	7.5 88	145.3	119.2	38	183.9	150.9		222,6	
39 30.1 24.7	89 68,8			8.1 89 8.8 90	146.1	119.9	39	184.7	151.6	89	223.3	183.3
40 30.9 25.4	90 69.6	-			146.8	-	40	185.5	152.2	_	224.1	-
41 31.7 26,0	91 70.3	57.7 141 58.3 42		9.4 191		121.1	241	186.2	152.8	291	224.5	184 5
43 33.2 27.3	93 71.9			0.0 92	149,1		42 43	187.c 187,8	153.5	92	225.6	185.2
44 34.0 27.9				1 3 94	149.9		44	188.6	154.7	93	226.4	186.8
45 34 8 28.5					150.7		45	189.3	155.4	05	228.0	187.1
46 35.6 29.2	96 74.2	60.9 146		2.6 196	151.5		246	190 1	156.0	296	228.7	187.5
47 36 3 29.8	97 75.0	61.5 47	113.6 9	3.2 97	152.2	124.9	47	190.9	156.6	971	220.	1,00.3
48 37.1 30.4	98 75.7	62.1 48	114.4 9	3.9 98	153.0	125.6	48	191.6	157 3	98	230.3	189.0
49 37.9 31.1 50 38.6 31.7		62.8 49 63.4 150		4.5 99	153.8	126.8	49	192.4	157-9	90	231.1	189.6
	==								158.5	-	231.8	-
Diff Dep Lat	Dift Dep	Lat Dift	Dep L	at Diff	Dep	Lat	Dift	Dep	Lat	Dift	Dep	Lat
								£	,	D		

for 41 Points.

72 Difference of Latitude and Departure for 38 Points

D	it La	t I)en r	Di	. I .	(.T)	In	11	-		1					J 7			
1-						t De	P Di	-	1	Di	ft La	t De	Di	It Lat	1 Des	Di	ti La	ID	-
1035	1 30		0.7	5.1			2 10	1 74.	8 67.	8 15	1 111,		-	_	9 135.		_		P
in the second	2 01	-		52				2 75.	68.	5 5				140	6 135	0 25		The second second	5
		2 0:		53			5 0	3 75	3 69.			3 102		150	4 136.		1	1 3	
		0 3:	C 42 7 3 3 1	54				+ 77.			1114.	1 103.	4 64						
_	5 03	70	3.4	55	40.	7 36.	0	5 77.	3 70.		5 114.	8 104,	1 05	1 -			4 188	,2 170	.5
	6 24	4 04	.0	56	41.	5 37.6	101	_	-	- -	the second		_	-	9 137,6		188	9171	,2
	7 25.	2 04	1.7	57								6 104.		152.	6 138		189	.6 171	.0
1			4	58	43.0						1110.	3 105		1 23.					- 5
1	06	7/06		59				1 0				c 106,		1 31	139.7	1 - 58	191		
10	0 7,	4 05	.7	60	-1			1 0				8 106,8			140.	59	191	9 173	
1	08.	2 07	.4	61		-	-	-				5 107.4		155.6	141.	60	1.92		
1:	1-0			62	113	2 To 2 2 2 2 2 2								156.	141.7	261	193	-	-
13	1			63								8.801	12	157,0			1	-1	
14				64		1					The state of the state of	7 109.4	13		143 0	63		8 176	9
1	1 21			65	47.4				of the contract			5 101	14	158.4	143 7	64		6 177	0
-	-	- -			-	137	-		decides services	65	122,	2 110,8	15	159.3					
16	* 1 4.92			66	48.9		10 100		77.9	166	123	111.5	216	A Transmission State	145.0			-	-
17					49.6			86.7	78.6	67			1-	160.0	145.7	266	1		
18				68	50.4				79.2	68		112.8			146.4				
19			- 11		51.1	46.3				69		113.5	19	162.2				- 1 /	
20	14.	13	,4	70	51.9	47.0	20	88.0	80.6			114.1	20			1	199.	3 180	6
21				71	52.6	47.7	131	89.6	81.2		-	114.8	-	1630	-	70	200	181.	3
22	16.	3 14	,8	72	53 3	48,3						115.5	22 I	163 7	148,4	271	200.	7 182.	0
23	17.0		.4	73	54.1	49.0	23	1	82.6			116.2	22	164.4	149,1	72	201	5 182.	6
24	17.8	16	.1	74	54.8	149.7	24	91.9	The same of the same			116.8	23	165 2	149.7	73	202.	2 183.	3
25	18.	5 16	.8	75	55.6	50 4	25	92.6	83.9				24	165.9		74	203,0	184.	
26	19.	17.	5	76	56.3	-	-	-	-	-		117,5	25	166 7	151.1	75		184	
27	20.0			77	57.0	51.0	126	93.3	84.6	176		118.2	226	167.4	151.7	-	-	185.	_1
28	20.7	1	4	78	57,8	52 4	27	94.1	85.3	77		118.8	27		152.4	77		186.	
29	21.			79	58.5			94.8	85.9	112 127		1195	28	168.9	153 1			186.	
30	22.2			80	59.3	53.0	29	95.6		79	132.6		29	169.6	1538	79	206	187.	1
	120	-		_	-	53.7	30	96.3	87.3	80	133.3	120.9	30	170.4	154.4	80	207.4	188,	5
31	23.0		1.0		60.0	54 4	131	97.0	88.0	181	134.1	121 5	231	171 1	-	281			
32	23.7	1000			60.7	55.1	32	97.8	88.6	82	134.8	122.2	32	171.9		82	200.2	188.	7
33	24.4			83	61.5	55 7	33	98.5	89.3	83	135.6	122.9		172.6			200.0	189.	3
34	25.2		° .		62.2	56.4	34	99,3	90.0	84	136.3	123.5	100000	173.3		83	209.6	190,0	
35	25.9		-	_	63.0	57.1	35	100 C	90.6	85		124,2	35	174.1		85	210.4		
36	26,7			86	63.7	57.7	136	100.7	91.3	186	137.8	1249	-	-	-	-	211.1		+
31	27.4	24.	8	87	64,4	58.4	37	101.5	92.0	87	128.5	125.6		174.8		286	211.9	192.0)
38	28.2	25.	5	88	05.3	59.1	38	102.2	92.7	88	139.3	126.2	38	175.0	159.1	87	212.6	192.	,
39	28.9	26,	Acres de la Contraction de la	891	05.9	59.8	39	103.0	93.3	80	140.c	126.0		176.3	159.8	88	213.3	193.4	
40	29,6	26.	9 9	90	56.7	60,4	40	103.7	94.0	90	140.7	127.0	39	177.0	160.5	89	214.1	194.0	
41	30.4	27.	5	91	67.4	61.1	-	104 4		1000	_	-		177.8		90	2148	194.7	
42	31.1			92	68,2	51.8		105.2	94.7	191	141.5	128.2	241	178 5	161.8			195.4	
43	31.9	28.		93	68,9	62.4		105.9	95.3		142.2		42	179 3	162.5	92	216.	196.1	1
44	32.6	29.		14	59.6	62.1		106.7	96.0		143.0		4.31	100,0	102 21	93	217.0	196.7	
	33.3	30.		5	70.4	62.8		107.4	96.7		143.7		44	180.7	163.8	94	217.8	197.5	ı
45	34.1	30.	-				-		97.4	95	144.4		451	18 T. cl	164 6	95	218.5	198.1	1
47	34 8	31.	6	7	71.1	64.5	146	108.2	98.0	196	145.2	131.6	246	182.2	165.2	296	7.7.0	700	1
48	35.6	32.		8	71.9	6,0	47	108.9	98.7	97	145.9	132.3	47	103,0	105.81	290	219.3	198.7	
49	36.3	32,		8	72.6	66	48	109.6	99.4	98	146,7	132.9	48	183.7	66.	98	10.0	199.4	
50	37.0			9 7	73.3	66.5	49	110.4	0.001	991	147 41	133.6	49	184.4	67.2	99 2	10.7	200.1	-
		33.				67.1	150	111.1	100.7	200	148.2	134.3	50 1	85.2	67.0	300 2	11.5	200.8	
Dift	Dep	Lat	D	ift	Dep	Lat	Dift.	Dep	Lat	Dift			-					201.4	
			12.5				-	- opi	Jat	יווני	Deb	Lat	Dift	Dep	Lat	Diff	Dep	Lat	
													1			14, 115,			

for 44 Points.

D. Harance of	Latitude and	Donoster	C D .
Dilici ciice OI	Latitude and	Departure	Tor A Points
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milli	ual.	neh.	Dill	Lat	Deh	Dift	Lat	Dep	Dift	Lat	Бер-	Dift	Lat	Dep	ift	Lat	Dep.
1	00,7	00.7	51	36.1	36.1	101	71-4	71.4	151	106.8	106.8	201	142.1	142.1	251	177,5	177.5
2	01,4	01.4	52	36,8	36.8	02	72,1	72.1	52	107.5		02	1000	142,8	52	178.2	178.2
3	02.1	Q2.I	53	37.5	37,5	03	72.8	72.8	53	108.2	108.2	03	143.5	143.5	53		178.9
4	02.8	02.8	54	38.2	38,2	04	73.5	73.5	54	108.9	108.9	04	144.2	144,2	54	179.6	179.6
5	03,5	03 5	55	38.9	38,9	05	74.2	74.2	55	109.6	109.6	05	144.9	144,9	55	180,3	180.3
6	04.2	04,2	56	39.6	39,6	106	74.9	74,9	156	110.3	110.3	206	145.7	145.7	256	181,0	181.0
7	04,9	04.9	57	40.3	40.3	07	75 7	75,7	57	111.0		07	146.4	146.4	57	181,7	181.7
. 8	05,7	05.7	58	41.0	41,0	08	76.4	76,4	58	111.7	111.7	08	147,1	147.1	58		182,4
9	11.	06.4	59	41.7	41.7	09	77.1	77.1	59	112.4	112.4	09	147.8	147.8	59	183,1	183.1
10	-	07.1	60	42 4	43,4	10	77,8	77.8	60	113.1	113.1	10	148.5	148.5	60		183.8
11			61	43.1	43.1	111	78.5	78.5	161	113.8	113.8	211	149.2	149,2	261	184.5	184.5
12	08,5	08.5	62	43.8	43.8	12	79.2	79,2	62	114.5	114,5	12	149.9	149.9	62	185,3	185,3
13	1	09,2	63	44.5	44.5	13	79.9	79.9	63	115 3	115,3	13	150,6	150.6	63		186,0
14		09.9	64	45.3	+5,3	14	80.6	80,6	64	116.0		14	151.3	151.3	64	186.7	86.7
15	10.6	10,6	65		46.0	15	81.3	81.3	65	116.7	116.7	15	152.0	152.0	65	187.4	187.4
15	11.3	11.3		46,7	46.7	116	82.0	82.0	166	117.4	117.4	216	152,7	152.7	266	188,1	188.1
17	1.07	12.0		47.4	47.4	17	82.7	82.7	67	118.1		17	153,4	153,4	67	188,8	188,8
18		12.7		48,1	48.1	18	83,4	83.4	68	118.8		18		154.1	68	189,5	189.5
19		13.4	69	48.8	48.8	19	84.1	84.1	69	1195		19	154.8	154.8	69	190.2	190.2
20	-	14.1	70	49.5	49.5	20	84.8	84,8	70	120.2	120.2	20	155.6	1556	70	1909	190.9
21	14,8	14,8	71	50,2	50.2	121	.85.6	85.6	171	120,9	120.9	221	156,3	156,3	271	191,6	191,6
22		15.6	72	50.9	50.9	22	86.3	86.3	72	121.6	The second second	22	157.0	157.0	72	192.3	192.3
23		16.3	F. 7.	51.6	51.6	23:	87.0	\$7.0	73	122.3		23	157,7	157.7	73	193,0	193.0
24		17.0	74	52.3	5 .3	24	87.7	87.7	74	123.0		24	158,4	158.4	74	193.7	193.7
25	17.7		7.5	53.0	53.0	_	88,4	88,4	75	123.7	123,7	25	159,1	159.1	75	194.4	194.4
26	18.4		76	53.7	53,7	126	89.1	89.1	176	1244	124.4	226	159.8	159,8	276	195,2	195.2
27	19,1	19.1	77	54.4	54.4	27	89.8	89,8	77	125.2	125,2			160.5	77	1959	195.9
28		19.8	78	55.2	55.2	28	90,5	90,5	78	125,0		28	161.2	161.2	78	196,6	196.6
29		20.5	79 80	55,9	55.9	29	91.2	91,2	79	126.6		29	161.9	161.9	79	197,3	197.3
30	-	-		-	-	30		91,9	-	127.3	-	30	162.6	162.6	80	198,0	198.0
31	1	21.9	81	57.3	57.3	131	92.6	.92.6	181	128,0		231	163.3	163.3	281	198.7	198.7
32	4	22,6			58.0	32	93.3	93,3	82	128.7				164.0	82	199 4	199.4
33		23.3		59.4	59.4	33	94,0	94.0	83 84	129 4			164,7	164.7	83	1 1 2	200,1
34	1	24.7	85	60.1	60.1	34	94,7	94.7	85	130.8	130.1	34	165,5	165.5	84	200.8	200.8
1100006	-	-	86	-		-			-	-		35		166.2	85	201.5	201.5
36		25.5		60.8	60,8	136	96.2	96.2	186	131.5		236		166.9	286	202.2	202.2
38		26.2	88	61.5	62.3	37 38	96.9 97.6	96,9	87	132 2	132.2	37	167,6	107.6	87	202.9	202,9
39		37,6		62.9		39	98.3		80	122.6	132.9		168,3		00	203.6	
40		28.3	90		63.6	40	99.0		90		134.3		169.0	169,7	09	204.3	204.3
41		-	_	64.3	-	-				-	,	40		-		_	-
2		29.0	02	65.1	65.1	141	99.7	99.7	191	135.1	135.1	241		170.4	291	205.8	205.8
43		30.4	03	65,8	65.8	43		101.1			136.5	42	171,1	171 8	92		
44		31.1	94		66,5	44		101.8			137.2		172.5	172.5	93		207.2
45	31.8	31.8	95		67.2	45		102.5	95		137.9	44	173.2			208.6	208.6
46		32,5		67.9		146	-	103,2			138.6	-			-	-	-
47	33.2	33.2	97		68,6	47	103.0		97	139.3	130.3		174.6	173,9		209,3	210.0
48		33.9	98			48	104,6	104,6			140.0	47		175.4		210.7	210,7
		34.6	99	70.0	70.0	49	105 4	105.4	1 99	140,7	140.7	49	176,1	176.1	90	211.4	211.4
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2 24 3 25 4 26 5 28 7 29 8 30 9 31 10 32 11 33 12 34 13 35 14 36 15 37	26 25 27 26 28 27 29 28 30 29 31 30 32 31 33 32 34 33 35 34 36 35 37 36 38 37 39 38 40 39 11 40 12 11 13 12 14 13	27 28 29 30 31 32 33 34 35 37 38 39 40 11 12 13 14 15 16 17 18 18 19 20 21 22 22 24	27 28 29 30 31 32 33 34 35 36 37 38 39 40 11 12 13 14 15 16	28 29 30 31 33 34 35 36 37 38 39 40 11 12 13 14 15 16 16 17 16 16 16 16 16 16 16 16 16 16	29 3 1 3 2 3 3 3 4 3 5 3 6 3 7 8 3 9 4 1 1 2 1 3 1 4 1 5 1 6 1 7 1 8 1 9 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	30 31 32 33 34 35 36 37 38 39 41 11 11 11 11 11 11 11 11 11 11 11 11	33 34 35 36 37 3 39 4 1 1 2 1 3 4 1 5 6 1 7 8 1 9 2 2 1 2 2 2 3 2 4 2 5 2 6 2 7 2 8 9 3 0	32 33 34 35 36 37 38 39 41 11 12 13 14 15 16 17 18 19 20 21	34 35 36 37 38 39 41 11 12 13 14 15 16 17 18 19 20 21 22 23	34 35 36 37 38 39 40 11 12 13 14 15 16 17 18 19 20 21 22 23	11 12 13 14 15 16 17 18 19 20 21	35 36 37 38 39 41 11 12 13 14 15 16 17 18 19 20 12 21 22 23 24	37 38 39 40 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	38 39 40 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	38 39 40 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26	38 39 40 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 27 28 29 20 20 20 20 20 20 20 20 20 20	39 40 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33	14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33	17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 35 36 37 37 37 37 37 37 37 37 37 37	16 17 18 19 20 21 22 23 24 25 26 27 28 29 31 31 31 31 31 31 31 31 31 31 31 31 31

	Year		Year 1782.															
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30 27 29 28 28 26 27 29 30 29 29 31 30 30 30 30 30 30 30 30 30 30 30 30 30	3040 40111214161617181816									

A	A TABLE of Numbers, &c. Year 1787.								n-	-	to	ABL any of	the for	
Month Days	January February March April May July Auguft September October November								lovember	ecemper	Num-	Tim	es answ	ering
1 2 2 2 3 2 4 2 5 5 6 2 7 7 2 8 2 9 3 1 1 1 2 1 3 1 4 1 4 1 1 3 1 4 1 1 1 1 1 1 1 1	2 24 3 25 4 26 25 27 26 28 27 29	23 24 2 24 2 25 26 2 27 2 28 20 29 30 3 3 3 3 3 3	255 265 277 288 299 3° 3° 11 3° 22 3° 3° 3° 4° 4° 35° 5° 6° 37° 7° 38°	27 28 29 3° 31 32 33 34 35 36 37 38 39 4°	28 29 30 31 32 33 34 35 36 37 38 39	29 30 31 32 33 34 35 36 37 38	30 31 32 33 34 35 36 37 38 39	32 33 34 35 36 37 38 39 40 11	33 34 35 36 37 38 39 40 11 12 13 14 15 16	134 35 36 37 38 39 40 11 12 13 14 15 16 17	11 12 13 14 15 16 17 18 19 20 21 22 23 24 25	C I Z 3 4 4 5 6 7 8 8 9 10 11 12 12 12 12 12 12	48 36 24 12 00 48 36 24 12 00 48 36 24 12 00	> A fternoon
16 17 18 16 20 21 22 23 24 25 26 27 28 2	37 39 38 40 39 11 40 12 14 13 15 14 16 18	38 3 39 4 40 1 11 1 12 1 13 1 14 1 15 1 16 1 17 1 18 1 19 2 20 2 21 2	9 4° 0 1 1 1 1 2 2 1 3 3 1 4 4 1 5 5 1 6 6 1 7 7 1 8	12 13 14 15 16 17 10 17 10 12 22 24 22 24 24 25 26 26 27 27 27 27 27 27 27 27 27 27 27 27 27	14 15 16 17 18 19 20 21 22 23 24 25 26	14 15 16 17 18 19 40 21 22 23 24 25 26 27 28	16 17 18 19 20 21 22 23 24 25 26 27 28	17 18 19 20 21 22 23 24 25 26 27 28 29 30 31	18 19 20 21 22 23 24 25 26 27 28 30 31 32	20 21 22 23 24 25 26 27 28 29 30 31 32	26 27 28 29 30 31 32 33 34 35 36 37 38 39	0 — I — I — I — I — I — I — I — I — I —		After Midnight



The Use of the foregoing Tables of Numbers.

In these Tables, each Page is divided into two Parts, by a black Line drawn down the Middle; and each of the Parts are marked at the Top with the Year for which they shew the Numbers; and under that, the Lest-Hand Column of each Part is marked with the Days of the Month, and the other Columns with the Months of the Year: So that if you would know the Number for any Day, suppose, for Example, on the 26th of March, 1780.

First, Find the given Year 1780, at the Top of the Table, and then under the given Month, which is *March*, and right against the given Day of the Month (which in this Case is 30) you will find the Number 30, which is the Number for that Day; and if from the Number so sound you subtract 10, the Remainder will be 20, the Moon's Age for that Day.

The Use of the Table of the Times, answering to the foregoing Numbers.

In this Table the Left-hand Column is marked with the given Numbers from 11 to 40, and the Figures right against any of these Numbers, give the Time answering to it in Hours and Minutes.

EXAMPLE I.

I would know what Time answers to the Number 23?

Answer. 10 Hours 24 Minutes Afternoon, that is, at 24 Minutes past 10 at Night.

EXAMPLE II.

What Number and Time answers to the 30th of January, 1780.

First, By the Tables of Numbers, I find the Numbers to be 33, and against that Number, in the Table of Times, I find 6 Hours 24 Minutes after Midnight, that is, at 24 Minutes past Six in the Morning.

A TIDE-TABLE.

A	H	M		MH	1
At Army	01	03	At Cork, Calis, Cape Clear,		1
At Amsterdam and Armentie	03	00	and in the Creek	04/2	20
		30			
At Abermorick and Antwerk	06	00	At Concalo-	060	00
	V 200		Without the Caskets -	28/1	
•			Between the Caskets and		
В			Guernsey, before Cromer, at Se-		
At Beachy, Blacktail, and be-			ven Cliffs, and at Catness	000	20
fore the Race of Blanquet -		200			
Thwart of Beachy	00	45	berness	00/1	1
At Blackness, in Bluet, and at		וכד	At Cows, in the Foss of Caen,	9 4	+
			in Calice and Chamberness Roads	100	2
Without Bluet, and at Ber-			Before the Haven of Caen,	10/3	5
보이 보고 있다고 말이라. 이 나를 하나 있다면 하면 하는데 이렇게 되었다면 하는데 있다면 하는데 없다면 하는데 없다면 다른데 없다면 다른데 다른데 다른데 다른데 다른데 다른데 다른데 다른데 다른데	7. 4.	A 12.14 " 1	in the Chamber, between Cripple		
Bourdeaux River, the South		S	Sand, and the Croyle, and at		
Coast of Bretaigne, the Coast of	198 - 3 .		Calshot —————	.,,	
Riscay and at Rackness -	02	00	Charleston Bar		
At Brest, before the Base,	03		parterior 15ar.	7.	3
and the River of Bourdeaux			At Dogum Pier and before		
	1 18.	15	At Dover Pier, and before	1 1 1	
	03	45	나는 마음이 가는 것이 되었다. 그는 사람들이 살아보고 그렇게 되었다. 그는 그들은 그들은 사람들이 되었다. 그는 사람들이 되었다면 그 사람들이 되었다.	12)
In Breefound, Bloy, and Bal-		20	At Denbeigh, and at Bowns		1000
Before Bremen and at Black-		30		02	
				03	
ney, and in the Channel before		-		04	-
		00			0
At Bristol Key		45		18	
At Bridgewater	07	1		09	
Bullen Deep ———	10	30	[[[[[[[[[[[[[[[[[[[
			At Dover, Dieppe, and Deal	10	3
7 2 1 .					
In Condada		00	E		
	1000	45			
Without Calis, at Corpus			before the Eyder, and before		
Christi Point, and at Camfer-		30	[18] [18] [18] [18] [18] [18] [18] [18]	12	C
Between Calis and Dover,			At Edam ————	21	1
before Conquet, and at the			Before the Eastern and Wes-		Se 7 15
Manual Cana	100	00	town Towns and at Townsends	00	-
North Cape	103	00	tern Emes, and at Engoments —	091	-

F	H	M	Mark the second	H	M
On the Coast of Flanders -				01	30
At Flushing	00	45	Before Hartlepoole —	03	00
Before the Fen in the Chan-			At Huntcliff Foot ——————————————————————————————————	03	14
	101	30	At Humber—	05	16
Without Fountny -	- 32	15	Before Hamborough at Hull,		
Without the Banks of Flan-			at the Holmes, and before Hum		
		1	ber's Mouth	P. C. S. S.	00
At Flamborough and Bridling-	1		At Haerlem, Havre de Grace,		
n —————————	04	30	and Home Head -	09	00
At the Forn, in Foy, at Fal			At St. Helens and Harwich,		
outh —	05	15	and without the Banks of Har		
Between Foy & Falmouth, in			wich -	10	30
e Channel, and at Foulness -	06	45	wich ————————————————————————————————————	11	I
Before the Coast of Frieze-					
nd, and the Fly	27	30	I		
Without the Fly———	38	15	At Jutland Islands -	12	00
At Freize and Fair Ifle -	00	00	On the West Coast of Ireland	03	C
At the Frith and South Fore			In all the Havens on the S.	1	
nd —————	10	10	In all the Havens on the S. Coast of Ireland	05	IA
In Fair Isle Road, and at the					
orth Foreland -		15	Κ		
			Kentish Knock	12	00
G ·			At Kelliers ————		
In Gibraltar Road, Gravel-			[[전 : 12] [[[전 : 12] [[[[[[] : 12] [[[] : 12] [[[] : 12] [[] : 12] [[] : 12] [[[[[] : 12] [[] : 12] [[] : 12] [[[] : 12] [[] : 12] [[] : 12] [[[[] : 12] [[] : 12] [[] : 12] [[[] : 12] [[] : 12] [[[] : 12] [[] : 12] [[] : 12] [[] : 12] [[[] : 12] [[] : 12]	04	1
g, and before Cherburg		00	At Kilduyn ————	12.	ind
Before Goree, at Guernsey, &			At Kildive		
Gravesend -		30		1	1
At Groine, at Gascoign, and	1	ľ	~ L		
e Coast of Galicia		00	At Leith	12	00
Thwart of Guernsey		4.5	[[] [[[[[[[[[[[[[[[[[02	1
In the Chamber, and Gore		1.	-At London	03	
nd —————	- 11	15	C - 1 1 1		
Н		1	fore Lynn ————	05	
Before the Hever, before	e		At Lynn Half-tide, at Lun-		1
orn, and at Hampton Key -		00	dey —	06	0
.			At Lynn	06	A
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At the Lizard by the Land At Lambay At Lambay At Leystoff, and thwart of it without the Banks Oog At Orkney At Orfordness within the Oog At In Leystoff Road, and at Long Sand Head Orwell Wales At Orfordness without the Sands At Orfordness without the Sands At Orfordness without the Orwell Wales At Orfordness without the Sands At Orfordness without the Sands Orwell Wales At Orfordness without the Sands Orwell Wales At Orfordness without the Sands II Is At the Maes, and before St Matthew's Point On the Coast of Portugal Os At St. Maloes At Moonless, and at St. Maloes Between Monse-bole and Falmouth, and in Mitford-Haven Or 300 Before Margate II Is At the Race of Portland Or 300 At Queenborough II Is At Newport Half-tide II Is At Newport Half-		H	M	0	HIM
At Leystoff, and thwart of it without the Banks ————————————————————————————————————	At the Lizard by the Land	07	30	At Orkness	HM
At Leystoff, and thwart of it without the Banks ————————————————————————————————————	At Lambay ————	08	16	At Orkney	03 00
without the Banks— In Leyfoff Road, and at Long Sand Head————————————————————————————————————	At Leyftoff, and thwart of it		3	At Orfordness within the	03 4
In Leystoff Road, and at Long Sand Head M Within the Maes at Maldon Pefore the Maes, and before St At the Maes, and before St Matthew's Point In the Mouse-bole, at St. Matthew's, and within Mount's-bay In Milford, at Moonless, and at St. Maloes Between Mouse-bole and Falmouth, and in Mitford-Haven In St. Magnes Sound, and Magnes Castle At the Isle of Man Before Margate N At Newport Half-tide At the West End of the Nore Before Nantz River At Newcosstle Before St. Nicholas At the Needles, at the Isle of Wight All the Coast of Normandy and Poierdy At Rochester At Rocheste	without the Banks———	00	15	Banks, & between Orford and	45
M Within the Maes at Maldon Before the Maes, and before St Matthew's Point In the Mouse-bole, at St. Matthew's, and within Mount's-bay In Milford, at Moonless, and at St. Maloes Between Mouse-bole and Falmouth, and in Milford-Haven In St. Magnes Sound, and Magnes Castle At the Isle of Man Before Margate N At Newport Half-tide At Newport Half-tide At Newcastle Before St. Nickolas At the West End of the Nore At Newcastle Before St. Nickolas At the Needles, at the Isle of Wight All the Coast of Normandy and Picardy At Confordness without the Sands At Portsmouth Half-tide At the Pens, Porthus, and Poistu On the Coast of Portugal On the Sands On the Coast of Portugal On the Sands On the Coast of Portugal On the Sands On the Coast of Portug	In Levitoff Road, and at Long	1 9			
M Within the Maes at Maldon Refore the Maes, and before St At the Maes, and before St In the Mouse-bole, at St. Matthew's, and within Mount's-bay of In Milford, at Moonless, and at St. Maloes Between Mouse-bole and Falmouth, and in Mitford-Haven In St. Magnes Sound, and Magnes Castle At the Isle of Man Refore Margate N At Newport Half-tide At Newcastle Before Nantz River St. Nickolas At the Needles, at the Isle of Wight All the Coast of Normandy and Poicardy At the Swin In the Pens, Porthus, and Poicium On the Coast of Portugal On the Coast of Portu			20	At Orfordness without the	10 30
Within the Maes at Maldon Before the Maes, and before St At the Maes, and before St In the Mouse-bole, at St. Matthew's, and within Mount's-bay of In Milford, at Moonless, and at St. Maloes Between Mouse-bole and Falmouth, and in Mitford-Haven— In St. Magnes Sound, and Magnes Castle At the Isle of Man— Before Margate In the West End of the Nore of At Newport Half-tide— At Newport Half-tide— At Newport Half-tide— At Newcastle Before St. Nicholas— At the Needles, at the Isle of Might— At the Needles, at the Isle of Might— All the Coast of Normandy and Poisin Hood's Before Rochel In Ramsay— In the Pens, Porthus, and Oslow In Plymouth, and before St. In Plymouth, and before St. In Plymouth, and before St. Paul's— Oslow At the Race of Portland— Oslow At Rechester— At Rochester— At Rochester— At Rouen and before Rochel In Ramsay— Oslow At Rochester— Oslow At Rouen and before Rochel In Ramsay— Oslow At Rochester— Oslow At Ro		1	3	Sands ——————	T 1 1,
At the Maes, and before St Matthew's Point In the Mouse-bole, at St. Matthew's, and within Mount's-bay 04 In Milford, at Moonless, and at St. Maloes Between Mouse-bole and Falmouth, and in Mitford-Haven In St. Magnes Sound, and Magnes Castle At the Race of Portland At Rochester At Roches	M				1 15
At the Maes, and before St Matthew's Point In the Mouse-hole, at St. Mat. thew's, and within Mount's-bay of In Milford, at Moonless, and at St. Maloes Between Mouse-hole and Falmouth, and in Mitford-Haven of In St. Magnes Sound, and Magnes Castle At the Isle of Man of Harden At Newport Half-tide At the West End of the Nore of At Newcastle Before St. Nicholas At the Needles, at the Isle of At Newcastle At the Needles, at the Isle of Might At the Coast of Normandy and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin 12000	Within the Maes at Mal-			P	
At the Maes, and before St Matthew's Point In the Mouse-hole, at St. Mat. thew's, and within Mount's-bay of In Milford, at Moonless, and at St. Maloes Between Mouse-hole and Falmouth, and in Mitford-Haven of In St. Magnes Sound, and Magnes Castle At the Isle of Man of Harden At Newport Half-tide At the West End of the Nore of At Newcastle Before St. Nicholas At the Needles, at the Isle of At Newcastle At the Needles, at the Isle of Might At the Coast of Normandy and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin 12000			45	At Portsmouth Half-tide -	1115
At the Maes, and before St Matthew's Point In the Mouse-hole, at St. Mat. thew's, and within Mount's-bay of In Milford, at Moonless, and at St. Maloes Between Mouse-hole and Falmouth, and in Mitford-Haven of In St. Magnes Sound, and Magnes Castle At the life of Man Before Margate N At Newport Half-tide At the West End of the Nore At Newcastle Before St. Nicholas At the Needles, at the life of All the Coast of Normandy and Scilly, at the Shoe, at the head of Lower In Plymouth, and before St. In the Haven at St. Paul's Before Poddessemen At the Race of Portland Og At Queenborough It pole Head At Rochester At Rochester At Rochester At Rouen and before Rochel In Ramsay Og At Sueenborough In Ramsay Og At Rochester At Rouen and before Rochel In Ramsay Og At Sueenborough In Ramsay Og At Rochester At Rouen and before Rochel In Ramsay Og At Sueenborough In Rochester At Rouen and before Rochel In Ramsay Og At Rochester At Rouen and before Rochel In Ramsay Og At Rochester At Rouen and before Rochel In Ramsay Og At Rochester At Rouen and before Rochel In Ramsay Og At Rochester At Rouen and before Rochel In Ramsay Og At Rochester At Rouen and before Rochel In Ramsay Og At Rochester At Rouen and before Rochel In Ramsay Og At Rochester At Rochester At Rouen and before Rochel In Ramsay Og At Rochester At Rochester At Rouen and before Rochel In Ramsay Og At Rochester	Before the Maes	01	30		
Matthew's Point— In the Mouse-hole, at St. Matthew's, and within Mount's-bay O4 In Milford, at Moonless, and at St. Maloes— Between Mouse-hole and Falmouth, and in Mitford-Haven— In St. Magnes Sound, and Magnes Castle— At the life of Man— Before Margate— At Newport Half-tide— At the West End of the Nore O5 I5 Before Nantz River— At Newcastle— At Newcastle— At the Needles, at the life of Man— At the Needles, at the life of Man— At the Needles, at the life of Man— Before St. Paul's— In the Haven at St. Paul's— Before Poddessemeck— Thwart of Plymouth— At the Race of Portland— At the Race of Portland— At Rochester— At Ramkins— At Rotterdam, in Robin Hood's Bay, and from the Race to the At Rouen and before Rochel In Ramsay At the Needles, at the life of Might— All the Coast of Normandy and Picardy— Between the Naze and Warbead of Lower— In Plymouth, and before St. In the Haven at St. Paul's— O6 045 At the Race of Portland— O9 00 At Queenborough— At Rochester— At Rotterdam, in Robin Hood's Bay, and from the Race to the At Rouen and before Rochel In Ramsay O5 15 S In the Sleeve, between Ushant and Scilly, at the Sboe, at the Spitts, at Southampton, and along the Swin— In Plymouth, and before St. In Plymouth, and before St. In the Haven at St. Paul's— O6 045 At the Race of Portland— O9 00 At the Race of Portland— O9 00 At Rochester— At Rochester— At Rochester— At Rochester— O1 30 At the Swin—				Poittu-	03 00
In the Moufe-hole, at St. Mai- thew's, and within Mount's-bay 04 In Milford, at Moonless, and at St. Maloes Between Mouse-hole and Fal- mouth, and in Mitford-Haven In St. Magnes Sound, and Magnes Castle At the Isle of Man Before Margate In St. Newport Half-tide At Newcastle Before Nantz River At Newcastle Before St. Nicholas At the Needles, at the Isle of At the Needles, at the Isle of At the Needles, at the Isle of At Rochester October At Rouen and before Rochel In Ramsay October St. Modelos At Rochester October At Rochester At Rochester October At Rouen and before Rochel In Ramsay October St. Modelos At Rochester October At Rouen and before Rochel In Ramsay October St. Modelos At Rochester October At Rochester Octo			45	On the Coast of Portugal -	03 45
In Milford, at Moonless, and at St. Maloes Between Mouse-hole and Falmouth, and in Mitford-Haven— In St. Magnes Sound, and Magnes Castle— At the Isle of Man— Before Margate— At Newport Half-tide—— Before Nantz River— At Newcastle— At Newcastle— At Newcastle— Before St. Nicholas—— At the Needles, at the Isle of Might— At the Needles, at the Isle of Man— Between the Naze and War- Between the Spitts, at Southampton, and along the Swin— 1200		1 -		In Plymouth, and before St.	3 13
In Milford, at Moonless, and at St. Maloes Between Mouse-hole and Falmouth, and in Mitsord-Haven— In St. Magnes Sound, and Magnes Castle— At the Isle of Man— Before Margate— At Newport Half-tide— At Newcastle— Before Nantz River— Before St. Nicholas— At the Needles, at the Isle of Marmandy and Picardy— At the Naze and Warhead of Lower— Between the Naze and Warhead of Lower— In the Haven at St. Paul's— Before Poddessemeck— At the Race of Portland— Op O	thew's, and within Mount's-bay	04	30		
Between Moufe-hole and Falmouth, and in Mitford-Haven - O7 30 In St. Magnes Sound, and Magnes Castle - O8 15 At the lsse of Man - O9 00 Before Margate - O7 15 At Newport Half-tide - O8 15 Before Nantz River - O8 15 Before St. Nicholas - O6 45 At the Newcastle - O5 15 Before St. Nicholas - O6 45 At the Needles, at the Isse of Man - O5 15 At the Needles, at the Isse of Normandy and Picardy - O8 15 Between the Naze and Warhead of Lower - O8 15 Between the Race of Portland - O8 15 Between the Race of Portlan	In Milford, at Moonless, and			In the Haven at St. Paul's-	06 00
Between Moufe-hole and Falmouth, and in Mitford-Haven - O7 30 In St. Magnes Sound, and Magnes Castle - O8 15 At the lsse of Man - O9 00 Before Margate - O7 15 At Newport Half-tide - O8 15 Before Nantz River - O8 15 Before St. Nicholas - O6 45 At the Newcastle - O5 15 Before St. Nicholas - O6 45 At the Needles, at the Isse of Man - O5 15 At the Needles, at the Isse of Normandy and Picardy - O8 15 Between the Naze and Warhead of Lower - O8 15 Between the Race of Portland - O8 15 Between the Race of Portlan	at St. Maloes	05	15	Before Poddessemeck —	06 45
In St. Magnes Sound, and Magnes Castle	Between Mouse-hole and Fal-			Thwart of Plymouth -	07 30
Magnes Castle — 08 15 At the Isle of Man— 09 00 Before Margate — 11 15 At Newport Half-tide——12 00 At the West End of the Nore 045 Before Nantz River — 03 00 Before St. Nicholas— 06 45 At the Needles, at the Isle of Normandy and Picardy— 08 15 All the Coast of Normandy and Picardy— 10 30 Between the Naze and War-bead of Lower— 11 15 Spitts, at Southampton, and along the Swin— 12 00	mouth, and in Mitford-Haven -	07	30	At the Race of Portland—	09 00
Refore Margate — 11 15 Refore Margate — 12 00 At Newport Half-tide — 12 00 At Ramkins — 01 30 At Newcastle — 05 15 Before St. Nicholas — 06 At the Needles, at the Isle of Wight — 10 30 All the Coast of Normandy and Picardy — 10 30 Between the Naze and Warkead of Lower — 11 15 At Queenborough — 12 00 At Queenborough — 12 00 At Rockester — 00 45 At Rotterdam, in Robin Hood's Bay, and from the Race to the Pole Head — 03 00 At Rouen and before Rockel 15 S In the Sleeve, between Ushant and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin — 12 00	In St. Magnes Sound, and				
Refore Margate N At Newport Half-tide 12 00 At the West End of the Nore 00 45 Before Nantz River At Newcastle At Newcastle Before St. Nicholas At the Needles, at the Isle of At the Needles, at the Isle of All the Coast of Normandy and Picardy Between the Naze and War- kead of Lower 11 15 At Rochester At Ramkins At Rotterdam, in Robin Hood's At Rouen and before Rochel In Ramsay S In the Sleeve, between Ushant and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin 12 00 At Rochester At Ramkins At Rotterdam, in Robin Hood's At Rouen and before Rochel S In the Sleeve, between Ushant and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin 12 00	Magnes Castle -	08	15	Q	
Refore Margate N At Newport Half-tide 12 00 At the West End of the Nore 00 45 Before Nantz River At Newcastle At Newcastle Before St. Nicholas At the Needles, at the Isle of At the Needles, at the Isle of All the Coast of Normandy and Picardy Between the Naze and War- kead of Lower 11 15 At Rochester At Ramkins At Rotterdam, in Robin Hood's At Rouen and before Rochel In Ramsay S In the Sleeve, between Ushant and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin 12 00 At Rochester At Ramkins At Rotterdam, in Robin Hood's At Rouen and before Rochel S In the Sleeve, between Ushant and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin 12 00	At the Isle of Man-	09	00	At Queenborough ———	I 2 00
At Newport Half-tide————————————————————————————————————					
At Newport Half-tide————————————————————————————————————				R	
At the West End of the Nore of Before Nantz River — 03 00 Bay, and from the Race to the At Newcastle — 05 15 Bay, and from the Race to the Pole Head O3 00 At Rouen and before Rochel O3 45 At Rouen and before Rochel In Ramsay — 05 15 S In the Sleeve, between Ushant and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin—— 12 00	. N			At Rochester —	00/45
Before Nantz River — 03 00 Bay, and from the Race to the At Newcastle — 05 15 Pole Head — 03 00 At Rouen and before Rochel 03 45 At the Needles, at the Isle of All the Coast of Normandy and Picardy — 08 15 Between the Naze and War-head of Lower — 11 15 Spitts, at Southampton, and along the Swin — 12 00					01/30
At Newcastle Before St. Nicholas At the Needles, at the Isle of All the Coast of Normandy and Picardy Between the Naze and War- head of Lower 11 15 Pole Head At Rouen and before Rochel In Ramsay S In the Sleeve, between Ushant and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin 12 00					
Before St. Nicholas————————————————————————————————————					3
At the Needles, at the Isle of Wight All the Coast of Normandy and Picardy Between the Naze and War- head of Lower In Ramsay S In the Sleeve, between Ushant and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin————————————————————————————————————	At Newcastle	05	15	Pole Head ————	0300
At the Needles, at the Isle of Wight All the Coast of Normandy and Picardy Between the Naze and War- head of Lower In Ramsay S In the Sleeve, between Ushant and Scilly, at the Shoe, at the Spitts, at Southampton, and along the Swin————————————————————————————————————	Before St. Nicholas-	06	45	At Rouen and before Rochel	03 45
All the Coast of Normandy and Picardy ————————————————————————————————————	At the Needles, at the Isle of			In Ramsay —	05 15
Between the Naze and War- bead of Lower————————————————————————————————————			15		
Between the Naze and War- head of Lower————————————————————————————————————	All the Coast of Normandy	7		S	
head of Lower————————————————————————————————————			30	In the Sleeve, between Ushant	
the Swin	Between the Naze and War-			and Scilly, at the Shoe, at the	
the Swin	head of Lower—	11	15		
Upon		1	1		
				Upor	j

	H	M		H	M
Upon the Coast of Spain,			Without Usbant -	The second	
and in Shetland	03	00	St. Vallery -		
At Scilly, in the Sound, Scar-					3
burgh, and at Staples	03	45	W		
At Seven-Isles, without the			At Winchelsey ————	00	45
Haven in the Broad Sound -		30	At the Weilings, and from the		
At the Mouth of the Severn,			West-end of the Wight -		
between Scilly and the Tixard	1		Refore the Wailings	00	
at the Spurn and Stockton -	05	15	At Whithy —	03	10
Without Scilly, in the Chan-			In the Sea of Wales and		
nel, and at Salcomb	06	oc	Severn ————	04	30
At Sedmouth, and at the Start	06	45	In Wales-	05	15
Off the Start in the Channel	07	30	At Wales, at Weymouth, and	Ĭ	
			at Waterford		00
Shelburgh	09	00	At Weymouth Key	06	45
At Shoreham -	109	45	At the Ness, by Wieringhen		
			at Winterton		30
			Thwart of the Isle of Wight		
T Wishin Grand			in the Channel, all within the		
Within Tervere ———	CO	145	Wight, between the Wight and		
Before Tervere, before the			Beachy by the Shore	08	15
Thames, and at Tinmouth	01	30	At the E. end of the Wight,		
Before the Tees & Tinmouth,			and on Wieringhen-Flats-	09	00
before the Bay of Tinmouth — At the Clifts of the Taxell—	03	00	Wexford	6	0
The the Chies of the Texen—	104	130			
In Torbay, and before the			Y		
Texell—————	06	00		01	30
In the Road of the Texell —	07	30	At Youghall ————	04	30
At Torgen —	09	45	At Yarmouth ————		15
			In Yarmouth Roads, and Yar-		
U	- 3%		mouth Haven —————	10	30
Before Ureck —	12	00			
At Use —————		oc		1 2	
Between Ushant and the Main		45	Z		
In the Vourd, at the Bay				01	
within Ushant —	04	30		03	00
		•	M 2 The		

The Use of the TIDE-TABLE, in finding the Time of High-Water.

In this Table the Names of the Places being fet in alphabetical Order, they will always be found under the Letter they begin with, as for Example, London will be found under the Letter L; Torbay under T; Scilly under S, &c. and the Figures right against any Place, shews the Time of High water at that Place on the Full and Change of the Moon.

Then if it be required to find the Time of High-water at any Place upon any given Day, First, (by the Tables of Numbers and Times answering) find the Number and Times answering for that Day, (as before taught) and to that Time add the Hours and Minutes that stand in the Tide Table against the Place you would know the Time of Highwater at, the Sum, if it doth not exceed 12 Hours, will the Time of High-water required; but if it should be more than 12 Hours, then subtract 12 from it, and the Remainder will be the Time of Highwater.

EXAMPLE I.

Suppose it was required to find the Time of High-Water at London, on the 21st of May, 1781.

By the Tables of Numbers I find the Number for the 21st of May, to be 38, with which Number entering the Tables of Times, I find the Time answering to be 10 H. 24 M. then looking for London in the Tide Table, I find against it 3 Hours, which added to the Time before found, gives 13 Hours 24 Min. from which subtract 12, and the Remainder 1 H. 24 M. is the Time of High water at London on the 21st of May, 1781, in the Morning.

EXAMPLE II.

Suppose it was required to find the Time of High Water at St. Helen's, on the 25th of April, 1782.

Look in the Tables as before directed, and you will find the Number answering to be 22, and against Number 22 in the Table of Times, is 9 H. 36 M. I then look for *Helen's* in the Tide Table, against which I find 10 H. 30 M. which added to the Time above found, gives 20 H. 6 M from which subtract 12 H. and the Remainder 8 H. 6 M. is the Time of High Water next Morning, viz. on the 26th Day in the Morning.

A TABLE of the Sun's Declination for the Years 1780, 1784, 1788, and 1792.

M. Day		January		February		March		April		May		June		July		August		Sept.		October		Nov.		Dec.
3 4	23 22 22 22	5 ⁸ 5 3 4 7	17 16 16	11 54 36 18	7 6 6 6	32	4 5 5 5	49 12 35 58	15 15 15	18 36 53	12 22 22 22	10 18 25	23 23 22 22	7 2 58 52	17 17 17	55 39 24 7 51	8 7 7 6	5 43 21	3 4 4	27 50 13 37	14 15 15	41	21 22 22 22	58 7 15 23
7		2ć 18	15	42 23 5 45 26	4 4	23 59 36 12 49	7 7 7	6 28 51	17 17 17	1 17 33	21 22 23	56	22 22 22	34	16	43	5 5 5	6	5 6 6	46 9 32	16 16 16 17	32 45 6	22	38 44 50 56
1 2 1 1 4	2 I 2 I	5 2 43 33 22 11	13 13 13	6 47 27 6 46	3 2 2	38 14	8 9 9	40	18	19 34 48	23 23 23	20	2 I 2 I 2 I	56 47 38	14	8 5c 31 13 54	3 3 3	20 57 34 11 48	8	4° 2 25	17 18 18		23 23 23	11 15 18 21
18	20 20 20	0 49 37 24 12	12 11 11	25 4 43 22	0 0	3 40 16	11	44 5 2 5	19 19	30 43 56	23 23 23	26 28 28	21 20 20	9 58 47	13 12 12	35 16 56 37 17	2 I I	24 1 38 14 51	9 9 10	31 53 15	19	12 26 40	23 23 23	20 20 20 20 20
22	19 19	45	9 9	39 17 55 33 11	0	19	12 12 13	26	20 20 20	32 44 55	23 23 23	29 28 27	20 20	0 47	11 11 10	57 36 16 56 35	000	43	11 11 12	19 40 1	20 20 20	20	23 23	29 28 27
27	17	47 32 16 1 44 28	8 8 8 7	49 26 4 41	2 2 3 3 4 4	29 53 16 40 3	14 14 14	41	21 21 21 21 21 21	26 35	23 23 23	21 18 15 11	19 18 18	21 7 50 36 21	9 9 9 8	14 53 31 10 48 27	I 1 2 2 3	53 17 40 33	13 13	23 43	2 I 2 I 2 I 2 I 2 I 2 I	18 29 39 49	23	23 20 17 13 9

A TABLE of the Sun's Declination for the Years 1781, 1785, 1789, and 1793.

M. Day		January		February		March		Aprıl		May		June		July		Augult		sept.	-	October	12	Nov.	•	Dec.
1 2 3 4	22 22 22 22	uth 58 53 47 40 33	16 16 16	55 38 20 2	7 6 6 6	4 I 58	4 5 5 5	52 15 33 55	15 15 15	15 33 50 8	22 22 22 22	8 16 24 31	23 23 22 22	6 2 57 52	17 17 17	rth 55 40 24 8 52	8 7 7 6	7 45 23	3 4 4	24 45 13 34	14	38 57 16 35	21 22 22 22	50
7 8 9	22 22 22	20 18 10 1 53	15 14 14	6	5 4 4	25 2 39 15 5 ²	7 7 7	3 27 48	16 17	58 15 30	22222	49 55 0	22 22 22	34 27 20	16 16	35. 19 2 44 27	5 5 5	16 53 31 8 45	5 6 6	43 6 29	16 16 16 17	29 46 3	22 22 22	4
11 12 1: 14 15	2 I 2 I	43 33 23 12	13 13 12		3 2 2		8 9 9	54 18 37	18	17 31 46	23 23 23	12 16 19	2 I 2 I 2 I	56 47 38	14 14 14	51 29 14 54	3 3 3	22 59 36 13 50	7 8 8	37 0 26	17 17 18 18	55 9 25	23 23 23	1
17	20 20 20	49 37 25 12 59	1 I 1 I 1 I	45 24 3	0 0	6 42 19	11	41 2 22	19	27 41 58	23 23 23	25 26 27	21 20 20	9 58 47	13 12 12	36 17 58 38 18	2 1 1	17	9 9 10	28 50 12	19	11 24 38	23 23 23	2 2
22	10	22	0	-8	10	20	12	22	120	20	2.	.20	120	10	***	58 38 18 57 36	-		10 11 11 11		100		23 23 23 23 23	2 2 2 2 2
27 28 29 30	18		8 7	29 6 43	2 2 3 3 4 4	13 37	14 14 14	I	2 I 2 I 2 I	24 35 43	23 23 23 23	17 14	19	8 54 40 25	9	15 54 33 12 50 29	1 2 2 3	51 13 37	13 13 13	0 20 44	21 21 21 21	16 27 37 46	23 23 23	2 1 1 1

A TABLE of the Sun's Declination for the Years 1782 1786, 1790 and 1794.

M. Day	Ianuary	Junual	Dohman	reninaly	Morch	TATALLII	Anril	midu	May		1	June	Tult	() ()	4	Augun	Cont	oche	Ogober	October	Now	TAON.	المور	
1 2 3 4	22	55 4) 4 ²	17 16 16	0 43 25 8	7 7 6 6	28 5 42 19	4 5 5 5	39 2 25 48	15 15 15	10 28 45 3	22 22 22 22	6 14 22 29	23 23 22 22	8 4 59 54	17	rth c 45 29 13 57	8 7 7 7	13	3 4 4	17 40 4 27	14 14 15	33 52 11 20	21	55 2 11 19
7 8 9	22	21 13 4	15 14 14	53 34	5 4	46 12	7 7	56 19 41	17	53 10 26	22 22 22	48 53 59	22 22 22	36 29 22	16 16	41 24 7 50 32	6 5	37	5 5 6	36 59 22	16 16 16 16	24 41 58	22 22 22	34 41 47 53 59
11 12 13 14	2 I 2 I 2 I	36 26 16	13 13 12	55 35 15 54 34	3 2 2	12 48	8 9	47 9 31	18	12 27 42	23 23 23	12 15 18	2 I 2 I	59 53 41	14 14 14	57 38	3 3	29 26 6 43 20	7 7	53	18	48	23 23 23 23 23	16
17	20	41 29 16	11	52	0 0	13 50 26	10	34 55 16	19	37 50	23 23 23	25 26 27	21 20	12	13	42 23 4 44 24	1 1	57 34 11 47 24	9	44	19	34	23 23 23 23 23	26
22		36	10	4	I	45 9 32	12	37 57	20	38	23	28	20	16	11	4 44 24 3 43	0 0 0	37	11	3 I 5 2	2020	27	32	28 28 27
20 20 20 30	18 18 9 17	23	8 7	1	3 2	4:	13 13 14 14 14	56 - 14		3 40	23023	2	3 19 1 19 8 18 5 18 1 18	59	9	18	1 2	44 7 30	13	54	2 I 2 I 2 I		23	18 14 10

A TABLE of the Sun's Declination for the Years 1783 1787, 1791 and 1795.

M. Day		January	•	rebruary		March		April	3,4	May		June	1.4.	Juny	V	Augun	Const	och.	Opples	October	Mow	TAOA.		Dec.
3 4	23 22 22	55 49 43	17 16 16	3 46 28 10	7 7 6 6	31 8 45 22 59	4 4 5 5	36 59 22 48 8	15 15 15	7 25 43 0	22 22 22 22	5 13 20 28	23 23 22 22	8 4 59 54	18 17 17	47 31 16	8 7 7 7	rth 17 55 33 11 48	3 3 4	37 0 24	Sou 14 14 15 15	30 49 8 26	21 22 22 22	52 1 9
8	22 22 22	6	15 14 14	34 15 56 37 17	5	36 13 49 26 2	6 7 7	30 53 15 38 0	16 17 17	51 7 23	22 22 22	47 52 58	22 22 22	37 30 23	16 16	26 9 52	6 5 5	18	5 6	10 33 56 19 42	16	21 31 56	22	40
12 13 14	2 I 2 I	28	13 13 12	58 38 18 57 37	3 2 2	39 15 52 28 4	8 9	22 44 6 28 49	18	10 25 40	23 23 23	11 14 17	22 21 21	0 51 42	14 14 14	59 41 22	3 3	32 10 47 23 0	7 7 8	27 50 12		46	23 23 23	
17 18	20 20 20 20 20	55 43 31	11 11	55 34 13	0 0	41 17 53 30 6	10	31 52 13	19 19	22 35 48	23	25 26 27	2 I 2 I 2 O	13 3 52	13 13 12	26 6 47	2 1 1	14 51	9 9 10	19		3 18 32	23	2
21 22 23 24 25	19 19 19 19	F 2	110	. 8	0	N18 42 5 20 52	112	TA	120	25	22	28	20	18	111	17	0	17	1	-	20	12	22	2
28 29 30	18	55 40 25 9 53 20	7	39 16 54	2		13 14 14	52 10 30 49	2 I 2 I 2 I	19 29 39 48	23 23 23	19 16 12	19 19 18 18		999	4	1 2 2 2	40 3 27	12 12 13 13	51 11 31	2 I 2 I 2 I 2 I 2 I 2 I	0 10 22 32 42		2 2 1 1 1

A TABLE of the Variation of the Sun's Declination to every 10 Degrees of Longitude.

Degrees of Longitude from the Meridian of LONDON.

1	1	1_		1_	1		1	1_	1_	N	1	1	1	1	1	1	1	T
21 22 23 24	1 1 1			2 2 2 2 2 2 2 2 2 2 2 2 2	2 3 3 3 3 3	3 4 4 3 4	1 4 1 4 1 4	1 5	5 6 6	6 6 6 7	6 7 7 7	7 7 8 8	8 8 8 9	8 9 9 9	9 10 10		10	10 11 11 12
17 18 19 20	1 1 1	1	2	2 2 2	2 3	2 3 3 3 3 3 3 3	3 3 4 4 3 4	1 4	1 5	5 5	6	6 6 7	7	7 7 7 8	7 7 7 8	7 8 8 9	8 9 9 9	8 9 9 10
12 13 14 15 16	0 0 0		1	2 2	2 2 2	2 2 2 2 2 3	2 3	3 3 3	3 3 3	4 4	4 4 5	4 5	5 5	5 5 6 6	5 5 6 6 7	5 6 6 7 7	6 6 7 7 8	6 7 7 8
7 8 9 10	0 0 0	0	1 1 . 1	I	1	1 1 2	2	2 2 2	2 2 3	2 2 3	2 2 3 3 3	3 3 3 4	3 3 4 4	3 3 4 4	3 3 4 4 5	3 3 4 5 5	3 4 4 5 5	3 4 4 5 5
4 5 6	0 0	01.52	1 2 4 4	0	1 I	1	1 1 —	1 1 —	I 1	2	1 2 —	2 2 -	2 2 —	2 2	2 2 —	2 2 —	3	2 3 —
2 3	0 0 0	0	0	c	0	0	I	1	100	I I I	1 1 1	I I I	I I I	I I 2	I I 2	I I 2	I I 2	I I 2
Daily Vari. —— Min.	10 - M	20 M		40 M	50 — M		-	_	0	100 — M	— — M	120 — M	130 — M	140 — M	150 — M	160 — M	170 — M	180 — M

[90]

To find the Sun's Declination by the foregoing T A B L E S.

A CH Page of the foregoing Tables contains the Sun's Declination for the four Years that it is marked with at the Top, and is divided into thirteen Columns; the first of which to the Left-Hand, shews the Day of the Month, and the other Twelve the Months of the Year, so that if it be required to find the Sun's Declination for any Day, as suppose for Example, on the 21st of August, 1780: First, I look for that Table that has 1780, at the Top of it, and then right against the 21st Day of the Month, and under August, I find 11 57, which shews the Sun's Declination to be 11 Degrees 57 Minutes North; according to the Title at the Top of the Column.

The Sun's Declination in these Tables being calculated for the Meridian of London, if you should be considerably to the Eastward, or to the Westward of London, it will cause some Alteration in it; to correct which, the

Table of Variation of the Sun's Declination is to be used, as tollows:

First, Look out the Declination for the given Day of the Month, and for the Day following it, and subtract the less from the greater, the Remainder is the daily Variation.

Second, Observe whether the Declination be increasing or decreasing, which you may know thus; if the Declination for the Day following the given Day be biggest, then it is increasing; but if it be least, it is decreasing.

Third, Look for the daily Variation in the first Column of the Table, and see what Number stands right against it, and under the given Degrees of Longitude, which Number is to be used as follows.

If the Difference of Longitude be Easterly, and the Declination increasing, it must be subtracted from the Declination found in the Tables for the given Day; but if the Declination be decreasing, it must be added.

If the Difference of Longitude be Westerly, and the Declination increasing, it must be added; but if the Declination be decreasing, it must be subtracted; the Sum in one Case, and the Remainder in the other will be the Sun's Declination at Noon in the Longitude required.

4 45

A TABLE of the Sun's Right Ascension.

Month Day	Taunary		Pohmore	reninary	March	marcin	Line V	apa	May	faraj	June	aumí	Tulle	J7	AA	Augun		September	Oachen	October	November	100000	December	
1 2 3	8 5 18 5	54 8 8 9 3	2 I 2 I 2 I 2 I	10	22 22 22 23	51 54 58 02	00	51 55	02	39 43 47	04 04 04	42 46 50	06 06 06 06	46 50 55	08 08 08	59	10 10 10	50 54	12 12 12 12	31 35 38 42	14	28 31 35 39	16 16 16	M 32 36 40 45 49
7 8	19	16 20 25	2 I 2 I 2 I	26 130 34	23	13 16 20	10	10	03	58 02 06	05 05	03 07 11	07 07 ○7	07 11 15	09	10 14 18	11 11 11	05	12	53 57 00		51	16 17 17	53 58 02 07
1500		38 42 46	2 I 2 I 2 I	46 50 53	23 23	31 35 39	10	28 32	03 03. 03	18 22 26	05 05 05	23 27 32	07 07 07	27 31 36	09 09	29 33 37	1 1 1 1	23 26 30	13 13 13 13	11 15 19	15 15 15 15 15	12 16 20	17 17 17	15 20 24 29 33
17 18	19 19 20 20 20	59 04 08	22222	05	23 23 23	49 53 57	01	43 46 50	03 03 03	38 41 45	5 05 05	4 4 6 - 5 2	97 97 7	48 52 56	09 09 09	52	11	41 44 48	13	30	15	32 36	17	4
22 23 24	20 20 20 20 20	2 25 29	22222	24 28	00	11	02	01	04 04	547 01	6 06	C C C C C C C C C C C C C C C C C C C	8 08	12	10	10	11	55 02 c6	13	49 53 57	15	53 57 02	18 18 18	0.
26 26 30	20 20 20 20 20 20 20	45 45 54	22	4	000	30 30	02	26	04	2:	2 06 6 06 0 06	30	808	3	10	2 2	12	20	14	12	16	14	81	3. 3. 4

A TABLE of the Right Ascension, in Time, and Declination of some of the most noted Fixed Stars.

		ght	Decl	ina-
The Names of the Stars.	Alce	nsion	tio	n.
	H.	M.	D.	M.
The Bright Star of Aries —————	OI	53	22	22N
Medusa's Head, Algol	02	52	-39	59N
The Bright Side of Perseus	03	07	48	58N
The Bull's Fye, Aldebaran-	04	22	16	O'N
The Goat Star, Capella	04	59	45	44N
The Bright Foot of Orion, Regel -	05	03	08	285
The Northern Horn of the Bull -	05	11	28	21N
Orion's Right Shoulder — — — —	05	10	06	04N
The Southern Horn of the Bull -	05	21	20	5 N
Middle Star in Orion's Belt -	05	22	00	30S
Orion's Left Shoulder———————	5	52	07	20N
Auriga's Right Shoulder	05	44	44	54N
Bright Foot of Gemini —	06	20	16	38N
The Dog Star, Syrius-	06	34	16	235
Castor, or the Head of the Northern Twin -		20	32	24N
The Little Dog Star, Procyon	07	26	05	49N
Pollux, or the Head of the Southermost Twin -	- 07	28	28	34N
Hydra's Heart —	09	16	07	37S
The Lyon's Heart, Regulus -	- 09	53	12	56N
The Lower of the Pointers	- 10		57	411
The Upper of the Points	- 10		03	031
The Lyon's Tail, Deneb	- 11		15	551
Upper of the two last in the square of Great Bear-	- 12	35	58	351
The first in the Great Bear's Tail	- 12		57	181
The Virgin's Spike-	- 13		09	
The middle of the three in Great Bear's Tail	- 13		56	221
Last but one in the Tail of Hydra	- 13		21	435
Last in the Great Bear's Tail	- 13		50	311
Areturus ——————————	- 14		20	261
Bright Star in the Southern Balance ———	- 14		14	538
Foremost Guard—	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00		1
2 of timejs Guara	15	51	75	• 5

A TABLE of the Fixed Stars.

			Decl	ina-
The Names of the Stars.	Afce	nsion	tio	n.
	H.	M.	D.	M
Bright Star of the Crown —————	- 15	22	27	33N
Bright Star in the Serpent's Neck	15	31	07	18N
The Scorpion's Heart, Antares -		41	25	515
The Head of Hercules		03	14	40N
In the Head of Serpentarius ————		22	12	47N
Bright Star in the Dragon's Head-		50	51	32N
Lyra, or the Harn —	- 18	27	38	33N
Lyrae, or the Harp ————————————————————————————————————	- 19	17	27	29N
Bright Star in the Eagle —————	19	39	08	14N
The Swan's Tail ———————	- 19 - 20			19N
Pegasus's Mouth ————————————————————————————————————		33	44	
Fomelhaut—————————	- 21	27	08	39N
가는 마음을 하는 물 바다가 되는 사람들은 것이 되는 것이 되었다. 하는 게 되는 사람들은 사람들은 사람들은 사람들은 사람들은 사람들은 사람들은 사람들은	- 22	42	30	55S
Pegasus's Wing, Marchab	- 22	53	13	53
Pegasus's Leg, Scheat	7	52	26	43N
Cephus's Knee		20	76	071
The Head of Andromeda	- 23	54	27	34N
End of Pegasus's Wing, Algenib———	- 23	58	13	39N
Pole star	- 00	42	88	001
Girdle of Andromeda——————	- 00	53	34	051
	R	ight	Dec	lina-
A TABLE of the Right Ascensio	nAfc	enfior	ti	on.
and Declination of the Crosiers.		M.	100000	M.
The Westermost of the two middle Stars—	- 12	03	57	285
The Eastermost	- 12	33	58	26S
The Northermost or highest Star-	- 12	18	55	30S
The Southermost or lowest —	- 12	12	61	485

To work an Observation, or to find the Latitude of the Place by the Tables of the Sun or Stars Declination, and their Zenith Distance, &c.

Note, When He N you take an Observation of the Sun, by the common Sea Quadrant, the Degrees and Minutes that your Sight Vane stands at, being added to the Degrees that your Shade or Glass Vane stands at, will give the Zenith Distance (or Complement of the Meridian Altitude) with which, and the Declination found in the Tables, you may find the Latitude as follows:

First, Take Notice whether the Sun or Star be to the Northward or to the Southward of you at the Time of Observation; if to the Northward, call your Zenith Distance North; or if to the Southward, call it South.

Then,

Second, If the Zenith Distance and Declination are both North, or both South, subtract the less from the greater, the Remainder will be the Latitude you are in, of the same Name with the Declination, if that be greater than the Zenith Distance, otherwise of a contrary Name.

Exemple of. Being at Sea on the 24th of August, 1781, I observed at Noon, and had on my Quadrant 8 40 (and the Sun to the Northward of me) what Latitude am I in?

Zenith Distance 8 40 North Declination 10 57 North

Latitude by Observation ______ 2 17 North Example 2d. Being at Sea on the 25th of December, I took the Altitude of the Log Star Syrius, on the Meridian to the Southward of me, 25d. I would know the Latitude?

Note, In all Cases (except where the Object is observed on the Meridian below the Pole) if the Meridian Altitude be given instead of the Zenith Distance, (as it is in this Example) then subtract it from 90d. and the Remainder will be the Zenith Distance.

Latitude by Observation ______48 37 North

To

[95]

To work an Observation.

Case the 2d. If the Zenith Distance and Declination be one North and the other South, add them together, and their Sum will be the Latitude required, of the same Name with the Declination.

Example 1st. Being at Sea on the 3d of November, 1780, I observed at Noon, and had on my Quadrant 8 17, (and the Sun to the Northward of

me) I demand the Latitude?

Zenith Distance

Zenith Distance

Declination

15 19 South

Latitude by Observation

Example 2d. Being at Sea on the 21st of June 1782, I took the Altitude of the Bright Star in the Harp Lyra, (on the Meridian to the Southward of me) 51d. I demand the Latitude?

The foregoing Rules are for observing by the Sun or Stars, when they are at their greatest Altitude, or upon the Meridian above the Pole; but as in some Parts of the Earth, the Sun does not set for several Days, and some Stars never set; in that Case they may be observed upon the Meridian, twice in the 24 Hours, that is, once at their greatest Height (as before) and again, when they are at the lowest, or upon the Meridian below the Pole; to work which Observation, take the following Rule.

Add the Complement of the Declination to the Meridian Altitude, the

Sum is the Latitude of the same Name with the Declination.

Example. Being at Sea, I took the Altitude of the Pole Star on the Meridian below the Pole, 46 21. I demand the Latitude?

Meridian Altitude — 46 21
Complement Declination — 01 56 North
Latitude by Observation — 48 17 North
The

REMARKS by the Revisor.) The Author in the above Rules and Examples, takes the Sum of the Numbers found on his Quadrant, and works with it, as if true, to find the Latitude; but the Latitude so obtained will differ several Minutes from the true Latitude. For obtaining which, the Zenith Distance, as found by the Quadrant, must be corrected, as shewn in the MARINER'S COMPASS RECTIFIED.

The Use of the TABLES of the Sun's and Stars Right Ascension, in finding what Time any known Star will be upon the Meridian, on any given Day.

Rule, Look for the Right Ascension of the Sun and Star in the forego. ing Tables, and subtract the Sun's Right Ascension from the Stars; but if the Sun's Right Ascension be greatest, add 24 Hours to the Stars Right As. cension, and then subtract the Sun's from it, the Remainder will be the Time of the Star's coming to the Meridian after Noon.

Example 1st. What Time will the Lyon's Tail Deneb be upon the Meridian on the 14th of April?

35

Example 2d. What Time will the Bull's Eye be on the Meridian on the 26th of October?

October 26th, at 14h. 18m. from Noon, or at 18m. past two in the Morning, of the 17th.

To find what Star will come upon the Meridian, at any given Time.

Rule, Add the Time from Noon, to the Right Ascension of the Sun, the Sum will be the Right Ascension of the Star required to be known, with which enter the Table of the Star's Right Ascension, and find what Star's Right Ascension agrees with, or comes the nearest to it, which is the Star required.

Example ift. I would know what Star will be on the Meridian, about

Time from Noon -

Right Asc. of the req. Star, the nearest to which -09 06 is Hydra's Heart. Example 2d. I would know what Star will be on the Meridian, at 1 past

two in the Morning, on the 26th of June?

Rt. Asc. of req. Star, nearest to which in the Tables 20 37 is Swan's Tail.

A TABLE of the Latitudes and Longitudes of Places, accounting the Longitudes from the Meridian of LONDON.

Places Names.	Lat	itude.	Lo	ngit.	Places Names.	Lat	itude.	. Lo	ongit.
The Coast of England.	D.	M.	D.	М.		D.	M.	D.	M.
D Erwick	55	48	01	45 W	Aberdeen -	57	24N	01	40W
B Newcastle -	- 55	12	01	30W	Dundee -	-56	28N		40W
Stockton —	-54	33	OI.	25 W	Edinburgh —	- 55	58N	02	59W
Spurn—————Yarmouth ————	53	45	00	13E 38E	The Coaf				
London ———	51	32	00	00	Dublin —	1		1.6	-6
North Foreland-	-51	25	OI	24E	Wexford —	-153	12	06	56
Beachy Head-	-50	46	00	25E		12.11	13 Z	07	27 ×
Dunnose	- 50	38 Z	OI	23	Waterford ———	- 32	09 0	00	40 0
Portland —	50	30 07	02	44	Cork —	-51	49 5		30 7
Start ———	-50	07	03	47	Cape Clear —	- 51		1.	100
Lizard —	49			14	Limerić ———			09	3500
Land's End	150	57 of 57 of	06	00 €	Galway ———	1,0	07 =	09	40 2
St. Mary Scilly ——	140	57 2	06		OTTITIO TTOMA	100	20 6		15 6
Hartland Point —	149	66 e	04	• ° €	Londonderry -	- 55	00.	07	20.
Lundy Island ———		20	04	35 L 40 S	Bellfast ———	-154	39	06	30
Briftol———	12:	33	04	400	The Coast of Ho	lland	and F	land	erd -
St. David's Head		00	04	3500	The Coan of 110.	nana .	and I	land	C13.
Barfey Ifle	152	44	05	00 e.	Scaw -	-157	30	10	20
Barfey Isle ————————————————————————————————————	5-2	23	04	50	Helighland —		24	08	
Liverpool	153	20	03	00	Hambrough —		412		35 35 kg
Whitehaven —	100	17	03	30	Embden-	-53	0	07	35 =
Carlifle —	154	47	03	05	The Fly——		15 5	05	305
	7)4	+/	-5		The Texel		15 1	05	30 ng
The Coast of		otland			Amsterdam -		23 1	05	04 =
The Coan (1 50	otiand	•		Rotterdam -	-51	55 %	04	
C1 C	4				The Brill	- 52	and the same of the same	04	30 de
Glafgow -	57		04	05	Sluice-	-51		03	
N. Part of Sky Isle	57	45 N 20 T	05	45 eft	Calais-	-150	58	01	54
N. Part Lewis Isle	58	207	07	20 7		,	-		21:
St. Kilday ———	57	52		450	The Coast of Fr	ance a	and Po	ortug	ral.
Farra Head	-58	34 2	05	1000	0.000	D. 19451			
Isles of Orkney	59	10 =	03	22 7	Dieppe	- 49	56N	A	09E
Shetland S. Point —	-60	04 d		000	Cape de Hague-	-49	47N		ooW
Buchanness -	57	45 ?	01	18.	Galkets	-49	50N		20W
	1	Winds.			Guernfey -	-149	33N	02	47 W

A TABLE of Latitudes and Longitudes.

Places Names.	Lati	tude.	Lo	ngit.	Places Names.	Lat	itude.	Lo	ngit.
The Coast of France and Portugal	D.	M.	D.	М.		D.	М.	D.	M.
Morlaix —	48	33	03	49	Ancona —	43	40	14	26
	48	30	05	02	Venice	45	25	12	10
Brest		23	04	25	Lepanto-	38	10	22	52
	47	48	04	24	Cape Matapan —		33	22	41
Bellisse	47	20	03	16	Cape St. Angelo-		32	23	56
Nantz ———	47	14	01	39	Athens——	37	58	24	05
Island Dieu —	46	34 2		13 €		1		-4	٠,
Isle of Ree	46	107	01	30 et		38	07	25	03
Rochel ———			01		Cape Monte Sancto	10	26	25	0.7
Bourdeaux —	40		00	38 5	Galipoly —	40		25	02
		50 2	1	58g.	Configurationals	40	33	27	20
Bilboa ————————————————————————————————————		29 =		502.			59 Z	1	56
Cape Ortegal —		_	07	48 40 40 40 40 40 40 40 40 40 40 40 40 40	Smyrna ————		-	1	25
Cape Finister——	43	12.0	09		Ephefus —		01 5	1-1	53°
Oporto ———	41	10	09	25	Antiocheta —	1-	30 2	32	40
Burlings —	39	35	09	24	Scanderoon -	-30	34 🗒	30	30
Rocks of Lisbon —		54	09	50	Tripoli ————	-34	38 5		15
Cape St. Vincent —	36	53	09	06	Alexandria -	-31	100	30	19
Cadiz———		33	06	01	Cape Rusato		48	21	25
Cape Trefalgar—	-36	10	06	01	Cape Miserato —		21	16	17
					Tripoly —	- 32	54	13	10
AND STREET AND					Cape Bona -		03	11	04
On the Main Contin	ent	within	the	Straits	Bona —	-36	52	08	19
on the Main Contin		, Italia			Algier —	-36	50	03	16
Gibralter -	-136	12	04	53W	Cape de Tres Forca	s 35	30	02	04
Cape de Gat-		40	oi	40W	11 etuan —		27	05	06
Cape Paul	-38	15	00	05		-35	54	04	45
Cape Martin——		46	00	40	Tangier —		42	05	22
Barcelona -		26 7		18				-	
Marfeilles —	43	18 2	OF	27 H	Islands withi	n th	e Strai	te	
Toulon —	-43	07 3	-06	02 -	ll manus withi	II til	Colla	113.	
Genoa —		25 -	108	02 L 43 B	Alboran —	-125	F4	los	29
Leghorn —	144	25 Latitude. 54 de.	100	2500	Formentaria —	35	54 N 33 O 50 E	CI	29
	-43	201	173	33 =	Yvica———	-38	33 0	01	55
Dome-	41	54 5	- 74	35 gitude.	Majorca City—		30 =	01	40
	-40	510	14	40 0	Port Mahor	39	30 F	103	03
Naples ———			16	55	Port Mahon —	- 39	42 5	.04	12
Naples ————————————————————————————————————	37	55	1-0						
Naples ————————————————————————————————————	37	56	18	05	Gallita		41 5	08	44
Naples ————————————————————————————————————	37 -38 -39	56	18		S. End of Sardinia N. End of Corfica	-37 38 42	42 41 46 6 56	08	12

Places Names.	Lati	tude.	Longit.		Places Names.	Lati	tude.	Lo	ngit.	
flands within the Straits.	D.	M.	D.	М.		D.	M.	D.	М.	
orgona —	43	34	09	38	Affinee	04	15	02	17W	
	-43	03	14	54	Cape 3 Points —	04	28 Z		50W	
ilboa-	-42	45	II	00	River Volta	05	55 %	03	25	
lessina ———	-38	07	16		River Formosa —		00 =	07	20	
Iaritimo	-38	12	17	09	Cape Formosa —	-04	15 2	06	40	
ape Paffaro -	-36	38	15	40	New Callabar -	- 04	42 =	108	33 년	
Ialta	35	53 -	14	32	Old Callabar——	-04	10 5	109	45 =	
Corfu——	-39	42 0	20		River Camaroons		25 :	10	IOH	
Zephalonia -	-38	15 3	21	00 =	River Angra —	- 00	50	10	ongitude.	
ant -	-137	46	21	145	Cape Lopez -	-00	55 40 ES	09	55 =	
Aorea ———	-36		21	3200	River Congo -	- 05	40 5	15	25 5	
emnos —	-39	59 E	25	37 =	Angola -	-08	57 2	115	56.01	
cio	-38	22 6	26		Cape Negro -	-16	08	12	31	S41120
C.St. John, West- 1	-	•		•	Cape St. Thomas -	- 24	10	14	43	
end of Candia	35	15	24	00	Cape Bona Esperanc	e 34	07		35	Nond
Cape Solomon, E.	-		-	00						Long 2
End of Candia	35	00	27	08	The West	ern I	flands			1
City of Rhodes	_36	42	28	05						
West-end of Cypru		57	32	23	Corvo —	-120		170		DOM:
East-end of Cyprus	35	31	35	00	Flores -	39	54	2 30 30 2 30	55 West	
	1		1		Fial ———	- 39 - 38	34 5	1 30	54 c	
					Pico —	-38	33:	7 20		
The Coast of Bar	rhary	and (Zuin	917			40	27		
The Coan of Dai	Dary	anu (Julii	cy.	St. George-	- 38	52	26		
0			-		St. Michael		5/1	25	34 itude	1
Cape Spartel	-35		05	49	St. Maries	- 36				Jamis
Sallee	-33	51	100	25	ot. Maries	- 30	59	123	30	your .
Cape Cantin	-32		109	10	m 0					100
		27	10	06,	The Car	lary I	liland	S.		
Cape de Geer —	-120	04	5 15	35 €		-	- 6-14			
Cape de Geer — Cape Bajadore —		AI	115	50 €	Ferro	- 27		17	45	
Cape de Geer — Cape Bajadore — Cape Olerado —	- 23	4.			Palma ———	Charles Bridge .	40	Z 17	45 36 ≤	
Cape de Geer Cape Bajadore Cape Olerado Cape Blanco	- 23 - 20	22	-17	35 -				The second second		
Cape de Geer Cape Bajadore Cape Olerado Cape Blanco Senegal	- 23 - 20 - 15	32	17	35 L	Gomera-	- 28	06	2 17	95	
Cape de Geer — Cape Bajadore — Cape Olerado — Cape Blanco — Senegal — Cape de Verde —	- 23 - 20 - 15	32 28 43	16	25 Dong	Teneriff-	- 28	23	01 17 10 16	28 -	Tat .
Cape de Geer Cape Bajadore Cape Olerado Cape Blanco Senegal Cape de Verde River Gambia	- 23 - 20 - 15 - 14	28 43 08	17 16 17 17 15	25 97 1 10 20 31 1	Teneriff- Madeira West-end	- 28	23	5 16	28 -	Tat .
Cape de Geer Cape Bajadore Cape Olerado Cape Blanco Senegal Cape de Verde River Gambia Serralion	- 23 - 20 - 15 - 14 - 13	28 43 3 08 3 36	17 16 17 15 12 12	25 ongitud 20 31 ud	Teneriff- Madeira West-end	- 28 32	23 44 12	th Lati	28 26 9	Tat .
Cape de Geer Cape Bajadore Cape Olerado Cape Blanco Senegal Cape de Verde River Gambia Serralion Cape Monferado	23 20 15 14 13 08	28 43 3 08 3 36 6 05	atitude 15	25 golf 1 57 57	Teneriff- Madeira West-end	- 28 32 - 33	23 44 12	th Lati	28 0 26 9 54 9 5	Tal . 34.49
Cape de Geer Cape Bajadore Cape Olerado Cape Blanco Senegal Cape de Verde River Gambia Serralion	- 23 - 20 - 15 - 14 - 13 - 08 - 08	28 43 3 08 3 36 6 05 4 13	atitude. 12	25 pongitude: 57 co2	Madeira West-end Porto Sancto	- 28 32 - 33	23 44 12	5 16	28 26 9	Tal . 34.49

Places Names.	Lati	itude.	Lo	ngit.	Places Names.	Latitude.		Lo	ngit.
Cape de Verde Islands.	D.	М.	D.	м.		D.	M.	D.	M.
St. Vincent St. Lucia St. Nicholas Brava Fuego St. Jago Isle of May Isle Sal Bonavista The Sout	- 17 - 17 - 14 - 14 - 15 - 15 - 16 - 15	North Laritude. 508 1400 05	23 24 23 22 22 22 22 22	West Longitude. 20 0 % 0 4 5 0 % 0 7	Bengal————————————————————————————————————	20 22 16 02 14 10 14 23 24	43 42 17 North Latitude. 18 28 55 44 35 59 55	102 100 105 107	52 21 East Longitude 55 00 56 06 50 35
Afcention Afcention St. Hellena Fernandepo Princes St. Thomas Annabona	- 77 - 16 - 52 - 51	30S 40S 00S 40N 40N 00 10S	06 14 06 10 09 08	01W 25W 14W 30E 15E 20E 27E	Madagascar or \ S.e. St. Laurence \ N.e.	25	47 10	46 51	10
The Coast on the Ea	ift Ind	lies.			Mayetta Mohillo Comero St. Juan de Nova	11 16	10 05 40 Sout	42	38 23 50 A
Cape Lagulias — Cape Corientes — Mofambique — River de Fugos — Cape Baffos — Cape Guardafoy — Cape Rofulgat — Cape Muca — Buffera — Surrat — Goa — Callicot — Cape Camarine — Fort St. George — Dew Point	- 00 - 04 - 11 - 22 - 23 - 29 - 21 - 15 - 11 - 09 - 07	32 or th	72	East Longitude. 38 0 45 0 55 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	Mauritius Diego Roys Romiras de Caftelamas Amfterdam St. Brandon Diego Gratiofa Quebella Baffos de Chagos Yas de Diego Rays Maldivia St. End Malique Sacatra Abdeleur	28 38 16 08 03 06	10 Latitude 38 40 33 55 20 14 Latitude 25 0 21 40 0 40 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1	61 67 72 64 68 52 68 72 73 76	17 45 30 25 36 45 00 04 22 58 05 04

Places Names.	Latitude	Lo	ngit.	Places Names.	Lati	itude.	Lo	ngit.	
Islands in the East- Indies.	D. M.	D.	M.	The Coast of America, in the South Sea		м.	D.	M.	
C. Gallo in Zeloan Yas de Amber Andama Nicobar Sumatra N. W. end Verkins Island Bencola Sumatra S. end Engano Selam Princes Island Bantam in Java Batavia Java E. end Straits of Sundy Banca S. end Borneo S. point Bandy Isles Celebes Celebes S. end Mindano W. Point Borneo N. Point	06 07 20 00 00 00 00 00 00 00 00 00 00 00 00	81 52 93 93 94 99 104 105 101 105 106 113 127 119	15 30 32 40 50 07 32 08 10 43 13	Cape St. Sebastian— Cape St. Lucia— Cape St. Lucia— Cape Corientes— Aquapulco— Aquatulco— Guatimala— Panama— Bay Bonaventura— Isle Gallopega— Cape del Ajuga— Lima— Arica— La Serena— I. Juan Fernando— Baldivia— Port Steven— Cape Victory—	17 15 14 08 03 06 12 18 29 33 39 46 52 57	45 North Latitude. South Latitude. 38 1500 58 1500 58 com.	127 111 109 104 102 101 81 78 90 80 77 73 76 83 81 82 83 79	55 46 30 18 03 00 52 10 10 10 10 10 10 10 10 10 10 10 10 10	
Luconia SW. Point NE. Point E. Point E. Point N. Point N. Point N. Point N. Point Silfand Chufan SE. Point SW. Point	t 12 30 t 18 35 19 30 19 55 22 00 25 30 - 23 30 - 30 38	North Latitude 1120	0 10 05 00 00 00 00 00 00 00 00 00 00 00 00	River Julian ————————————————————————————————————	48 46 34 31 27 23 19 16	40 50 35 55 50 59 31	75 74 72 57 57 52 49 42 40 41 37	54 54 54 50 50 10 10 10 10 50	

Places Names.	Lati	tude.	Longit.		Places Names.	Latitude.		Longit.	
The Coast of Brazil, &c.	D.	M.	D.	M.		D.	м.	D.	М.
Cape St. Augustine	08	35S	35	zoW	St. Bartholomew—	17	52	62	06
Cape Roque	05	oos	35	47 W				62	10
Tristian de Cunha—	27		13	24W			17	62	13
Trinidada —	20	30S	1	woo			30 Z	1	25 €
1 Tillianan	120	300	130		St. Cruz		52 ort	62	
·		*** 0			Bieque —		00 =	62	300
Main Continent in	n the	West	-Ind	ies.	Porto Rico St. John's		20 -	6.5	
							30 1	65	37 9
R. Amazons Entrance	00	00	149	56	St. Domingo, Hisp.	1.0	25 1	109	3000
North Cape ——	02	05	49	56	Porto Royal Jamaica	17	40 de.	70	32 ude 55 e
Surinam	-06	25	56	50	East-end of Čuba —		15.		55 .0
Oronoque -	108	15 2		25 €	Havanna -		40	82	55
Cape Conquibaca -	12	40 9	70	42 E	Bay of Hondy -		45	83	40
Carthagena -		285	75	21	Cape St. Anthony-	21	45	85	32
Scots Settlement-	-08	30 5	. 1 3	45 8					
Nicaragua Entrance	1 . VA .	25 1	.81	1509					
Cape Catoche		25 11	86	10 =	Bahama	Illa	nds.		
Campechy	10	30.0	00	10 de.					
Campechy————————————————————————————————————	119	12	1						
Escondido ———	119	20	97	48	Bermudas	132	25	163	40
Cape Florida——	130		89	30	N. Point of Baha- 1	28	00	78	27
Cape Florida	-124	57	80	30	ma Bank —— J	120	00	10	35
					Bahama Island -	- 26	50	79	36
The Caril	be I	ilands	•		Abacco S. Point -	- 26		73	46
					Harbour Island -	- 25	. 37	76	47
Trinidado ———	110	15	160	17	Andros N. Point -	- 25	10	78	50
Tobago West-end-		10	59	10	Providence -				20 3
Granado -	-111	.57	60	20	Illathera S. Point -			75	56
Barbadoes -		38	58	50	Cat Island —		25 5	75	09
St. Vincent -		12		12 <	Watling Island -		03	74	25 9
St. Lucia -	-12	55 2	60		III T			171	35 50° 55
Martinico —	1:3	55 g 43 g	60	54 =	Evnma	- 22	45 22 2	75	200
Dominico —	1.4	43 =	60	345	Creeked Idand N.)	123	0	1/3	33
Marrigalante	1.3	231	60	30 5	Exuma ————————————————————————————————————	22	56	74	. 12
Marrigalante——— Guardalupe ———	1.5	58	100	2009	Point				
Montforet	10	10	60 61 62	15 tude.	Atkins Key	- 22	17	74	05
Montserat -	-110	45 8	02	150	Meraparvouz-	21	58	74	45
Antigua-		05	01	45	Atwood Key	- 23	10	73	35
Nevis-	-17	05	62	32	French Key -	- 22	40	73	40
St. Christophers-	-17	17	62	40	Mayaguana -	- 22		72	46
Barbuda	-17	56	60	40	Hogsties-	1	17	73	55

Places Names.	Lati	itude.	Lo	ngit.	Places Names.	Latitude.		Longit.	
Bahama Islands.	D.	M.	D.	М.	The Coast Hudson's Bay and Straits.	D.	М.	D.	M.
Heneago —	20	52N	73	46W	Buttons Isle -	60	25	66	27
Caices Bank North]	21	50N	.0 17	15W	Cape Charles	62	10	75	35
Point \	1.1.22	All and the second	1		Cape wainingham		35	77	55
Turks Island ———		35N		08W				80	30
Abrolho N. Point-		35N		06W	Cape Jones —	54		78	58
Plate Wreck —	-120	ION	68	15W	Rupers River-	51	.30 Z	79	26 €
	745				Albany River —		26 9		50 €
The Coast of Caroli	na,	Virgin	ia,	Mary-	The Cubbs —			82	40 [
land, Penfilvania,	, Ne	w-Eng	lan	d, and	C. Henrietta Maria			84	30 9
Newfoundland.					Port Nelfon ——		10 =	93	5809
					Cape Churchill——		55 tude:	.95	20 0
Charles Town up- 1			1		Cape Southampton	61	55.	82	48 6
on Ashley River	32	45	78	46	Shark Point		30	82	55
Cape Hatteras —	- 25	15	74	20	Nottingham Isle —		30	79	53
Cape Henry —	27	00	75	24	Queen Ann's Forel.		48	74	45
Cape Charles —	27	16	74	16	Refolution Isle		50	65	04
Cape Hinlopen —	- 28	50	74	56	Cape Farewell —	-59	45	146	45
Long Island ——		50	72	45					
New York ———	-40	58	1	53	The Coast of Icelan	d, C	Freenl	and,	Nova
Cape Cod -		12	73 68	55	Zembla, and				
Boston —		30 -	69	23					
Cape Sable -	- 43	500	64	58 €	Sound Royal-	-166	22	114	22
Cape Sable ————————————————————————————————————	-44	20 5	1 20 . 34	OI #	Bargazar Point —		20	16	33
Cape Britain -		00 -		305		-65	27	20	35 ₹
Quebec :	-46	55 2		4800			25	17	05 E
Bay of Brest -		10 2		F7 =	IIHalliford	16.			120
Bell Island -	-52	07 e	155	25 5	Fair Foreland -	-66	30 Z	26	2709
Cape St. John -	-50	15	52	48 .	Grims Island	-67	15 3	22	24 2
Cape Bonavista -	- 49	15	52	12	Westmania Isles-	-63	30 -		43 on gitude.
Trinity BayEntranc		42	52	20	Isles of Fero -		06	OF	00
Conception Bay -	-48	20	52	08	Beerenberg, or]			1 1	
St. John's Harbou	r 48	00	51	39	John Man's Isle	71	45	04	30E
Bay of Bulls -	-47	50	51	29	Point Look-out-	- 76	25	15	36E
Cape Race-	-46	40	51	52	Horn-Sound -	-76	45	13	36E
Cape St. Mary -	-47	10	53	23	Fair Foreland -	- 79	20	10	52E
Placentia -	-47	45	53	58	Hacluits Foreland-	79	55	11	OOE
Cape Roy	-48	00	157	40.	Helie's Sound	178	55	21	50E

In jurge Brok 14-4511 by 15 7 Block Soland -

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earl william

31.25 25.43 6.42 402 734

Places Names.	Latitude.		Longit.		Places Names.	Lati	itude.	Longit.	
The Coast of Iceland, Greenland, Nova- Zembla, and Nor- thern Islands.	D	м.	D,	М.		D,	М.	D.	М.
Lees Foreland Whale's Head Hope Island Cherry or Bear Isle— Admiralty Island— Fretum Borough— Cape Candinose— Catnose— Archangel Bar— Cross Island— Sweetnose— Kilduyn— North Cape— Surroy— Tromsound— Læfort S.W. Point Dronten— Stadland— North Bergen— Naze of Norway— The Coast in the Mardon— Larwick— Christiana— Maesterland——	77 76 74 75 70 69 65 64 66 68 69 71 70 68 63 62 60 57		35 40 36 34 31 23 16 15 09 10 04 05 07 Bal	East Longitude. 57 E E E E C C C C C C C C C C C C C C C	Gettenburgh Elfinore Copenhagen Valfterborn Kalmer Stockholm Wybourgh Peterfburgh Narva Revel Riga Derwinda Koningfberg Dantzick Wifby in Gotland Bornholm Straelfound Lubeck Anout Lefon Scaw	- 56 - 55 - 55 - 56 - 59 - 60 - 59 - 57 - 54 - 57 - 54 - 55 - 56 - 57	50 22 41 28 40 20 52 00 27 27 43 22 30 15 25 06 50 50 50 50 50 50 50 50 50 50 50 50 50	28	15 42 50 00 35 30 16 25 16 25 10 35 36 36 36 36 36 36 36 36 36 36 36 36 36

The Latitudes of any two Places being given, to find the Difference of Latitude between them.

Rule, If the Latitudes are both North, or both South, subtract the Less from the Greater, the Remainder will be the Difference of Latitude.

But

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an

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But if one Latitude be North, and the other together, and their Sum will be the Difference of I	South, then add the Latitude.	them
Example of. What is the Difference of Latitu	ide between the L	izard
and Barbadoes?	d. m.	
Lizard in Latitude—————		101
Barbadoes, in Latitude -	12 58 N.	631
The Difference of Latitude ————————————————————————————————————		
Cape Bona Esperance? Jamaica, in Latitude ————————————————————————————————————		63.
Cape Bona Esperance, in Latitude		76346
The Difference of Latitude————————————————————————————————————	그 선생님은 그리고 그는 그들은 이렇게 하는 사람이 많아 된 것이 없다면 하는데 되었다.	4.20
taken in, will give the Difference of Latitude in —	-2107 Miles	

Rules for Latitude.

The Latitude sail'd from, and the Difference of Latitude being given,

to find what Latitude the Ship is come into.

Case the 1st. When you sail from North Latitude to the Northward, or from South Latitude to the Southward, add the Difference of Latitude (it being first brought into Degrees, if need be, by dividing it by 60) to the Latitude sail'd from, the Sum will be the Latitude you are come into, of the same Name with the Latitude sail'd from.

Example 1st. A Ship from a Place in the Latitude 14 10 N. fails to the Northward, till she makes her Difference of Latitude 04 21. What

Latitude is she come into?

Example 2d. A Ship from the Latitude 29 17 S. fails to the Southward till she makes her Difference of Latitude 374 Miles: What Latitude is she tome into?

Latitude of the Ship ______35 31 S.

Case the 2d. When you sail from North Latitude to the Southward, or from South Latitude to the Northward, subtract the Difference of Latitude, if least, from the Latitude sailed from, the Remainder is the Latitude come into, of the same Name with the Latitude you sail'd from

But if the Difference of Latitude be biggest, then subtract the Latitude, from the Difference of Latitude, the Remainder will be the Latitude come into, of a contrary Name to the Latitude you sailed from.

Example 1st. A Ship from Latitude 49 14 N. fails to the Southward till her Difference of Latitude be 521 Miles. What Latitude is she come into?

Example 2d. A Ship from Latitude 4 18 S. fails to the Northward, till her Difference of Latitude be 10 24. What Latitude is she come into?

Rules for Longitude.

The Longitude of any two Places being given, to find the Difference of Longitude between them.

Rule. If the Longitudes are both East, or both West, subtract the lesser from the greater, the Remainder will be the Difference of Longitude.

But if one Longitude be East, and the other West, then add them together, and their Sum (if less than 180 Degrees) will be the Difference of Longitude; but if it be more than 180 Degrees, then subtract it from 360,00, and the Remainder will be the Difference of Longitude.

Example 1st. What is the Difference of Longitude between Cape Fini-

Calq

fro

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fre

36

CO

Wa

811

Longi-

[문항문화] 경영화 수업적으로 하다 중앙하는데 하셔요? 하는데, 그는 이는 아는 아들이 하는데 하면 하게 하고 있는데, 이를	
Cape Finistere, in Longitude-	r9 40 W.
Antigua, in Longitude	61 45 W.
The Difference of Longitude———	<u>52 05</u>
Example 2d. What is the Difference of Long and the Rock of Liston? Barcelona, in Longitude	02 18 E.
Rock of Liston, in Longitude-	
The Difference of Longitude	12 08
Example 3d. What is the Difference of Long Point of Japan, and the Island of St Christopher's S. E. Point of Japan, in Longitude————————————————————————————————————	——140 30 E.
Exceeds 180, Subtract it fro	
The Longitude sailed from, and the Difference given, to find what Longitude the Ship is come in Case 1st. When you sail from East Longit from West Longitude to the Westward, add tude to the Longitude sailed from, the Sum (if the Longitude come into, of the same Name with from. But if the Sum should be more than 180 Degree 360.00, and the Remainder will be the Longitude.	nto. ude to the Eastward, or the Difference of Longi- less than 180 Degrees) is h the Longitude you sail'd ees, then subtract it from
contrary Name to the Longitude you failed from. Example of A Ship from Longitude of 48 ward, till she makes her Difference of Longitude gitude is she come into?	East, sails to the East- 287 Miles. What Lon-
Longitude failed from	48 21 E.
Difference of Longitude 287 Miles, or -	
Longitude come into Example 2d. A Ship from the Longitude of Westward till her Difference of Longitude be 12	178 47 W. fails to the
the come into?	7:

P 3

Rules for Longitude.

Longitude failed from— Difference of Longitude		to the state of th
	Exceeds 180,00—191 Subtract it from—360	
Remains the Longitude	come into————————————————————————————————————	56 E.

Case the 2d. When you sail from East Longitude to the Westward, or from West Longitude to the Eastward, subtract the Difference of Longitude (if least) from the Longitude you sailed from, and the Remainder will be the Longitude come into, of the same Name with the Longitude sailed from.

But if the Difference of Longitude be the biggest, then subtract the Longitude from the Difference of Longitude, and the Remainder will be the Longitude come into, of a contrary Name to the Longitude sailed from.

Example the 1st. A ship from Longitude 98 17 E. sails to the W.ward, till she makes her Difference of Longitude 14 21: What Longitude is she come into?

Longitude sailed from	The state of the s
Longitude come into	56 E.

Example the 2d. A ship from Longitude 44 21 West, sails to the East-ward till her Difference of Longitude be 81 42: What Longitude is she come into?

그는 그 그는 그 그는 그는 그는 그는 그는 그는 그는 그는 그를 가장하는 것이 되었다. 그는 그는 그는 그는 그는 그는 그를 가는 그는 그를 가지 않는 것이 되었다. 그는 그를 가장 그를 다 살다.	
Longitude come into	37 21 E.

Here follows a Table of Meridional Parts, to every Degree and Minute of Latitude.

		-								-				and the state of the
VI	od	10	2 0	30	401	50	60	7 d	8 d	901	100	idl	124 11	3 d W
-	0	60	120	180	240	300	361	421	482	-			-	
0	1	61	121	181	241	301	362		483	542	603	664	725	787 6
1	A STATE OF THE STA	62	132	182			302	422		543	604	665	726	788 1
2	2	63	50 50 50 1	183	242	302	363	423	484	544	605	666	727	789 2
3	3		123	103	243	303	364	424	485	545	606	667	728	790 3
4	4	64	124	184	244	304	365	425	486	546	607	668	729	791 4
5	5	65	125	185	245	305	366	426	487	547	608	669	730	792 6
6	6	66	126	186	246	306	367	427	488	548	609	67c	731	793 6
7	7	67	127	187	247	307	368	428	489	549	.610	671	732	794 7
8	8	68	128	188	248	308	369	429	490	550	611	672	733	795 8
9	9	69	129	189	249	309	370	430	491	551	612	673	735	756 5
10	10	70	130	190	250	310	371	431	492	552	613	674	736	-
11	II	71	131	191	251	311	372	432	493	553	614	675		797 10
12	12	72	132	192	252	312	373				615		737	798 11
	13	73	133	193	253	313		433	494	554	616	670	73	799 12
13			134	194	254	314	374	434	495	555		677	739	8001
14	14	74					375	435	496	556	617	675	740	So1 1.
15	15	75	135	195	255	315	376	436	497	557	618	679	741	802 1
16	16	76	136	196	256	316	377	437	498	558	619	680	742	803 10
17	17	77	137	197	257	317	378	438	499	559	620	(81.	743	804 1
18	18	78	138	198	258	318	379	439	500	560	621	688	744	805 1
19	19	79	139	199	259	119	380	440	501	561	622	683	745	806 1
20	20	80	140	200	260	320	381	441	502	622	623	684	746	807.2
21	21	81	141	201	261	321	382	442	503	563	624	685	747	8082
22	22	82	142	202	262	322	383	443	504	564	625	686	748	
23	23	83	143	203	263	323	384	444	1	566	626	688		80,2
24	24	84	144	204	264	324	385	445		567		689	749	810 2
25	25	85	145	205	265	325	386	446		568	628			8112
26	26	86	146	206	266	326	387			569		1 - 7 -	751	8:22
			147	207	267	327	388	447		100000			752	813 2
27	27	87	148	208	268	328		448		570				8:42
28	28	88			269		389	449		571	631	693		816 2
29	29	89	149	209	209	329	390	450	511	572	633	(94	755	817 2
30	30	96	150	210	270	330	39 r	451	512	573	634	695	756	8183
31	31	91	151	211	271	332		452				196		8193
32		92	152	212	272	333		453	The second second					820 3
33	33	93	153	213	273	334		454						8213
34	34	94	154	214		335		455				699		8223
35	35	95	155	215	11/2 1 2 2 2	336					639			
		96						457				700		823 3
36				217		338	398	458	519		641	701		824 3
37	37	97		218		330		450	3.9	300	641	702		825 5
38	38	98		200	270			459	520	581	642	703		826 3
<u> 39</u>		99	159	219		340	400	460	-	-	-			827 3
40	40	100		220		341	401	461	522	583	644	705	766	828 4
41	41	101		221	281	342		462		584	649			829 4
42		102	162			343	403	463						830
43		103	163			344		464						8314
44		104	164	224	284	345		46						832
45	45	105								588	640			82.
46	46	106				347				589				83314
47	47	107	1			348								8.4
47		108				349			1 -					8:5
		109												830
49	49	-	-	-		350		-	-				-	837
50	50	110				351	411	471			654	715	776	83
51	51	111	171	231	291	352	412	472	533			716		839
52		112				353						717		840
53		113				354						718		841
54		1114				355						715		843
		1115				356						720		842
55		116								590				
56	56	117	Carried St.									State of the same of		844
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7	41	51	65	82	02	26	55	87	25	67	16	7¢	31	99	37
	42	53	67	84	04	28	57	90	27	70	1.8	73	34	99 59 ⁰²	38
	44	55	69	86	06	31	59	92	29	72	21	75	36	05	39
0		4257	4370	1488	1608	4733	1861	4994	-	5275	5423	5578	5739	:908	40
	48	59	72	90	10	35	63	96	5132 34	77	26	80	42	11	41
2	50	60	74	92	12	37	65	99	36	80	28	8:	45	14	42
3	52	62	76	94	14	39	65	1000	39	82	31	86	47	17	43
4	53	64	78	95	16	41	70	03	41	84	33	88	5c	19	44
5	55	66	80	97	18	43	72	05	43	87	36	91	53	22	45
6	57	68.	82	99	20	45	74	08	46	89	38	94	56	25	46
1	59	70	84	4501	23	47	76	10	48	92	41	96	58	28	47
13	61	72	86	03	25	50	79	12		94		99	61	31	48
	62	74	88	05	27	52	81	14	51	97	43	:602	64	31	49
9 4	164	275	4390	4507		4754	4883	5017		5299	5448		5767	5937	50
1	66	77	92	09	31	56	8.	19	5455	5301	51	0-	70	40	51
2	68	79	94	11	33	58	85	21	60	04	54	10	72	43	52
3	70	81	96	13	35	60	90	23	62	06	56	12	75	46	53
4	72	83	98	15	37	62	92	26	65	09	59	15	78	48	54
5	73	85	99	17	39	64	94	28	67	11	61	17	81	51	55
	75	87	1401	19	41	66	96	30	69	14	64	20	83	54	56
7	77	89	63	21	43	69	98	33	72	16	66	22	86	57	37
8	75	91	05	22	45	71	1901	35	74	19	69	2.5	89	57	58
		0	07	22	47	73	03	37	76		71	28	92	63	50

M	70 d	71 d	72 d	73 6	740	75 a	70 d	77 d	78 d	79 d	80 d	814	Szd	83d	10
0	5966	6146	6335	6534	6746	6970	7210	7467	7745	8046	8375	8739	1145	9606	1
1	69	49	38	38	49	74	14	72	49	51	81	45	53	14	1
2	72	52	41	41	53	78	18	76	54	56	87	52	60	22	1
3	75	55	45	45	57	82	22	81	59	61	93	58	67	31	1
4	78	58	48	49	60	86	27	, 85	64	67	98	65	74	39	1
5	81	61	51	52	64	90	31	90	69	72	8404	71	82	47	1
6	84	64	54	55	68	94	35	94	74	77	10	78	89		
7	86	67	58	.58	71	97	39	98	78	83	16	84	96	64	I
3	89	70	61	62	75	7001	43	7503	83	88	22	91	9203	72	1
9	92	73	64	65	79	05	47	07	88	93	27	97	11	80	
10	5995	6177	6367	6569	6782	7009	7252	7512	7793	8099	8433	8804	9218	9689	1
11	98	8c	71	72	86	13	56	16	98	3104	39	10	25		
12	6001	83	74	76	90	17	60	21	1803	09	45	17	33	9736	1
13	04	86	77	79	93.	21	64	2.5	08	15	51	23	40	14	1
14	07	89	80	83	97	25	68	30	13	20	57	30	48	23	1
15	10	92	84	86	6801	29	73	35	17	25	63	36	55	A CONTRACTOR OF THE PARTY OF TH	
16	13	95	87	90	04	33	77	39	22	31	69	43	62	40	-
17	16	98	90	93	80	37	81	44	27	36	74	49	70	48	1
31	19	ñ201	94	97	12	41	85	48	32	41	8c	56	77	57	
10	22	05	97	6600	15	45	89	51	37	47	86	63	85	65	-
-	6025	6208		6603	6819		_	-	7842	8152	8492	3869	-		1
20	28	11	6400			7048	7294	7557	47	58	98	76	9292	9774	
1.5	31	14	03	07	23	52 56	7302	66	52	63	8504	83	9300	The state of the s	1
22		17	07	the spirit	1000	65	06	100	57	68	1 10		07	The second second	1
23	34	20	17.17	14	30	64	11	71 76	62		16			9300	1
14	37	1.1	13	17	34	68			67	74	22	:023	22		1
25		23	17	21			15	1 . 10	72	79	28	09	30		1
26	43		20	24	41	72 76	19			85	1 7 7 7 7	1 - 7	37	100	1
27		30	23		45	80	23	89	82	90	34	100	45		1
3.5	49	33	27	31	49	84		94	87	, 96	40		53		1
29	52	36	30	35	53	-	32	-	-	201	46		60		1
30	6055	6239	6433	6639	6856	7088	7336	7603	7892	8207	8552	1936		9861	1
31	58	42	37	42	60	92	41	08	97	12	58		70	70	1
32	61	45	40	46	64	96	45		7902	18	65		83	79	
33	64	49	43	49	68	7100	49	17	07	23	71		91	88	1
34	67	52	47	53	71	04	53	22	12	29	77		99	197	1
35	75	55	50	56	75	08	58		1 17	34	83	70	9407	9906	
36	73	58		60	79	12				1		77	14	15	1
37	76	61	57	63	83	16	66		27		95 3601	84	22		1
38	79	64	60	67	86	20	71		32	51	And the second second		30	33	
39	82	68	63	70	90	24	75	35	1 37	56	07		38	42	1
19	6085	6271	63 6467	6674	6894	7128	7279		7942	8262	8614	9005	9445	1200	1
41	88	74	70	77	98		7379	54	48	67	20	12	53	9951 60 69 78	4
42	91	77	73	81	6901	32 36	88	59	53	71	26	18	61	69	14
43	94	80	77	85	05	40	92		58	79	32	25	69	78	ŀ
44	97	83	80	88	09	45	97		63	84	38	32	77	87	1.
45	5100	87	83	92	13	49	7401	73	68	90	44		85	9996	1
46	03	90	87	95	17	53	06	78	73	95	51	46	93	10005	1
47	06	93	90	99	20	57	10	83	78	8301	57	53	9501	10015	4
47	09	96	94	6702	24	61	14	87	81	07	62	60	09	10024	4
40	12	99	97	06	28	65	19		89	12	69	67	17	10033	
-	6115	-	6500	6710	6932	65 7169 73	7423		7994	8318	8676	9974	0525		
50	18	6303	6500	13	36	7.09	27	77.02	99	24	8676	9074	9525	10043	-
51 52	21	09			40	73			8004	29	88	88	33	10052	
		12	07	17		77 81	32		09		95	96	41	10071	
53	24			20	43	85	41		14		8701	9103	49	10071	
54		15	14	24	47	89		The state was a	20			10	57	10089	
55		19	17		51		45			100	07	The second second	05	10000	
56	33	22	21	31	55	94	49		25		14	17	73	10099	
57	36	25	24	35	59	98	54		30		26		0.	10108	
58	40	The same of the same of		38	66	7202	58 63	35	35				09	10110	5
-	. 41	1 22	1 31	42	. 00	. 00	1 03	10	40	1 09	33	1 30	1 90	1.01.	

M	84 d]	85 d)	86 d	87 d	88 d	89 d [M
10	10137	10765	11533	12522	13916	6300	0
1	147	776	547	541	945	357	1
2	157	788	561	561	974	416	2
3	166	799	5-6	580	14003	476	3
4	175	811	605	599	033	537	4
5	185	834	620	639	093	599 662	5
10.00	205	846	634	659	123	726	7
8	214	858	649	6-9	154	7.2	8
9	224	869	664	6:5	184	858	2
10	10234	10881	11679	12719	14216	16926	10
11	24+	893	694	735	247	956	11
12	25.	905	70,	759	279	17067	12
13	264	917	724	780	311	135	13
14	273	929 941	735 755	801	343 376	213	14
15	293	953	770	842	408		16
17	303	965	785	86;	442	445	17
18	314	978	801	824	475	\$26	18
19	324	950	816	506	100		19
20	10334	11002	11832	12927	14543	17693	20
2 1	344	014	848	949	578	781	21
12	354	017	863	970	613	8.0	22
23	364	C39	879	992	648		23
24	374	052	911	13014			25
25	385	077	927	059			26
27	405	089	543	081	791		1:7
28		102	959	104	830	461	28
29		115	76	126	868	570	29
30	16437	11127	11952	1314	14906	18682	30
31	447	140	12008	172			31
32	457	153	C25	195			32
33		1: 6	041	235			33
34		192	058	247			
35			092		and the same of		
137	510		109	314	182	596	37
38	521	31	126	338	220	749	138
39	532	244		362	26	8 60:	19
40	10512	11257	12100	13385	1531	1 20076	10
41	553	270	179	41	1 55	253	
42				43	6 35	8 439	12
4:	575		217		44	7 843	43
44				51	53	2 2106	+!
4	508			53	57	9 30	140
4	619	351	28	2 56	- 62	5 55	7
45	630	36	30	58	0.	3 83	2 48
49	64	37	31				
50	1065	1139	1233	6 1364	1 1577	0 2145	9 15
5	00	3 400	6 35	4 66		9 2282	9 5 5 6 5 5 5 5
5	67				5 86	0 2322	5 5
5		6 44	4 39				5
5	70	8 46		8 77			2 5
5	5 71	9 47	6 44	7 80	07	8 2560	9 5
15	7 73	c 49	0 46	5 83	2 13	2 2659	8 5
5	8 74	2 50.	4 48	4 8c	0 18		2 5
15	9 75	31 51	2 50	3 88	18 24	1 3019	5 5
-							

The Use of the Table of Meridional Parts.

In this Table the first and last Column of every Page marked M, begining at 0, and ending at 59, contain the Min. answering to every Degree or Latitude, the other Column marked 1d, 2d, &c. contain the Meridional Parts, answering to the Degree of Latitude they stand under.

So that if you would find the Meridional Parts, answering to any Latitude, suppose for Example, the Latitude 51.32, look in the Column under 51d. and right against 32, (in the Column for Minutes) you will find 20, to which prefix 36, the two Figures in the same Column that stand above 20 towards the Lest-Hand, and it makes 3620, the Meridional Parts required.

Two Latitudes being given to find the Meridional Difference of Latitude.

Case 1st. If both Latitudes be North, or both South, subtract the Meridional Parts of the Less from the Meridional Parts of the Greater, the Remainder will be the Meridional Difference of Latitude.

Case 2d. If one Latitude be North and the other South, then add their Meridional Parts together, and the Sum will be the Meridional Difference of Latitude. Q 2

A TABLE of Amplitudes, from the Latitude oo Deg. oo Min. to the Latitude 12 Degrees either North or South.

Degr Decl								Th	ie .	De	gre	ees	of	L	ati	tu	de.							
Degrees of Declination.				2		3		4		5		6		7		8		9		10		11		12
	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	N
1	01	00	01	OC	10	oc	00 01 02	00	10	00)I	00	01	cc	10	00	01	CO	01	01	10	01	01	0
3	03	co	03	oc	3	co	03	co	03	00	03	01	03	01	03	02	03	02	03	03	03	0;	3	(
6	06	00	06	00	06	00	05 06 07	01	:6	01	06	01	06	02	06	03	06	04	06	06	୍6	07	06	(
8	08	00	08	00	08	Ci	08	01	08	02	08	02	8	03	08	04	08	06	28	08	08	09	08	
IJ	11	00	11	00	11	01	10	01	11	03	11	03	II	05	11	06	11	08	11	11	11	12	11	
13	13	00	13	00	13	01	13	02	13	05	13	04	13	06	13	08	13	10	13	13	13	15	13	
16	16	00	16	01	15	01	15 16	02	16	04	16	05	16	C7	16	09	16	12	16	16	16	18	16	
18	18	00	. 8	01	18	01	18	02	18	04	18	06	18	08	18	11	18	14	18	18	18	21	18	
21	2 1	00	21	01	2 I	02	20 21 22	03	21	05	2 I	07	21	10	21	13	21	17	21	21	21	25	21	
	23	CC	23	01	23	02	23	03	23	05	23	80	23	11	23	14	23	18	23	23	23	28	23	

ATABLE of Amplitudes, from the Latitude 13 Deg. 00 Min. to the Latitude 24 Degrees either North or South.

)egre													1		1	itu	<u> </u>							
Degrees of		13	1	14	. 1	15		6		17		18		19		20		21		22	1	23	2	24
	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	M	D	M
																00								
3	02	03	02	03	02	04	02	05 07	32	08	02	06	02	07	02	08 02 15	02	08	02	09	02	10	02	17
6	05 06 07	10	06	09	06	13	06	15	26	16	06	19	06	21	06	19 23 27	06	26	05 06 07	28	05 06 07	31	05 06 07	3
	08	12	08	15	08	17	28	19	28	22	08	25	08	28	03	31	98	34	08	38	28	42	08	4:5
11 12 13	11 12 13	19	11 12 13	22 24	11 12 13	23 25 28	11 12 13	27 29 32	11 12 13	30 33 36	11 12 13	34 38 41	11 12 13	38 42 47	11 12 13	38 43 47 52 55	1 1 2 1 3	48 52 58	11 12 14	52 57 04	11 13 14	58 03 10	12 13 14	570
16 17 18	15 16 17 18	26 28 30	15 16 17 18	3° 32 34	16 17 18	35 37 40	16 17 18	40 42 45	16 17 18	45 48 51	17	51 54 57	18	57	17	00 03 07 11 16	17 18	15	17 18	18 23 28	17 18 19	25 31 33	17 18	2: 3: 4: 4: 5:
21 22 23	21 22 23	35	21 22 23	41 43 45	2 I 2 2 2 3	46 49 51	21 22 23	53 56 59	23 24	00	22 23 24	08	22 23 24	16 20 24	22 23 24	20 25 29 34	22 23 24	34 36 44	22 23 24	44 50 55	22 24 25	55 01 07	23 24 25	12

A TABLE of Amplitudes, from the Latitude 25 Deg. 00 Min. to the Latitude 36 Degrees either North or South.

Degr	,							1	Cho	e I)eg	gre	es	of	La	atit	ud	e.							
Degrees of	2	2	5	2	6	2	27	2	8	2	9	3	30	3	31	3	2	3	33		34		35	1	36
		D!	и	D	M	D	M	D	M	D	М	D	М	D	М	D	M	D	N	D	M	D	M	D	
	1	10	of)1	07	11	07	01	08	10	08	10	cg	21	00	21	10	10	11	01	12	01	13	01	
	3	2;	18	03	2	03	22	03	24	23	25	03	28	23	30 40	03	33	03	35	23	37	3	40	03	7
	5 6	06	37	06	41	6	44	06	48	06	52	06	56	27	5° 0° 10	07	C4	27	00	07	15	27	20	27	
	1	08	50	8	54	28	59	9	01	09	09	39	15	29	31	09	2	29	33	09	36	29	47	09	
	11	13	16	13	15 23 31	13	22 25 38	13	29 37 46	13	3¢ 4; 54	13	43	14	41 52 02 13	13	00 11 23	13	21	13	1 ¹ 31 44	13	21 42 56	14	1
	15	16	>5	16	44	16	53	17	03	17	12	17	23	17	34	17	46	17	58	18	11	18	45	18	3
7	17	18	49	18	59	19	05	19	20	19	31	19	43	19	45 56 08 14	20	10	20	37	20	39	20	54	21	!
	20	22	10	22 23 24	30	222 23 24	34 43 51	22 23 25	48 57 06	23 24 25	01	23 24 25	16	23	31 43 55	23 25 26	47	24 25 26	18	24 25 26	36	24 25 27	4c 56	25 26 27	
23	22	25	32	2 25	46	5 26	00	26	16	26	32	2 26	49	127	0;	27	26	27	46	28	07	128	21	28	3

A TABLE of Amplitudes, from the Latitude 37 Deg. 00 Min. to the Latitude 48 Degrees either North or South.

Deg Dec								Th	e]	De	gre	es	of	L	ati	itu	de.							
Degrees of Declination.	3	7	3	8	3	9	4	.0	4	1	4	.2	4	3	4	14	4	15	4	6	4	17	4	.8
	D	M	D	М	D	M	D	М	D	М	D	M	D	M	D	M	D	M	D	M	D	M	D	M
c		14,10		1 1 1	00			1 10 10 10		Can The St.										A GALLERY	22. 1		1 1 1	00
1	1 44. 1 04.	15		16	2 200			18								23					6.50	28	2	29
2	100	30	8	32	03	34														53		56		59
4	05	45 00			05																		05	59
~5	56	15	26	21	55	26	56	32	o6	38	05	44	o6	51	05	58	07	05	27	12	07	20	27	29
	27		27	37		43												100	18		08		38	59
7		Sec. 10.00	08	54		01										45			10		10		10	30
	11		11		10												1000		13	34		16	1	31
10	12	32	12	43	12	54	13	05	13	18	13	31	13	44	13	58	14	13	14	28	14	44	15	02
	13	49	14	01	14		1.4	25	14	39	14	53	15	07	15	22	15	38	15	56	16	15		34
12	-		15			31		45	100			15		31		48					1000	44	100	ot
1	17		16		16											13			18				19	12
15	18	54	19	10	9	27	19	44	20	04	20	23	20	43	21	0;	21	28	21	52	22	18	22	45
			The state of the s		20								5-9								23	200	24	20
	21		21		22	1								34		11.0	24		24		25	23		55
			23		23			47			24 25		24	59 25			25		26 27		26	57 32	29	07
	-		-		26		_	—	-		-		-	-	-		-	-	-	-	30	07	30	45
21	26	30	27	01	27	27	27	53	28	21	28	50	29	20	32	53	30	27	31	03	31	42	32	23
22	27	58	28	2:	28	49	29	16	29	45	30	16	130	48	31	22	31	58	32	37	133	18	34	03
23	20	17	29	43	29	11	30	40	31	11	31	43	32	16	32	51	133	30	34	12	134	56	35	43
23,29	29	56	30	22	30	50	31	20	31	52	32	28	33	03	33	40	34	20	35	03	35	48	36	35

A TABLE of Amplitudes, from the Latitude 49 Deg. 00 Min to the Latitude 60 Degrees either North or South.

Deg Decl								TI	ie	De	gre	ees	of	L	atit	ud	e.							
Degrees of Declination.	4	19		0		51	ı	5 2		5		54		55		56		57		58		59		60
	D	M	D	M	D	M	D	M	D	M	D	M	D	M	5	M	D	M	D	M	D	М	D	1
1	01	31	01	33 06	01	35 10	01	07	01	39	21 23	42	01	45)1)3	47	01	50	01	53 46	01	5' 53)2 4	
3	o6	34 of	o4 :6	14	04 06	46	06	5 ² 30	06	59 39	06	43	06	59	o7	10	05	31	05	34	07	47	06	
5 6	29	10	09	21	09	33	09	46	10	00	10	15	10	30	10	47	11	11 04 56	11	22	11	42	12	
8 9	12	14	12	29	12	45	13	02	13	21	13	41	14	02	14	24	14	48	15	14	15	41	16	
11 12 13	16 18 20	54 28 03	17 18 20	16 52 29	17 19 20	39 18 57	18 19 21	03 44 26	18 20 21	29 12 57	18. 26 22	57 43 30	19 21 23	26 15 05	19 21 23	56 49 43	20 22 24	33 29 25 23 21	21 23 25	04 04 07	21 23 25	43 47 54	22 24 26	
15 16 17 18	23 24 26 28	14 51 28 06	23 25 27 28	45 24 03 43	24 25 27 29	18 59 41 24	24 26 28 30	52 36 21	25 27 29 30	28 16 04 53	26 27 29 31	07 58 50 42	25 28 30 32	49 43 39 35	27 29 31 33	34 32 31 33	28 30 32 34	22 24 27 34 46	29 31 33 35	14 21 28 40	30 32 34 36	12 22 32 53	31 33 35 38	
20 21 22	31 33 34 36	25 06 48 33	32 33 35 37	08 52 37 26	32 34 36 38	54 41 30 23	33 35 37 39	44 34 27 24	34 36 38 40	39 31 29 29	35 37 39 41	35 32 26 40	36 38 40 42	36 39 47 56	37 39 42 44	42 51 04 19	38 41 43 45	53 09 27 50	40 42 44 47	12 34 59 30	41 44 46 49	37 05 40 21	43 45 48 51	

A TABLE of Amplitudes, from the Latitude 61 Deg. 00 Min. to the Latitude 66 Deg. either North or South.

Degrees Declinat		Т	he	De	gr	e e s	of	La	atit	ud	e.	
egrees of eclination.	6	1	6	2	6	3	(54	6	5	6	66
	D	M	D	M	D	М	D	M	D	M!	D	M
¢	00	00	00		00		00			111	ဂဝ	
1	02	03	02		02		02		02	22		27
2	1		04	15			04		94		04	55
3	08	12	06	32	05	17	09		07	30	2.	52
4	00	./		2 -	. 0	,,,	09		-09	30	-9	٠,
5	10	21	10	41	11	04	11	28	11	54	12	22
(12	27	12		13		13		14	19		53
7	14	34	15		45		16	08		45	17	26
8	16	40	17		17	51	18	30	19	13	20	00
, 9	18	49	9	28	20	09	20	54	21	43	22	37
10	20	57	21	40	22	27	23	18	24	13	25	14
11	23	10	23		24	51	49	48			27	58
12		2	26	17	27	15	28	19	1		30	4
13	27	39	28	37	29	42	30		32		33	34
14	29	56	31	01	32	12	33	30	34	55	36	20
15	32	16	33	27	34	45	36	11	37	46	39	3
16			35		37		38	57	40		42	40
17	37	05	38		40	05		49	1		45	58
18	19	36	4 I	10	42	54	44	49	46	59	49	20
19	42	11	43	54	45	49	47	57	50	23	53	1
20	44	52	46	4	18	53	51	17	54	02	57	1.
21	47	40	19	41	52	07	54	50	157	59	61	4
	50		52	56	55	36	58	43	62	20	07	0
23		42	56	20	159	24	63	02	67	36	73	5
23,29	155	17	58	04	61	22	65	22	70	33	178	2

The Ute of the TABLES of Amplitudes.

The Amplitude of the Sun, or any Star, is so many Degrees Distance as they rise or set from the East or West Points of the Horizon, either Northerly or Southerly.

Note, When the Sun or Stars have North Declination, then the Amplitude found by these Tables must be reckoned from the East toward the North at their Rising, or from the West toward the North at their Setting.

But if they have South Declination, then the Amplitude must be reckoned from the East toward the South at their Rising, or from the West toward the South at heir Setting.

To find the true Amplitude by the Tables.

Look for the given Latitude at the Top of the Table, and the Declination in the first Column to the Left-Hand, and in the common Angle of Meeting you will find the Amplitude required, in Degrees and Minutes.

Case ist. WHEN the Latitude and Declination are both given in even Degrees, as for Example. Suppose I would know the Sun's true Amplitude at his Rising in the Latitude of 40.00, his Declination being 17.00 N.

Under Latitude 40, and right against Declination 17, I find 22 26, which is the Sun's true Amplitude, to be counted from the Fast towards the North, (because it is at his Rising, and the Declination is North) that

is, E. 22 26 North.

Case 2d. When the Latitude is given in even Degrees, and the Declination in Degrees and Minutes, as for Example. Suppose I would know the Sun's true Amplitude at his Setting, in the Latitude of 57.00, his Declination being 11 33 S.

Find his Amplitude as before, for the Latitude 57, and for

the Declination { 11 deg } which will be { 20 29 } then

fubtract the Less from the Greater, the Diff. is 1 56, or 116 Minutes, to which put two Cyphers, and it makes 11600, which Number must be divided by the Number standing against the odd Minutes of Declination (in the following Table) which in this Case is 181, and the Quotient gives the proportional Parts in Minutes, which Parts are always to be added to the Lesser of the two Amplitudes which you took the Difference of, and the Sum gives the true Amplitude as follows.

181)11600(64 proportional Parts in Minutes, 740 makes 1 Deg. 4 Min.

Case 3d. When the Declination is given in even Degrees, and the Latitude in Degrees and Minutes, as for Example. Suppose I would know the Sun's true Amplitude at his Rising, in the Latitude 51 14, his Declination being 14.00 S.

Find his Amplitude as before, to 14 Degrees Declination, and for the Latitude \{ \frac{51}{52} \text{ Deg.} \} which will be \{ \frac{22}{23} \text{ o8} \} and fubtract

the Less from the Greater, the Difference is ___ o 31 Minutes

To the Difference of Amplitudes found on the foregoing Side, which is 31, put two Cyphers, and make it 3:00, which must be divided by the Number standing against the odd Minutes of Latitude, (in the following Table) which in this Case is 428, and the Quotient gives the proportional Parts in Minutes, to be added to the lesser of the two Amplitudes, as in Case the 2d.

428)3100(7 proportional Parts in Minutes.

Leffer of the Amplitudes————	22	37
	00	
True Amplitude—————————	-E. 22	44 S.

Case 4th. When the Latitude and Declination are both given in Degrees and Minutes, as for Example: Suppose I would know the Sun's true Amplitude at his Setting, in the Latitude 49 18, his Declination being 19 41 N.

First, Find his Amplitude for Latitude 49 Degrees, and Declination 19 41 (as in Case 2d) which will be 30 53.

In the same Manner sind his Amplitude for Latitude 50 Degrees, and Declination 19 41, which will be 31 35.

Then from the Greater Amplitude—————31	35
Subtract the Less——————30	53
	42 Minutes.

Put two Cyphers to this Difference, it makes 4200, which must be divided by the Numbers standing right against the odd Minutes of the given Latitude (in the following Table) which in this Case is 333, the Quotient gives the proportional Parts in Minutes, to be added to the Lesser of the two Amplitudes, &c.

The Lesser Amplitude	-30	53	
Proportional Parts to be added ————————————————————————————————	-00	12	
True Amp. for Lat. 49. 18, and Decl. 19 41 N. W.	31	05 N.	1000

A TABLE of Numbers for finding the proportional Parts to the odd Minutes of Latitude or Declination, in finding the Sun's true Amplitude.

Odd Minutes.	Num- bers	Odd Minutes	Num- bers.	Odd Minutes.	Num- bers	Odd Minutes:	Num- bers
1 2 3 4 5 6 7 8 9 10	6000 3000 2000 1500 1200 1000 857 750 666 600	16 17 18 19 20 21 22 23 24 25 26	375 353 333 316 300 285 273 261 250 240 230	31 32 33 34 35 36 37 38 39 40	193 187 181 176 171 166 162 158 154	46 47 48 49 50 51 52 53 54 55	130 127 125 122 120 118 115 113 111
12	545 500 461	27	222	41 42 43	146	56 57 58	107
14	428 400	30	207	44 45	136	59	101

The Use of this Table is to find a Number to divide the Difference of Amplitudes by, in order to find the proportional Parts, when the Amplitude is required for any Latitude or Declination that is given in Degrees and Minutes, (as in the foregoing Cases) to find which Number, look in some of the Columns under the title of odd Minutes for your given Min. of Latitude or Declination; as suppose for 37 Minutes, and right against that you will find 162, which is the Number required.

To find the Variation of the Compass by an Ampiitude.

To do this, you must have given both the true and magnetic Amplitudes.

The true Amplitude is to be found by the Tables as before taught.

The magnetic Amplitude is to be found by the Compass, at the Time of the Sun's Rising or Setting, and is so many Degrees or Minutes as you see it rise from the East, or to set from the West, either to the Northward or Southward: As for Example, suppose, being at Sea, I find, by setting the the Sun with my Compass, that he rises 10 deg. 15 min. to the Northward of the East, then the magnetic Amplitude is E. 10 15 N. or suppose I find by the Compass, that he sets 14 deg. 12 min. to the Southward of the West, then the magnetic Amplitude is W. 14 12 S.

Then if your Amplitude and magnetic Amplitude are both to the Northward, or both to the Southward, subtract the Less from the Greater, the Remainder is the Variation.

But if one be to the Northward, and the other to the Southward, add them together, and the Sum will be the Variation.

Example 'st.	True Amplitude — — — Magnetic Amplitude — —	E. 18	M. 34 N. 37 N.
	Variation————	 04	03 Easterly
Example 2d.	True Amplitude————————————————————————————————————	W. 2	o6 N.
	Variation————	<u> </u>	17 Westerly

And thus having found how much the Variation is, it remains in the next Place to find which way it is, that is, whether it be Easterly or Westerly.

Rule. If the Amplitude be taken at Sun-rising, and the magnetic Amplitude be farther from the North than the true Amplitude is, then the Variation is Westerly; but if it be nearer to the North, it is Easterly.

If it be taken at Sun-setting, if the magnetic Amplitude be farther from the North than the true Amplitude is, then the Variation is Easterly, but if nearer to the North, it is Westerly, as may be seen by the two foregoing Examples.

By keeping a Journal, is meant, keeping such an Account of the Ship's Way, that at any Time you may be able to know what Latitude and Longitude the Ship is in.

When a Ship is bound from any one Place to another, that lies so far from it, that she is obliged to go out of Sight of Land for any considerable Time, as suppose from England to Barbadoes, then at the Time she leaves the Land, she is said to take her Departure, and that Part of the Land she then leaves, as suppose the Start, the Lizard, the Land's End, &c. is said to be the Place they take their Departure from; and at the Time of taking such Departure, the Captain or Mate generally takes the Bearing and Distance of that I and, according to his Judgment, and sets it down on the Log-board, or in the Log-book, against the Time it was taken, thus;

Lizard, N. by W. Distance 5 Leagues.

Or, Start, NNE. Distance 6 Leagues, &c.

And in the same Manner for any other Place, Bearing and Distance, as you will see in the first Day's Log, in the following Journal.

The Log-book being marked as follows, with Columns for Course, Distance, Northing or Southing, Easting or Westing, Latitude by Dead Reckoning, Latitude by Observation, Meridian Distance, Longitude made, and Longitude in, you are to take Notice.

That in the Column for Course you are always to set down the Course you have made by your Reckoning for those 24 Hours, (that is, from the Noon of the Day before, to the Noon of the Day you work on) the Sea Account being always kept from Noon to Noon.

In the Column of Distance you are to set down the Distance made by your Reckoning for these 24 Hours.

In the Column for Northing and Southing, you are to set down the Difference of Latitude made that 24 Hours, marking the Column with N. if the Difference of Latitude be Northerly, or with S. if it be Southerly.

In the Column of Easting or Westing, you are to set down the Departure made that 24 Hours, marking the Column with E. if the Departure be Easterly, or with W. if it be Westerly.

In the Column marked Lat. by D. R. you are to set down the Latitude you reckon yourself in on that Day.

In

In the Column marked Lat. by Obs. you are to set down the Latitude you find yourself to be in by Observation, if you have one, if not, then let it stand open.

In the Column for Mer. Dist you are to set down (in Degrees and Minutes) how much Departure you have made in all from the Place you took your Departure from.

In the Column of Long. made, you are to fet down (in Degrees and Minutes) how much Difference of Longitude you have made in all from the Place you took your Departure from.

In the Column of Longitude in, you are to set down what Longitude you find yourself to be in on that Day by your Reckoning.

Note, The Account of Longitude made, being what is always kept in his Majesty's Navy; and the Account of Longitude in, being most generally kept on board the Merchant Ships: I shall in this Treatise shew how to keep them both, and shall leave it to the Practitioners Choice which he will make Use of, they both being equally true, and there being no Occasion to keep more than one of them.

And now having (I think) given a sufficient Account of Things that are to be set down in the different Columns, I shall lay down these few necessary Rules following, and then proceed to shew how they are all to be found, or the Method of working a Day's Work at Sea.

Rule ist. Variation, if there be any (as most certainly there is) must be allowed upon all Courses steered, and upon all Bearings, &c. that are taken by the Compass, that is, if it be the Easterly Variation, it must be allowed to the Right Hand; but if Westerly Variation, then to the Lest Hand of the Course or Bearing: Suppose yourself placed in the Centre of the Compass, and looking directly forward to the Point you are to allow the Variation from.

Example. Suppose I steer S.W. and there is one Point Westerly Variation, then my true Course will be S.W. by S. or suppose I set a Point of Land, and find it to bear by my Compass E.S.E. and I know there is half a Point Easterly Variation, then the true Bearing is SE. by E. $\frac{1}{2}$ E.

Rule 2d. Lee-way (which I need not here describe, being sufficiently known to every Seaman) must be allowed to the Right Hand of the Course steered, when the Larboard Tacks are Aboard, and to the Lest-Hand when the Starboard Tacks are Aboard.

Example. Suppose I steer NE by E. with the Larboard Tacks aboard, and make one Point Lee-way, then my Course made good is ENE.

Rule 3d. Lee-way and Variation, when they are both to be allowed one Way, that is, both to the Right-Hand, or both to the Left, add them together and allows their Sum the forms Way they were to be allowed.

ther, and allow their Sum the same Way they were to be allowed.

But if they are to be allowed, one to the Right-Hand, and the other to the Left, subtract the Less from the Greater, and allow the Remainder the same Way as the Greater of them was to be allowed.

Example. Suppose I steer NNW. with my Starboard Tacks aboard, and make one Point Lee-way, there being at the same Time half a Point Westerly Variation, I would know my true Course?

Lee way to the Left-Hand — 1 o Point Variation to the Left-Hand — 0 1/2 Point

Their Sum to be allowed to the Left-Hand I $\frac{1}{2}$ Points, makes the true Course NW. by N. $\frac{1}{2}$ W.

Example 2d. Suppose I steer SW. by W. with my Larboard Tacks aboard, and make $2\frac{1}{2}$ Points Lee-way, and I have $1\frac{1}{4}$ Points Westerly Variation, what is my true Course?

The Remainder to be allowed to the Right-Hand I & Points, makes the true Course WSW. & W.

Rule 4th. When a Ship is lying too under a Mainfail, Mizen, &c. then observe how she comes up and falls off, and take the Middle between the two Points, and from that allow the Lee-way and Variation, as in Rule 3d.

Example. Suppose a Ship lying too under a Main sail, with the Starboard Tacks aboard, comes up E. by S. and falls off to NE. by E. there being one Point Westerly Variation, and she makes 5 Points Lee-way, what Course does she make good?

The Middle between E. by S. and NE. by E. is E. by N. from which allowing fix Points to the Left-Hand, by Rule 3d, the true Course will be N. by E.

Rule 5th. Currents, the Way they set you, and the Distance you suppose you are driven by them, is to be set down in the Traverse Table for the Day, as any other Course or Distance.

Example

Example. Suppose I try the Current, and find it to set W. by N. per Compass i Mile per Hour, the Variation being one Point Easterly, then if I sail in that Current 24 Hours, I set down in the Traverse Table, as a Course, WNW. distant 24 Miles.

Rule 6th. Heave of the Sea is to be accounted for in the fame Manner as Currents: As suppose there is a great Sea heaving toward the SW. by my Compass, there being $\frac{1}{2}$ Point Westerly Variation, I then set down in my Traverse-Table SW. by S. $\frac{1}{2}$ W. with so much Distance as I judge the Sea has heaved the Ship.

Rule 7th. At leaving the Land, the opposite Point to the Bearing (with the Variation allowed upon it) and the Distance you judge yourself from it, must be set down in the Traverse-Table, as a Course and Distance.

Example. Suppose having 4 Westerly Variation, the Start bears by my Compass NNE. distant 4 leagues, the opposite Point to NNE. is SSW. which with the Variation makes S. 3 W. for the Course to be set in the Traverse Table, distant 12 Miles.

Rule 8th. When you make the Land, the Bearing itself (with the Variation allowed upon it) and the Distance you judge yourself from it, are to be set in the Traverse-Table, as a Course and Distance: This needs no Example.

Note, If you keep only the Account of Longitude made, and would at any Time know what Longitude you are in, look out the Longitude of the Place you took your Departure from, and with that Longitude, and the Longitude made, taken as Difference of Longitude, find the Longitude come into, by the Rules in Page 107, and 108. And the Longitude fo found must be counted from the same Meridian that the Tables you looked out the Longitude of the Place departed from, counts it.

RULES to correct the Dead-Reckoning by an Observation.

WHEN yo have made all the proper Allowances you can, fuch as for Variation, Lee-way, Currents, &c. and still find that your Latitude by Dead Reckoning will not agree with the Latitude by Observation, within five Minutes, then you must correct as follows.

CASE the First.

If your Course found by Dead Reckoning be due North, or due South.

Rule. First find the Difference of Latitude (in Miles) between the last Observation, and the Observation on the Day you correct, which will be the true Difference of Latitude, then will your true Course be the same as the Course by Dead-Reckoning. Your true Distance the same as the true Difference of Latitude. Your Departure co, and your Meridian Distance, Longitude made, (or Longitude in) will be the same as they were on the Day you had the last Observation.

CASE the Second.

If the Course found by Dead-Reckoning be less than three Points, or less than thirty-three Degrees.

Rule, First find the Difference of Latitude (in Miles) between the last Observation, and the Observation on the Day you correct, which will be the true Difference of Latitude. Then make your true Course the same as the Course found by Dead-Reckoning, since the last Observation, and with that Course, and the true Difference of Latitude, find the true Distance and Departure, (as in Plane Sailing Case the 2d. Page 48.) then to find the Meridian Distance, the Longitude made, and the Longitude in, take the following Rule.

N.B. The Difference of Longitude is to be found by the true Course, and the Meridian Difference of Latitude between the two Observations (as usual) and the Meridian Distance, Longitude made (or Longitude in) are to be found by adding, or subtracting the true Departure and Difference of Longitude to, or from the Meridian Distance, Longitude made (or Longitude in) on the Day you had the last Observation, which is the Day you always correct from.

CASE

CASE the Third.

If the Course found by Dead Reckoning be more than three Points, or more than thirty-three Degrees, and less than 6 Points, or 67 Degreees and a Half.

Rule, First find the Difference of Latitude in Miles between the last Observation, and the Observation on the Day you correct, which will be the true Difference of Latitude: Then with the Course sound by Dead-Reckoning, since the last Observation, and the true Difference of Latitude, find a new Departure (by the second Case of Plane Sailing, Page 48.) add this new Departure to the Departure found by Dead Reckoning since the last Observation, and take half their Sum for your true Departure: Then you have given the true Difference of Latitude and Departure to find your true Course and Distance, (by Plane Sailing, Case the 6th) read here N.B. in Case the 2d.

CASE the Fourth.

If the Course found by Dead Reckoning be more than six Points, or sixty-seven

Degrees and Half.

Rule, First find the Difference of Latitude in Miles between the last Observation, and the Observation on the Day you correct, which will be the true Difference of Latitude, and make your true Departure the same as the Departure found by Dead Reckoning since the last Observation: Then you have given the true Difference of Latitude and Departure, to find the true Course and Distance, (by Plane Sailing, Gase 2d.) read here N.B. in Case 2d.

Note, As the Knowledge of which Case you are to correct by, depends upon knowing your Course by Dead Reckoning, and as when you correct only for one Day, that Course is always sound by the Difference of Latitude and Departure in your Traverse Table for that Day; therefore if you are to correct for a longer Time than one Day, you must take the Northing, Southing, Easting, and Westing, that you have made for every Day since the last Observation, (or if it be your first Observation, then for every Day from your leaving the Land) minding not to leave out the Difference of Datitude and Departure for the Day you are correcting on, and bringing them into a Traverse Table; by which you will find the whole Difference of Latitude and Departure, made by Dead - Reckoning since the last Observation, and with that same Difference of Datitude and Departure,

132 Rules to correct the Dead-Reckoning, &c.

find the Course made by Dead-Reckoning, then observe which of the foregoing Cases that Course comes under, and correct by the Rules for that Case, finding every Thing except the Distance.

And when you have so corrected, you are to set down in your Book only the Latitude by Dead Reckoning, the Latitude by Observation, the Meridian Distance, and the Longitude made (or Longitude in) and rub

out the Course, Difference of Latitude and Departure.

Then you have given the Latitude by Observation on the Day you correct, and the Latitude by Dead Reckoning on the Day before it, to find the Difference of Latitude for the last 24 Hours (by the Rules for Latitude, Page 105.) Also the Meridian Distance on the Day you correct, and the Meridian Distance on the Day before it, to find your Departure, (by subtracting the lesser from the greater, if they are both East, or both West; or by adding them together, if one be East and the other West.) And with that Difference of Latitude and Departure find your Course and Distance, (by the 6th Case of Plane Sailing) which Course, Distance, Difference of Latitude and Departure are to be set down instead of those you rubbed out.

Rules to find the Meridian Distance.

Case 1st, If the Meridian Distance on the Day you work from the East, and you have sailed to the Eastward; or if it be West, and you have sailed to the Westward, then add the Departure to the Meridian Distance, and the Sum will be the Meridian Distance you have made, of the same Name with that you worked from.

Case 2d, If your Meridian Distance be East, and the Departure be Westerly; or if the Meridian Distance be West, and Departure Easterly, then subtract the Less from the Greater, the Remainder will be the Meridian Distance you have made, of the same Name with the Greater of the two.

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A

JOURNAL

OF

A VOYAGE from ENGLAND

TOWARDS

MADEIRA.

134 A Journal from England towards Madeira.

Н.	К.	нк	F.	Courfes	Winds	Lec- way	Transactions, Thursday, May the 11th, 1780.
2 4 6 8 10 12 2 4 6	The 4 4 5 5 5 5 5	Start	N	byE.Di SWbW 		ag.	Moderate Gales, and fair Weather, at 6 (p. m.) the Start bore as per Long. from which I take my Departure, it being in the Latitude 50.7 N. and Long. of 3.45 W. from London.
8 10 12	5 5 6	I I					Variation 4 Point Wosterly.
Cou				W Lath 48		at.by	Ob Mer. Dist. Lon. made Lon. in 00 53W 01 22 W 05 07W

The Manner of working this Day's Work.

The opposite Point to the Bearing of the Land is S. by W. which with the Variation allowed upon it (as before taught) makes S. 4 E. and the Distance from the Land 6 Leagues, or 18 Miles, which are to be set down for the first Course and Distance in the following Traverse-Table.

Then the first Course steered being S. W. by W. the Variation allowed upon it will make it SW. by S. \(\frac{1}{4}\) W. and the Sum of all the Distances from 8 o'Clock, where that Course begins, to 2 o'Clock where it ends, being 18 Miles and a Half, I double that Sum, because the Book is marked only for every two Hours, and it makes 37 Miles for the Distance belonging to that Course. But if the Book had been marked for every Hour, as it is in the Navy, and aboard the East India Ships, then I must have taken the Sum without doubling it for the Distance, and in the same Manner I reckon the other Course and Distance; all which will be as in the following Traverse-Table.

And then every Thing being found as on the other Side, I set them down in their proper Columns as above.

· Course

Courfes I	Dist. N.	S.	E.	W.	
S. \(\frac{1}{4}\) E.	18	18.0	0.9		
SW by S. 3 W.	37	27.4		24.8	
SSW 3/4 W.	56	48.0		28.8	
Diff. of Latitu	de South	93.4	0.9	53.7	
				0.9	
				52.7	Dep. W

The feveral Courses and Distances in this Table being looked out and cast up as n the Rules for Traverse Sailing (Page 52,) I find my Difference of Latitude to be 93 Miles and 4 Tenths, and my Departure 52 Miles 7 Tenths; then I mark down (upon my Slate, or the Paper that I work upon) every Thing that is to be found, and as I find what

they come to, I fet against them as follows:

1,24	CourseS	. 30	00 W
	Distance		
	Diff. of Lat.	- 93	S.
	Departure -		
()	Latitude by D.R. 48 -	• 34	N.
D.R	Lat. by Observation		
	Meridian Dist ————————————————	53	W.
	Longitude made -o1		
	Longitude in-05		

Because the Diff. of Lat.isS. and the Dep. W.

Note, When the Tenths in any Side are more than 5, or half a Mile, you must call that Side I Mile more than you found it to be; but when they are less than 5, then you need take no Notice of them. As in this Case the Diff. of Lat. being 93.4 I reject the 4th Tenths, and call it only 93 Miles, and the Dep. being 5227 instead of the 7 Tenths I put I Mile to it, and call it 53 Miles.

But when you take the Difference of Latitude and Departure to find the Course by, then

take them in Miles and Tenths.

Then in the first Place, with my Difference of Latitude 93.4, and my Departure 52.7, (as taught in Plane Sailing, Cafe the 6th) I find my Course to be 30 Degrees, and my Distance 108 Miles, which I set down against Course and Distance as above.

Second, For the Latitude by D. R.

Third, For the Meridian Distance.

Take the Latitude failed from 50 07 N. And the Diff. Lat. 93 Miles, or 1 33 S. Day's Work, is always the sub. (as per Rule) gives Lat. D.R. 48 34 N. Dep. which here is 0.53 W. Note, the Meridian Distance on the first Day's Work, is always the fame as that Day's

Fourth, For the Difference of Longitude. The Meridional Parts of-3485 The Latitude failed from-Of the Lat. by D. R .-3343 Meridional Difference of Latitude 142

Then I look for my Course 30 Degrees, in the Tables of Diff. of Lat. and Dep. and for the Meridian Diff. of Lat. 142, in some of the Diff. of Lat. Columns belonging to that Course, the Dep. 82, which answers to that Diff. Lat. is my Diff. Long.

Fifth, for the Longitude made.

The Longitude made on the first Day's Work, is always the fame as that Day's Diff. of Long. which here is ____ 1 22 W. | Sub. (as per Rules) gives Long.in 5

Sixth, For the Longitude in. Take the Longitude failed from 3° 45' W. And the Diff. Long. 82 Miles, or 1 22 W.

H.	K.	HK	F. C	ourses	Wind	ls Lee- way	Transactions, Friday, May the 12th, 1780.	
2	6		S	WbW	N			
4	5	I					Moderate Gales and fair	
6	5				NV	V	Weather, at 8 (a m.) far	
8	5						Ship to the Northward.	
10	4	I		SW				
I 2	4	I						
2	4	I			WNI	N		
4	4	1						
6	4	1						
8	5		S	WbyS				
10	4	I					Variation 4 Point Westerly.	
12	4							
Cou	rſe	Dist.	$S \mid V$	V Latb	yDR	Lat.byC	Ob Mer. Dist Lon. made Lon.	
	oo W			1 46			1 54 W 2 55 W 6 40	

The Variation being allowed, and the Distances summed up as before, the Traverse-Table will be as follows.

- Courfes	Dift.	N.	S.	E	W
SW by S 4 W	43		319		28
$SSW = \frac{3}{4}W$	45		386	40	23.1
S by W 3 W	27		25 4	11.7	0.1

First, With my Difference of Lat. 95.9, and Departure 611, (by Plane Sailing, Case 6,) I find my Course to be 33 Deg. and my Distance 144 Miles.

Second, For my Latitude by D.R.
Take the Latitude in yesterday 48 34 N.
And my Diff. of Lat. 96 Miles or 1 36 S.
Gives the Latitude by D. R. — 46 58 N.

Third, For the Meridian Distance.

Take the Mer. Dist. yesterday—0 53 W. And the Departure to day—1 01 W.

Gives the Meridian Distance—1 54 W.

	Course————————————————————————————————————	33	00 .W 114 Miles
	Difference of Lat. —		96 S.
Ву	Departure ———		61 W.
	Lat. by D. R.	46	58 N.
D.R.	Lat. by Observation		
	Meridian Distance—		
1	Longitude made —	2	55 W.
(Longitude in-	6	42 W.
Fou	rth, For the Diff. of I	ong	itude.
Take the	Mer. Parts of yest. L	at	3340
	he Latitude to-day-		

Fifth, For the Longitude made.

Take the Long. made yesterday — 1 22 W.

And the Diff. of Long. to-day } 1 33 W.

Gives the Long. made to-day — 2 55 W.

with which, and the Course (as in the first

Day's Work) I find my Diff. of Longitude to

Gives the Mer. Diff. of Latitude -

Sixth, For the Longitude in.

Take the Long. in yesterday 5 07 W.

And the Diff. of Long. to-day 1 33 W.

Gives the Longitude in 6 40 W.

Н.	K.	HK	F.	Courfes	Winds	Lee- way	Transactions, Saturday, May the 13th, 1780.
2	4		-	SW	WNW		
4	4						Moderate Gales, and Cloudy.
6	4						
8	4	1		SWbS	WbyN	$\frac{1}{2}$	
10	4	I					
12	4	I					
2	4	1		In Ift Rec		pfails	
4	4			SSW	W	I	
6	4		_				
8	4						V-:-: D: W 0 1
10	4						Variation 1 Point Westerly.
12	4		1		<u> </u>		1
Coti	ırfe	Dist.	S	WLath	by DR L	at by	Ob Mer. Dist. Lon. made Lon. in
110	ooW	97	95	24 45	23N.		2 18 W. 3 29 W. 7 14 W

The Leeway and Variation being allowed, as before taught, the Traverse-Table will be as follows.

Courfes	Dist.	N.	S.	E.	W.
SW by S	24		20.0		13.3
S by W ½ W	36		34.5		10.4
South	40		40.0		
			95.5		23.7

First, The Course and Distance sound (by Plane Sailing Case 6) as before, will be as in the other Column.

Second, For my Latitude by D.R.

Take the Latitude in yesterday 46 58 N.

And the Dist. of Latitude 95

Miles

Gives the Latitude by D.R. — 45 23 N.

Third, For the Meridian Distance.

Take the Mer. Dist. yesterday

And the Departure to-day

O 24 W.

Gives the Meridian Distance

2 18 W.

By Difference of Lat. 95 S. Departure — 24 W. Lat. by D.R.—45 23 N. Lat by Obser.—

Meridian Dift.— 2 18 W. Longitude made 3 29 W. Longitude in— 7 14 W.

Fourth, For the Diff. of Longitude.

The Mer. Parts of yesterday's Lat. — 3200
Of to-day's Latitude — 3063
The Mer. Diff of Latitude — 137
with which, and the Course (as before) I find the Diff. of Long. to be 34 Miles West.

Fifth, For the Longitude made.

Take the Long. made yesterday— 2 55 W. And the Diff. of Long. to-day— 0 34 W. Gives the Longitude made — 32 9 W. Sixth, For the Longitude in.

Take the Long. in yesterday— 6 40 W. And the Diff. of Long— 0 34 W. Gives the Longitude— 7 14 W.

Н.	K.	нк	F.	Courfes	Winds	Lee- way	Transactions, Sunday, May May the 14th, 1780.	
2	4		-	S	WSW	1		
4	4						Moderate Gales, and hazy the	
6	4	1					first Part, the latter fresh Ga	
8	4				ef both To		and Kain.	
10	4			SSE.	SW.	$I\frac{1}{2}$		
12	4	1	100					
2	4							
4	4				/			
6	4				he Fore 7			
8	4			S by E.	SWbW	2		
10	4				T 1		Variation 1 Point Westerly.	
12	3	I	1		Tack'd			
Cou	rſe	Dift.	S	E. Lath	by DR L	at by	Ob Mer.Dist. Lon.made Lon. i	
3 20	oo E	02	72	60 44	IIN.		1 18 W. 2 07 W. 5 52 V	

The Ship having her Starboard Tacks aboard, when the Leeway and Variation are allowed, (as before taught) the Traverse-Table will stand as follows:

Courfes	Dift.	N.	S.	E.	W.		Course—S. 39 00 E. Distance — 93 Mi
SSE.	33		30.5	12.6			Difference of Lat. 72 S.
$S E \frac{1}{2} E$.	40		25.4	30.9		Ву	Departure — 60 F Lat. by D. R.—44 11 N.
SE.	23		16.3	16.3		D.R.	Lat. by Obser.—
			72.2	59.8			Meridian Dift 1 18 W. Longitude made 2 07 W.
							Longitude in 5 52 W.

Having been very particular in explaining the Manner of working a Day's Work, (in the three foregoing Days) and as all Day's Works, where there is no Correction wanting, are to be worked from the Difference of the Latitude and Departure found by the Traverse-Table, (as before) I have only set down the Traverse-Table, and what all the other Things come to, and have left the finding them to exercise the Learner.

н.	K.	н к	F.	Courses		Lee- way	Transactions, Monday, May the 15th, 1780.
2	4			NWbW	SWbW	2	
4 6	3						Fresh Gales, and Rain all these 24 Hours.
8	3					3	
10	3			Hand I	Main To	opsail	
12	3	I		NW	WSW	3	
2	3	I					
4	3	I					
6	3						
8	3						
10	3			NW b N	W by S	$3\frac{1}{2}$	Variation 1 Point Westerly.
12	3		1.3			1	
Cou	ırfe	Dift	S	WLat	byDRL	_at.by	Ob Mer. Dist. Lon. made Lon. in
N29	ooW	75	65	36 45	16 N.		1 54 W 3 00 W 6 45 W

The Ship having her Larboard Tacks aboard, when the Leeway and Variation allowed, the Traverse-Table will stand as follows:

Courfes	Dift.	N.	S.	E.	W.		Course — N. Distance —		
NW	32	22.6			22.6		Diff. of Lat.		75 65
NW	33	30.5	(=111)		12.6	Ву	Departure —— Lat. by D.R. —		36
N = W	12	11.9		1.2	D,R. Lat. by Obser.—		10		
		65.0			36.4		Meridian Dist.— Longitude made	1	54
					w 157 (c)		Longitude in —	6	45

To find the Course.

Note, In this Case the Difference of Latitude being just 69 Miles without any Tenths, after you have put two Cyphers to the Departure, you must not divide it by 65, but by 650, the Figures being put to supply the Place of Tenths, as directed in the Rule for Plain Sailing.

Diff. Lat. D. with Cyphers (56 the 3900)

Natural Tang. of the Course answering to 29d. 15m. or (neglecting the 15m. 29d. N.W.erly)

н.	K.	нк	F.	Courfes	Winds	Lee- way	Transactions, Tuesday, May the 16th, 1780.
_ 2	3			WNW	SW	$3\frac{1}{2}$	Hard Gales, and Squaly, with
6	3 3		1	Handed		refail	Rain.
8	Lay	-too,	u	p NW.	off N.	5	
10	Dri	ft 1 1/2	Mi	iles per	Hour.		
2 4 6			Up	NbyW.off	NE byN		
8				PNNWo			
10			S	et the F	orefail		Variation 1 Point Westerly.
Cou	rfe	Dift.	N	E Lath	DyDR L	at.by(Ob Mer. Dist. Lon. made Lon. in
N 8 c	00 E	35	34	5 45	50 N		1 49 N 2 53 W 6 38W

Having allowed the Leeway, and the Variation upon the first Course, and also from the Middle between what she comes up and falls off, (as taught in the Rules for laying too,) The Traverse-Table will stand as follows.

		34.2		16.3	11.4		Longitude in— 6 38
NE	6	4.2		4.2			Meridian Distance 1 49 Longitude made 2 53
NEbyE	9	5.0	E	7.5		D.R.	Lat. by Obser.—
NNE	12	11.1		4.6		Ву	Departure 5 Lat. by D.R — 45 50
VWbW½W	18	13.9			11.4		Difference of Lat. 34
Courses	Dist.	N.	S.	E.	W.		Course — N. 8 co l

н.	K.	HK	F.	Courfes Win	ds Lee	
2	3			N W WS	W 4	Fred Cales the G.A.D.
4 6	3			WNW SV	v	Fresh Gales the first Part, the latter moderate, with small Show-
8	3			Set Main	l'optail	ers.
10	3	I		NWWS	W 3	
12	3	I				
2	3	I		Set Fore	l'opfail	
4	4			W by SS by	W 2	1
6	4					
8	4			0 15 0		
10	4			Out 2d Reef bot		
12	4	I		W SS	$W \mid I^{\frac{1}{2}}$	
Cou	rfe	Dift.	S.	W Latby DI	Lat.b	Ob Mer.Dift. Lon.made Lon. in
N540	ooW	72	42	58 46 32 N		2 47 W 3 00 W 8 02 W

Courfes	Dift.	N.	S.	E.	W.
N by W	12	11.8			2.3
NW by N	12	10.0			6.7
NNW	21	19.4			8.0
W	32				32,0
$WbN\frac{1}{2}W$	9	0.9			9.0
		42.1			58.0

	Course - N.	54	00	W.
	Distance —		72	Miles
	Diff. of Lat.		42	N.
By	Departure —	30	38	W.
	∠Lat. by D.R. —	46	32	N.
D,R.	Lar. by Obser.			
	Meridian Dist.			W.
	Longitude made	4		W.
	Longitude in —	8	02	W,

н.	K.	нк	F	Courses	Winds	Lee- way	Transactions, Thursday, May the 18th, 1780.
2	4	I		WbyN	SWbS	1	
4	4 4	1		Out 1ft R	eef both T	opsails l	Moderate Gales, and thick nazy Weather.
8	4	I		W	SSW	$\frac{1}{2}$	
10	4	I				. 1	
12	_ 4	1				,	
2	4			W by S	S by W		
4 6	4						
6	_ 4						
8	4	I		wsw	S		Variation 1 Point Westerly.
12	3						
Cou	rſe	Dift.	s	WLath	yDR L	at.byO	b Mer. Dist. Lon. made Lon. in
820	ooW	95	13	95 46	19 N		4 22 W 6 33 W 10 18 V

Courfes	Dist.	N.	S.	E.	W.
W by N	26	5.1			25.5
$W b \overline{S_{\frac{1}{2}}} W$	27		2.6		26.9
$\overline{WSW_{\frac{1}{2}}W}$	32		9.3		30.6
SWbW ₂ W	13		6.1		11.5
		5.1	18.0		94.5
			5.1		
Diff. of	12.9				

	Courfe S. 82 co W.	
	Distance 95 Miles	1
	Difference of Lat. 13 S.	
By	Departure — 95 W.	
	Lat. by D R — 46 19 N.	
D.R.	Lat. by Obser.—	
	Meridian Distance 4 22 W.	
	Longitude made 6 33 W.	
	Longitude in— 10 18 W.	
17,000		

H.	K.	нк	F.	Courfes	Winds	Lee- way	Transactions, Friday, May the 19th, 1780.
2	2	I		WSW	S		Little Wind, and small
4 6	2	1					Showers of Rain.
6	2	<u> </u>					Showers of Ram.
8	2						•
10	2						
12	2						A great Swell from the SW. for which I allow 6 Miles.
2	I	I					for which I allow 6 Miles.
4	I	I		SWbW	S by E		
6	I	1	3				
8	I						
10		I					Variation 3/4 Point Westerly.
12		I				1	
Cou	ırfe	Dift.	S	WLath	DyDRL	lat.by	Ob Mer.Dist. Lon.made Lon. in
S ₅₇	ooW	34	19	29 46	oo N		4 51 W 7 15 W 11 00W

Courfes	Dift.	N.	S.	E.	W.
SW by W	30		16.7		24.9
\overline{SW}	10		7 1		7.1
NE by Ni	6	5.0		3.3	
		5.0	23.8	3.3	32.0
			5.0		3.3
			18.8		28.7

	Course - S. 57 00 W.
•	Diftance — 34 Miles
	Difference of Lat. 19 S.
Cor-	Departure — 29 W.
rected	Latitude by D.R. 46 oo N.
rected	Lat. by Obier,
	Meridian Distance 4 51 W.
	Longitude made 7 15 W.
	Longitude in 11 00 W.

Note, In this Day's Work the Swell coming from the S.W. leaves the Ship towards the N.E. and the Variation allowed upon it makes N.E. by N. for the last Course in the Traverse-Table.

H.	к.	HK	F.	Courfes	Winds	Lee- way	Transactions, Saturday, May the 20th, 1780.
2 4 6 8 10 12				Calm	(3.12) (3.13)	-	Tried the Current, and found it to be fet WSW. I Mile per Hour, at which Rate I allow it for this 24 Hours. Zenith Distance—27 52 S.
2 4 6 8				SSW	W		Declination ——— 17 41 N.
10	2 2	1					Variation 1 Point Westerly.
Cot	ırfe	Diff	s. s	WLat	byDR	Lat.by	Ob Mer. Dist. Lon. made Lon. in
S42	00 W	$\sqrt{\frac{3}{3}}$	2	4 22 45	36 N	45 33	N. 5 13 W 7 50 W 11 35

Courfes	Dift.	N.	S.	E.	W.
S by W	11		10.8		2.1
SW by W	24		13.3		20.0
			24.1		22.1

Course — S. 42 co W.
Distance — 32 Miles
Disterence of Lat. 24 S.
Departure — 22 W.
Latitude by D.R. 45 36 N.
Lat. by Obser. — 45 33 N.
Meridian Distance 5 13 W.
Longitude made 7 50 W.
Longitude in — 11 35 W.

Note, The Current fetting WSW. 1 Mile per Hour, I allow the Variation upon it, which makes it SW. by W. and fet it in the Traverse-Table, with 24 Miles Distance as above.

H.	к.	HI	KF.	Courfes	Winds	Lee- way	Transactions, Sunday, May the 21st, 1780.
2	3			S by W	W by S		
- 4	3	I					Moderate Gales and fair Wea-
6	4		- -				ther, at 9 (a. m.) spoke with Ship from Barbadoes, and bou
8	4						for London.
10	4						ror London.
12	4					-	
2	4						
4 6	4						
6	4						
8	4						
10	4						Variation 1 Point Westerly.
12	4						
Cou	rſė	Dift	S	- Lath	yDR L	at.by	Ob Mer.Dift. Lon.made Lon. in
Sou	ith	10	3 103	- 44	00 N 4	3 50	N 5 13 W 7 50 W 11 35 W

By Distance 93 Distance 93 Diff. of Lat 93 Departure 00 Lat. by D.R 44 00N. Latitude by Obser. 43 50N.	Cor- ected Cor- e
--	--

In this Day's Work, there being 10 Miles Difference between the Latitude by Dead-Reckoning and Observation, I am to correct, and therefore I do not find the Meridian Distance, &c. by (D.R.) as I did when there, was no Correction; but I mark them all down again as above, and correcting (as in Case the First, of the Rules for correcting) because my Course by D.R. since the last Observation was due South, I set them all down as in the above Correction.

H.

Н.	K.	HK	F.	Courses	Winds	Lee- way	Transactions, Monday, May the 22d, 1780.
2	4			SWbS	WNW		
4	4	1					Moderate Gales and fine clea
4	4	1					Weather.
8	4	1					
10	4						
12	4						
2	4	1					
4 6	4	I		SSW			
6	4						
8	4						
10	4		1				Variation 1 Point Westerly.
12	4	I					
Cou	rfe	Dift	. s	. W Lat	byDRL	at.by	Ob Mer. Dift. Lon. made Lon. i

Courfes	Dist.	N.	S.	E.	W.
SSW	60		55.4		23.0
SbyW	42		41.2		8.2
			196.6		31.2

A
Courfe S. 18 co W.
Distance 112 Miles
Difference of Lat. 106 S.
Departure — 35 W. Latitude by D.R. 42 13 N. Lat by Obser — 42 04 N.
Latitude by D.R. 42 13 N.
Lat by Obser - 42 04 N.
Meridian Distance 5 48 W.
Longitude made 8 37 W.
Longitude in — 12 24 W.

By	- Course-S.	18	00	W.
	Distance -			Miles
	Diff of Lat		97	S.
last '	Departure		31	W.
Obser	Latitude by D.R.	42	13	N.
vation	Latitude by Ob.	42	04	N.

Having found as far as to the Latitude by Dead-Reckoning and Observation, I see they differ 9 Miles, therefore I correct (by Case) the 2d) because my Course sound by Dead-Reckoning since the last Obser is less than 33. Degrees, and the Result is as above.

78 Miles 53 S. 57 W.

н.	K.	HK	F.	Courfes	Winds	Lee- way	Transactions, Tuesday, May the 23d, 1780.
2	4			SW	NW		
4	4	I					Moderate and Fair.
6	4		_				
8	4			SWbW			
10	3	. I		SWOW		1	
12	4	-	-	 			
2	4 3	I			N		
4	3.	I					
8	3	I					
10	3	I			NE.		Variation 3 Point Westerly.
12	3	I					
Cou	rfe	Dift.	S	WLath	DyDRL	Lat by	Ob Mer. Dift. Lon. made Lon. in
347	oo W	78	53	57 40	59N.	41 11	N. 6 45 W. 9 53 W. 13 38 V

Courfes Dift. N.	26.5 38.9	19.7	Cor-	Course————————————————————————————————————
	65.1	[62.7]	recteu	Lat. by Obser.—41 11 N. Meridian Dist.— 6 45 W. Longitude made 9 53 W. Longitude in —13 38 W.

```
Course —— S. 44 00 W. Distance —— 91 Mil
                                              New Departure -
                                  91 Miles
                                              Departure by D.R. -
  By
                                  53 S.
         Difference of Lat.
                                 63 W.
fince last ) Departure-
                                              Their Sum -
Obser. Latitude by D R. 40 59 N. Lat. by Obser. 41 11 N.
                                              Sum, or true Dep .-
```

In this Case, the Course by D.R. since the last Observation, being more than 33, and less than 67 Degrees, I correct by Case the 3d.

H.	K.	HK	F.	Courfes	Winds	Lee- way	Transactions, Wednesday, May the 24th, 1780.
2	4			W	SE		
4 6	.4						Cloudy the first Part, the lat-
6	4						ter moderate and fair.
8	4						
10	4						
12	4				_E.		
2	4						
4	4						
6	4						
8	3	1					
10	3	I					Variation 1/2 Point Westerly.
12	3	I			NNE.		
Cou	rſe	Dist.		WLath	yDR L	at by(Ob Mer. Dist. Lon. made Lon. in
We	est	93	_	93 41	02N. 4	III	N. 8 18 W. 11 56 W. 15 41 V

Courfes					
\overline{W} bS $\frac{1}{2}$ \overline{W}	93		9.1		92.6
		D	iff. L	at.	Dep

Corrected by Case the 4th, the Course by D. R. being more than 6 Points.

```
By Distance — W. by S. ½ W. Distance — 93 Miles Difference of Lat. 9 S. Departure— 93 W. Latitude by D.R. 41 02 N. Lat. by Obser.— 41 11 N.
```

	Course	- Wes	ŧ
	Distance — Difference of Lat.	93 Mil	108
Cor-	Departure — Lat. by D.R.—41	93 W.	
rected	Lat. by Obser.—41 Meridian Dist.—8	II N.	
	Longitude made 11 Longitude in —15	56 W.	

Note, When the Course is due East or due West, as in this Case, then the Difference of Longitude cannot be found by the Course, and the Meridional Difference of Latitude as before, but must be sound as follows; look in the Tables of Difference of Latitude and Departure, for the nearest Degree to your Latitude, which here is 41, and in some of the Difference of Latitude Columns belonging to that Degree find your Departure, which in this Case is 93, the Distance answering to that which is 123, gives your Difference of Longitude.

H.	K.	HK	F.	Courses	Winds	Lee- way	Transactions, Thursday, May the 25th, 1780.
2	4	I		S by W	N		Little Wind and Hazy all thefe
6	3	1					24 Hours.
8	3			ssw	NW		
10	3	•					,
2.	3						
6	3			SbWIW	WNW		
8	3.						
10	3						Variation 1/2 Point Westerly.

Courfes	Dift.	N.	S.	E.	W.		Course — S. 11 00 V Distance — 76 N
$S \stackrel{\mathbf{I}}{=} W$	28		27.9		2.7		Difference of Lat. 74 S
5 by W 1/2 W	24		23.0		7.0	Ву	Departure — 14 V Lat. by D R — 39 57 M
S by W	24		23.5		4.7	D.R.	Lat. by Obser.—
			74.4		14.4		Meridian Distance 8 32 V Longitude made 12 15 V
*					4	•	CLongitude in- 16 00 V

Note, Having in the foregoing Days Works given an Example to every Case of correcting, (for a single Day) I shall now set down two or three Days Work by D. R. and then shew how to correct them all together by an Observation, that is, how to correct for a longer Time than one Day.

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Н.	K.	нк	F.	Courfes	Winds	Lee- way	Transactions, Friday, May the 26th, 1780.
2	3	1		SSW	WbyN		Timbo Wind and Claude
6	3 4	1					Little Wind and Cloudy.
8	4				7117		
10	4			IS by W	W		
12	3	-	_				
2	3 3	1		S	wsw		
6	3						
8	3		_			10 / 10 mm 10	
10	- 3			SbWIW	W		Variation 4 Point Westerly.
12	3	I					
Coi	irfe	Dift.	S	WLath	by DR L	at.by(Ob Mer. Dist. Lon. made Lon. i
12 (00 W	83	82	17 38	35 N		8 49 W 12 38 W 16 23V

Courses	Dist.	N.	S.	E.	W.
by W 4 W	30		28.2		10.1
\$ 3 W	29		28.7		4.3
S 1/4 W	12		12.0	0.6	
S by W 4 W	13		12.6		3.2
			81.5	0.6	17.6
					06.6
					17.0

	CCourle S	oo W
	Course — S. 12 Distance —	83 Miles
	Difference of Lat.	82 S.
Cor-	Departure —	17 W.
	Lat. by D.R — 38	35 N.
ecled	Lat. by Obser.—	
	Meridian Distauce 8	49 W.
	Longitude made 12	38 W.
	CLongitude in— 16	23 W.

Н.	K.	нк	F.	Courfes	Winds	Lee- way	Transactions, Saturday, May the 27th, 1780
2	3	I LI I		SbW 4W	W _, byN		Little Wind and fair Weather
6	3	1	_	-		-	· · · · · · · · · · · · · · · · · · ·
8	3 3	I					
12	3		_				
2 4	3 3			S by W	w		
$\frac{6}{8}$	3	1	-			-	
10	3	1					Variation 4 Point Westerly.
12	3		1	 	<u> </u>	<u> </u>	
Cou	rfe	Dift.	S	W Lath	by DR L	at.by(Ob Mer. Dist. Lon. made Lon. in
S14 (ooW	74	72	17 37	23 N		9 06 W 13 1 W 16 46W

Courfes	Dist.	N.	S. 1	E.	W.
$SbW_{\frac{1}{2}}W$	46		44.0		13.3
$S \frac{3}{4} W$	28		27.7		4.1
			71.7		17.4

	Course ————S.	14	CO	W.
	Distance		74	Miles
	Difference of Lat.		72	S.
By	Departure		17	W.
1	Lat. by D R	37		
D.R	Lat. by Obser	ere Circ		
	Meridian Distance	9	06	W.
1	Longitude made	13	01	W.
l	Longitude in -	16	46	W.
	W The second sec			

н.	K.	нк	F.	Courfes	Winds	Lee- way	Transactions, Sunday, May the 28th, 1780.
2 4 6	4 4 4			S by W	WbyN		Moderate Gales and Fair.
8 10 12	4 4 4						
2 4 6	4 4 4			S b W ¼ W			
8 10	4 4 4						Variation 4 Point Westerly.
45 1 1 1 1			1.	1 .1 .			
Coi	irfe	Dift.	S.	WLath	by DR L	at.by(Ob Mer. Dist. Lon. made Lon. in

Now being to correct from the last Observation, which was on Wednesday, May 26, I take the Northing, Southing, Easting, and Westing for every Day since, and bring them into a Traverse-Table as follows.

Departure -

day Latitude by D.R. 35 48 N. Latitude by Ob. 35 36 N.

yester-)

B		N.	S. E.	W
By D.R. fince the	On Thursday, May 25		74	14
laft	On Friday 26		82	17
Obser.	On Saturday 27		72 1	17
vation.	On this as above 28		95 1	16
	Whole Diff. of Lat. by D.I	R. S.	323 Dep. 6	64W.
	Gives Course by D.R. since	last Ob	sfer. S. 11.0	ooW.

94.6

My Course found by D. R. since the last Observation, being S. 11 00W. which is less than 33 Degrees, I am to correct by Case the 2d, (Page 48) and to find every Thing, except the Distance, as follows;

First, For the true Difference of Latitude.

Take the Latitude by the last Observation ————————————————————————————————————	41 11 N. 35 36 N.
Gives the Difference of Latitude	5 35 S.
Which multiplied by 60, makes —	335 Miles.

Second, For the true Courfe.

The Course by D. R. since the last Observation, being S. 11 00 W. I set it down for the true Course, as per Rule in Case the 2d.

Third, For the true Departure.

With the true Course 11 Degrees, and the true Difference of Latitude (divided by 2, because too great to be found in the Tables) which makes it 167.5, (by Plane Sailing, Case the 2d) I find the Departure 32.6, which multiplied by the same Number the Difference of Latitude was divided by, viz. 2, gives 65.2 Tenths for the true Departure.

Fourth, For the Meridian Distance.

Take the Meridian Distance at the last Observation ————————————————————————————————————			
Gives the Meridian Distance To-day	9	23	w.

Fifth, For the Difference of Longitude.

Take the Meridional Parts of the last Observation	- 2716
And the Meridional Parts of To-day's Observation	- 2288
Gives the Meridional Difference of Latitude	428

Sixth,

X

My

Sixth, For the Longitude made.

Take the Longitude made in the last Observation —	d. - 11	m. 56 W.
And the whole Difference of Longitude	— I	23 W.
Gives the Longitude made ————————————————————————————————————	- 13	19 W.
Seventh, For the Longitude in.		
Take the Longitude in the last Observation ————————————————————————————————————	d. - 15 - 1	m. 41 W. 23 W.
Gives the Longitude in	- 17	04 W.
Distance ————————————————————————————————————	d. m 9 00 8 M 7 S. 7 V	o W. Iiles
The Course, Difference of Latitude and Departure, as above, being made fince the last Observation (which was four Days ago) and as it them down only as they are made from Noon to Noon, therefore they are out, and found again as follows:	is usi	ial to fet be rubbed
First, Take the Latitude by D.R. Yesterday And the Latitude by Observation To-day	d. - 37 - 35	. m. 23 N. 36 N.
Gives the Difference of Latitude		47 S.

Then, with the Difference of Latitude 107, and the Departure 17 Miles, (by Plane Sailing, Case 6.) I find the Course to be 9 Degrees, Distance 108 Miles, as above.

Second, Take Yesterday's Meridian Distance —
And the Meridian Distance To-day

Gives the Departure -

o6 W.

17 W.

Н.	к.	нк	F.	Courfes	Winds	Lee-way	Transactions, Sunday, May the 28th, 1780.
2 4 6 8 10 12 2 4 6 8 10	5 5 6 7 7 8 8 8 8 8 9	I I I		S by W	N		By Reckoning I make my Course from the Start to the Island of Madeira S. 32 00W. Distance 420 Leagues; Meridian Distance and Disserence of Latitude as underneath. At Noon saw the Island of Madeira, bearing S.W. by W. Distance 14 Leagues. Variation 00.
Cou	irle	Dift.	S	WLat	byDR	_at.by	Ob Mer.Dist. Lon.made Lon.in
\$19	00 W	213	10:	70 32	14 N		10 32 W 4 43 W. 18 30 W

Courfes	Dist.	N.	S.	E.	W.
S by W	182		178.5		35.5
SW by W	42		23.3		34.9
			01.8		70.4

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The Bearing of the Land being SW. by W. diffant 14 Leagues, or 42 Miles, I fet them in the Traverse-Table as a Course, &c.

Course-S.19	00	W.
Distance	213	Miles
Difference of Lat.	202	S.
Departure —	70	W.
Lat. by D.R. — 32		N.
Meridian Distance 10	33	W.
Longitude made 14		W
Longitude in 18	30	W.

It being customary upon making the Land, to find what Course and Distance the Ship has made, by reckoning from the Place sailed from, to the Place arrived at, it is to be done as, follows:

CASE the First. When you keep the Account of Longitude in.

With the Latitude and Longitude of the Place you failed from, and the Latitude and Longitude you are in by your Reokoning on the Day you make the Land, find the proper Difference of Latitude, the Meridional Difference of Latitude, and the Difference of Longitude in Miles, and with them find the Course and Distance, as it is shewn at large in Mercator's Sailing, Case the First, Page 55.

CASE the Second. When you keep the Account of Longitude made.

Then the proper Difference of Latitude, and the Meridian Difference of Latitude are to be found as before, and the Difference of Longitude is to be found, by bringing the Longitude made into Miles, with which roceed, as in Case First.

The

The Agreement between these two Ways may be seen as follows:

On the 29th of May, when I made the Longitude in was Long. of the Start, or Place failed from -	Land, my -18 30 W. -3 47 W.	On the same Day my Longitude made was ———————————————————————————————————
The Difference of Longitude ————————————————————————————————————	14 43 E.	Makes the Diff. of Long. 883 Miles The fame as in the other Cafe.
Makes —————	883 Miles.	

To find the Bearing and Distance of any Place from the Ship, upon any given Day.

Example. Suppose I would know how Madeira bore from me, and what Distance on the 23d of May, by the foregoing Journal.

First, Supposing I kept only the Account of Longitude in;

Then, with the Latitude in 41 11 N. And the Latitude of Madeira 32 44 N.	2716 M.P. 2080 M.P.	And with Long. in — 15 43 W. And the Long. Madeira 7 26 W.
I find the proper Diff. of Lat. 8 27 S.	636	I find the Diff. Long. 1 43 W.
Which multiplied by 60 makes 507 Mi.	M. D. L.	Which makes — 103 Miles.

Then with that Meridional Difference of Latitude, and Difference of Longitude, I find the Course to be S. 09 00 W. and the Distance 501 Miles, as in Mercator, Case 1.

But if I had kept only the Account of Longitude made, which is Difference of Longitude, then,
d. m.

With the Longitude failed from ______ 3 47 W. And the whole Difference of Long. or Long. made _ 11 56 Westerly,

By Rules for Long. (Page 107) I should have found Long. in 15 43 W.

And then I have given the Latitude and Longitude in, &c. as before.

I have, in the foregoing Journal, shewn how to correct, either for a fingle Day, or for a longer Time, and given Examples of every Case for correcting from one Observation to another; but as it may happen that you may be some Days at Sea, from the Time of your leaving the Land, before you have an Observation, and that when you get the first Observation, you may have Occasion to correct, and there being nearly the same Difference between working the Correction from one Observation to another, and between the first Observation and the Land, as there is between working the first Day's Work, and any of the following Days, I shall here give an Example from the foregoing Journal.

To correct from the Time of leaving the Land to the first Observation.

Example. Suppose that in the foregoing Journal, on the 13th of May, I was by Observation in Lat. 45 10 N. my Latitude by D. R. being 45 23 N. my Southing by

D. R. 95, and Westing 24.

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Now being to correct, and having had no Observation before To-day, I must correct from the very beginning of my Journal, that is, from the Time of my leaving the Land, by bringing the Northing, Southing, Easting and Westing, for every Day I have been at Sea, into a Traverse-Table as follows.

By D. R. from the Time of leaving the Land.

	N.	S.	E.	W.
On the first Day.		93		53
On the fecond Day.		96		61
On the Day I correct.		95		24
Whole Difference of Lat. by D. R.	S.	2841	ep. 1	38W

Gives the Course by D. R. from the Time of leaving the Land S. 26.00 W.

The Course found by D. R. from the Time of leaving the Land, being less than 33 Degrees, I am to correct by Case the Second, and to find every Thing, except the Distance, as follows:

First, For the true Difference of Latitude.

Take the Latitude of the Place failed from — 50 07 N.

And the Latitude in by Observation — 45 10 N.

Gives the true Difference of Latitude — 4 57 S. or 297 Miles.

Second, For the true Courfe.

The Course by D. R. since the Time of leaving the Land being S. 26 00 W. I set down for the true Course, as by the Rules for correcting.

Third, For the true Departure.

With the true Course 26 Degrees, and half the true Difference of Latitude 148.5, (because the whole is too large to be found in the Tables) by *Plane Sailing*, Case the Second. I find the Departure 72.3, which being doubled (because the Difference of Latitude was halved) gives 144.6 for the true Departure.

Fourth, For the Meridian Distance.

Whenever you correct from the Time of your leaving the Land (as you do here) the Meridian Distance will always be the same as the true Departure found by correcting which in this Case is 145 Miles, or 2.25 W. Fifth

Fifth, For the Difference of Longitude.

Take the Meridional Parts of the Latitude failed from ————————————————————————————————————	- 3485 - 3044
Gives the Meridional Difference of Latitude — — — — —	441
With the Half of which (because the whole is too large to be found in the Tables) and the true Cogrees (as directed in the first Day's Work, Page 134) I find the Different tude 107.4, which doubled (because the other was halved) gives the true Longitude 214.8.	ice of Longi.

Sixth, For the Longitude made.

Whenever you correct from the Time of your leaving Land, as you do in this Case, then the Longitude made will always be the same as the whole Difference of Longitude found by the Correction, which in this Case is 215 Miles, or 3.35 W.

Seventh, For the Longitude in.	đ	m.	
Take the Longitude of the Place you failed from ————————————————————————————————————	- 3	47	W.
Gives the Longitude in			

5. 26 00 S. 16 00 W. 113 Miles Distance -Diff. of Latitude — 108 S. 297 145 W. Departure -----31 W. Corrected Latitude by D. R.— 45 23 N. Lat. by Observation 10 N. 45 Meridian Distance -25 W. 2 Longitude made — 35 W. [Longitude in — 22 W.

The Course, Difference of Latitude and Departure, as above, being what has been made in the whole, from the Time of leaving the Land, which is three Days, and as it is usual to set them down only as they are made from Noon to Noon, therefore they are to be rubbed out, and found again as follows:

First, Take the Latitude by D. R. Yesterday ————————————————————————————————————		
Gives the Difference of Latitude	I	48 S.
Second, Take the Meridian Distance Yesterday ————————————————————————————————————	I	54 W. 25 W.
Gives the Departure	0	31 W.

Then with the Difference of Latitude 108, and the Departure 31 Miles (by Plane Sailing, Case 6.) I find the Course to be S. 16 00 W. Distance 113 Miles, as above. Having, in the preceding Journal, shewn how to find what Latitude and Longitude the Ship is in, on any Day, I shall in the next Place shew how

By that Longitude and Latitude in, to mark off the Place of the Ship on the Mercator's Chart.

Rule. Lay a Ruler across the Chart, in the Latitude your Ship is in, then look upon the Equinoctial, or Line marked with the Degrees of Longitude, for the Longitude your Ship is in by your Reckoning, and setting one Foot of your Compasses in that Longitude, take the nearest Distance to some North and South Line, and from where that Line crosses the Edge of the Ruler which lies in the given Latitude, lay off the same Distance, by the Edge of the Ruler, to the Right Hand, if the Longitude you are in be to the Right Hand of the North and South Line, or to the Left Hand, if it is to the Left; where this falls will be the Place of the Ship. But this will only serve when the Longitude marked off the Chart, and your Reckoning of Longitude in, are both counted from the same Meridian, therefore for a general Rule, take the following

By the Latitude in, and Longitude made, to mark off the Ship's Place, &c.

Rule. Set one Foot of your Compasses in the Place you take your Departure from, and take the nearest Distance to some North and South Line, and from where that Line salls upon the Equinoctial, or Line marked with the Degrees of Longitude, set off that Distance the same Way as the Place lies from it (that is, to the Right Hand, if the Place lies to the Right Hand of the North and South Line, or to the Lest Hand, if it lies to the Lest) and make a Mark with a black Lead Pencil; this Mark will serve to mark off by, until you come to take a new Departure, and then you rub it out, and make a new one, as before.

Then lay a Ruler across the Chart in the Latitude you are in, and taking so many Degrees in your Compasses (from the Line of Longitude) as your Longitude made comes to, set them off from your Black Lead Mark to the Eastward, if the Longitude made be East, or to the Westward, if it be West; where this falls will be the Longitude the Ship is in by the Chart, from which take the nearest Distance to some North and South Line, and from where that Line, &c. as in the first Case.

The Ship's Place on the Mercator's Chart being found, as before taught, it remains in the next Place to shew how to find the Bearing and Distance of any Place from the Ship; and first,

To find how any Ship bears from the Place.

Rule. Lay a Ruler from the Place of the Ship to the Place you would know the Bearing of, then fet one Foot of your Compass in the Center of some Compass near the Ruler, and take the nearest Distance to the Edge of the Ruler, then move one Foot of your Compasses along by the Edge of the Ruler, and observe what Point of the Compass the other comes nearest to, which will be the Bearing required.

To

To find the Distance of any Place from the Ship.

Case the 1st. If the Place be under the same Longitude that the Ship is in, (that is if it bears due North or due South) then the Difference of Latitude between them (found as by the Rules for Latitude, Page 105) and turned into Miles, or Leagues, will be the Distance.

Case the 2d. If the Place be in the same Latitude that the Ship is in, that is, if it bears due East or due West, then take half the Distance between the Ship and the Place, in your Compasses, and setting one Foot (on the Line marked with Degrees of Latitude) in the Latitude the Ship is in, see what Latitudes the other Foot will reach to, both above and below it; the Difference between these two Latitudes, found as per Rule for Latitudes, will be the Distance required.

Case the 3d. If the Place be neither in the same Latitude nor Longitude with the Ship, then take the Difference of Latitude between them, in Degrees from the Equinoctial Line, and laying a Ruler from the Ship to the Place, apply one Foot of the Compasses so to the Edge of the Ruler, that the other Foot turned about may just touch some East and West Line which is crossed by the Ruler; then take the Distance along the Edge of the Ruler, from the Place where the Compasses rested, to the Place where the Ruler crosses the said East and West Line; that Distance measured on the Equinoctial, or Degrees of Longitude, will give the Distance in Degrees, which you may turn into Miles or Leagues; and in the same Manner as you find the Bearing and Distance of any Place from the Ship, you may also find the Bearing and Distance of one Place from another.

F 1 W 1 S.

